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#### **STRUCTURES DESIGN BULLETIN C10-05**

DATE:	July 12, 2010
TO:	District Directors of Production, District Design Engineers, District Structures Design Engineers, District Construction Engineers, District Prestress Engineers, Ghulam Mujtaba, David Sadler
FROM:	Robert Robertson, P.E., State Structures Design Engineer
COPIES:	Brian Blanchard, Lora Hollingsworth, Steve Plotkin, Jeffrey Ger (FHWA)
SUBJECT:	Implementation of Squaring the Ends of Florida-I Beams, Reorientation of Bearing Pads and the Elimination of Permanent End Diaphragms in Concrete Girder Bridges

This Structures Design Bulletin (SDB) is a follow-up to SDB C10-04 released in May 2010. This SDB implements the squaring of the ends of Florida-I Beams, reorientation of Bearing Pads, and the elimination of permanent end diaphragms in Florida-I Beam pretensioned simple span bridges. The plan for these improvements was included in SDB C10-04; included here are the effects of the implementation.

#### **REQUIREMENTS**

#### 1. Design Standards

The Florida-I Beam and related Design Standards Index Sheets have been updated and Index No. 20512 has been released for implementation with the July 2010 Interim Design Standards. Copies of these sheets and their associated data tables are included with Attachment 'A' as listed below.

Attachment 'A', New and Released Design Standards:

- a. Index No. 20010 (2 Sheets): Typical Florida-I Beam Details and Notes
- b. Index No. 20036 (2 Sheets): Florida-I 36 Beam Standard Details
- c. Index No. 20045 (2 Sheets): Florida-I 45 Beam Standard Details
- d. Index No. 20054 (2 Sheets): Florida-I 54 Beam Standard Details
- e. Index No. 20063 (2 Sheets): Florida-I 63 Beam Standard Details
- f. Index No. 20072 (2 Sheets): Florida-I 72 Beam Standard Details
- g. Index No. 20078 (2 Sheets): Florida-I 78 Beam Standard Details
- h. Index No. 20510 (1 Sheet): Bearing Pad Details for Florida-I Beams
- i. Index No. 20512 (2 Sheets): Bearing Plate Details for Florida-I Beams

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### 2. Structures Manual Volume 1: Structures Design Guidelines

Revise the Structures Design Guidelines as follows:

a. Section 4.2.10: Skewed Decks – Revise the last sentence of Paragraph B as follows:

In addition For all bridges, except those with a thickened slab end as used with Florida-I beam simple span structures, three No. 5 Bars at 6-inch spacing, full-width, must be placed parallel to the end skew in the top mat of each end of the slab.

b. Section 4.2.13: Thickened Slab End Requirements – Add the following section:

For pretensioned simple span Florida-I Beam bridges, design thickened slab end at locations of slab discontinuity not supported by full depth diaphragms. See *SDM* Chapter 15 for thickened slab end details.

- c. Section 4.3.1: General Replace Paragraph F, add Paragraph G, H and I and add Commentary:
  - <u>F.</u> Click to view Standard Prestressed Beam Section Properties. <u>Standard prestressed beam</u> properties are included in Volume 3 of the Structures Manual.
  - <u>G.</u> For pretensioned simple span Florida-I Beam bridges, eliminating the permanent end diaphragms is the preferred option. However, in cases where there are significant lateral loads, partial depth, permanent end diaphragms may be used. See *SDM* Chapter 15 for partial depth diaphragm details. For spans requiring end diaphragms, determine if diaphragms are necessary for every bay.

Commentary: For spliced post-tensioned girder bridges, diaphragms at the splice and anchorage locations are required.

H. Analyze spans subject to significant lateral loads to determine if diaphragms are needed.

Commentary: When investigating the effect of significant lateral loads such as vessel collision or wave loads, check the stresses at the interface of the beam top flange and the beam web, from each end of the beam to a longitudinal distance approximately equivalent to the beam height.

I. When precast pretensioned I-beam ends are not encased in concrete diaphragms, coat the ends of beams with two layers of type F-1 epoxy compound within seven days of detensioning. Prepare concrete surface and apply in accordance with the manufacturer's recommendations. The finish thickness of the epoxy coating must be a minimum 1/16 inch.

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- d. Section 6.5.2: Maintainability Revise Paragraph A.3 and Paragraph B and add Commentary:
  - 3. Design and detail provisions for the removal of bearings, such as jacking locations, jacking sequence, jack load, etc. Verify that the substructure width is sized to accommodate the jacks and any other required provisions. Simple span pretensioned Florida-I beams are exempt from this requirement.
  - B. The replacement of bearings for conventional girder structures, particularly concrete beams, is relatively simple, as jacking can be accomplished between the end diaphragms and substructure. For these bridges, a note describing the jacking procedure for replacing bearings will usually suffice. Certain non-conventional structures, such as steel girders or segmental concrete box girders, require separate details and notes describing the jacking procedures. For steel I-girder bridges, design so that jacks are placed directly under girder lines. For steel box girder bridges, design so that jacks are placed directly under diaphragms. Always include a plan note stating that the jacking equipment is not part of the bridge contract.

<u>Commentary: Few concrete I-beam bridges have required elastomeric bearing pad</u> <u>replacement. Occasional replacement of these pads does not justify requiring these</u> <u>provisions for every bridge.</u>

- e. Section 7.6: Widening Rules Add Paragraph F and Paragraph G:
  - <u>F.</u> When widening with Florida-I beams, squaring Florida-I beam ends, placing bearing pads orthogonally and eliminating permanent end diaphragms are the preferred options. However, skewed beam ends, skewed bearing pads and end diaphragms may be used at the discretion of the DSDE.
  - <u>G.</u> Where the existing bridge uses end diaphragms and diaphragms are proposed for the widening, connect the new diaphragm to the existing diaphragm. Drill and epoxy rebar into the adjacent existing diaphragm. Do not drill into existing beams.

#### 3. Structures Manual Volume 2: Structures Detailing Manual

Revise the Structures Detailing Manual as follows:

- a. Section 15.2: Superstructure Drawings Framing Plan Revise Sentence 3 as follows:
  - 3. Intermediate <u>and end</u> diaphragms
- b. Section 15.5: Superstructure Drawings Concrete Diaphragms Delete this section.
- c. Section 15.6: Superstructure Drawings Details Change section to 15.5, revise Paragraph D and add Paragraphs E through H:
  - D. Stay-in-place form details. See Figure 15.8-3, Figure 15.9-2, Figure 15.9-3, Figure 15.9-4 and Figure 15.9-5.

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- E. Thickened slab end detail. Show section and plan view. Use the standard dimension and reinforcement details shown in Figure 15.5-1 and Figure 15.5-2.
- F. Sections through diaphragms at piers and end bents. Detail reinforcement, expansion joints, construction joints and control joints. Include compressible material if cast back-to-back (such as two or more layers of 30lb felt paper) between adjacent diaphragms at interior supports. Show dimension between adjacent diaphragms at expansion joints. Coordinate with expansion joint details.
- <u>G.</u> <u>Section through intermediate diaphragms. Detail reinforcement to avoid conflicts with slab steel.</u>
- H. Jacking locations. Show jacking service loads in tabular format.
- d. Section 15.7: Deck Drains Change section to 15.6
- e. Section 15.8: Superstructure Design Considerations General Change section to 15.7
- f. Section 15.9: Superstructure Design Considerations Prestressed Beams Change to Section 15.8, revise Paragraph A and B as follows and add Paragraph F:
  - A. Avoid conflicts between diaphragm reinforcement and slab reinforcement. Detail these areas in the plans and on the bar list to ensure that there are no conflicts. Include diaphragm reinforcement in the bar list.
  - B. To facilitate jacking procedures, detail the bottom of end diaphragms as flat from corner to corner of adjacent beams, i.e. no steps or haunches. Generally, end diaphragms should be 12" thick. See Figure 15.9 1. When end diaphragms are required on spans with a Florida-I beam superstructure, partial depth diaphragms may be used. Show one vertical row of #5 bars at a minimum in each diaphragm threaded into inserts cast into beam. Show insert layout in the framing plan. See applicable beam Design Standard for vertical spacing of inserts. See Figure 15.8-1 and Figure 15.8-2 for details. Details shown are minimum dimensions and reinforcing. Diaphragm dimensions and reinforcing can be increased when required by analysis.
  - F. <u>Square all beam ends on simple spans utilizing Florida-I beam superstructures. See</u> Figure 15.8-4 through Figure 15.8-6 for details related to the squaring of beam ends.
- g. Section 15.10: Superstructure Design Considerations Steel Girders Change section to 15.9

Several figures included in Structures Manual Volume 2 were added due to the changes detailed herein. Copies of these figures are included with Attachment 'B' as listed below.

Attachment 'B', New Figures in the Structures Detailing Manual:

- a. Added Figure 15.5-1: Thickened Slab End Details
- b. Added Figure 15.5-2: Thickened Slab End at Interior Support
- c. Added Figure 15.8-1: Concrete End Diaphragm Details
- d. Added Figure 15.8-2: Concrete End Diaphragm Reinforcement Details
- e. Added Figure 15.8-4: Squared Beam End Details Exp. Joint at Int. Support
- f. Added Figure 15.8-5: Squared Beam End Details Continuous Deck at Int. Support

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g. Added Figure 15.8-6: Squared Beam End Details – Expansion Joint at End Bent

#### 4. Structures Manual Volume 3: Instructions for Structures Related Design Standards

Several sections of the Structures Manual Volume 3 were affected by the changes detailed herein. Copies of these sections are included with Attachment 'C' as listed below.

Attachment 'C', New and Revised Instructions for Structures Related Design Standards:

- a. Index No. 20010: Prestressed Florida-I Beam Instructions
- b. Index No. 20512: Bearing Plate Details for Florida-I Beams

#### 5. FDOT Standard Specifications for Road and Bridge Construction

a. Section 932 NONMETALLIC ACCESSORY MATERIALS FOR CONCRETE PAVEMENT AND CONCRETE STRUCTURES – Tentative changes are as follows, to be implemented with the January 2011 Standard Specifications:

SECTION 932-1.4 changed to 932-1.3.5 SECTION 932-1.5 changed to 932-1.3.6 SECTION 932-1.6 changed to 932-1.3.7 SECTION 932-1.4 to 932-1.6 (Pages 882–883) are deleted and the following substituted:

932-1.4 Pre-cured Silicone Sealant:

932-1.4.1 General: Pre-cured silicone sealants are intended for sealing vertical joints on concrete surfaces. Type V1 sealant is intended for contraction joints or joints with movements less than 1/4 inch. Type V2 sealant is intended for expansion joints not exceeding 200% of the nominal joint opening. Type V2 sealant may be substituted for Type V1 sealant. The joint sealant must be listed on the Department's Qualified Products List (QPL). 932-1.4.2 Physical Requirements: Sealant material shall be a nominal 1/16 inch thick, available in standard widths from 1 inch to 6 inches, colored to match the finish surface coating of the concrete, and meet the following minimum testing requirements:

_	TEST PROPERTY DESCRIPTION	TEST METHOD	TYPE V1	TYPE V2
	Minimum Movement, Cohesion/Adhesion	ASTM C 1523	100%	200%
	Dry/Room Temperature Loss of Adhesion/Cohesion	ASTM C 1523	None	None
	Water Immersion Loss of Adhesion/Cohesion	ASTM C 1523	None	None
	Frozen Loss of Adhesion/Cohesion	ASTM C 1523	None	None
	Heat Loss of Adhesion/Cohesion	ASTM C 1523	None	None
	Artificial Weathering Loss of Adhesion/Cohesion	ASTM C 1523	None	None

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TEST PROPERTY DESCRIPTION	TEST METHOD	TYPE V1	TYPE V2
Artificial Weathering Loss of Adhesion/Cohesion	ASTM C 1523	None	None
Tear Propagation	ASTM C 1523	NT or PT (No Tear or Partial/Knotty Tear)	NT or PT (No Tear or Partial/Knotty Tear)
Ultimate Elongation	ASTM D 412	250%	500%

The Contractor must submit one 6 inch long sample to the Engineer for approval, prior to installation, for each different colored surface to be sealed on the project.

932-1.4.3 Qualified Products List: Manufacturers seeking evaluation of their product shall submit an application in accordance with Section 6. Applications must include test results, an IR scan and a product data sheet with the recommended adhesive and installation requirements.

#### **COMMENTARY**

The following attachments may be used to assist in preliminary design and cost estimating:

Attachment 'A' (New and Revised Design Standards) Attachment 'B' (New Figures in the Structures Detailing Manual) Attachment 'C' (New and Revised Instructions for Structures Related Design Standards)

#### BACKGROUND

The implementation plan for squaring the ends of prestressed concrete Florida-I Beams, reorienting bearing pads, and eliminating diaphragms was introduced in SDB C10-04, released in May, 2010. The rationale for these improvements was detailed in that bulletin. Provided herein is the background regarding the decisions that were made in the process of implementing these changes.

In the process of revising the Florida-I Beam Standards to correspond with the change to no end diaphragms, the Bars '4L' were studied for their effectiveness in helping the Florida-I Beams (FIBs) meet the AASHTO *LRFD* 5.8.3.5 requirement for longitudinal steel. All cases of maximum and minimum FIB depths and spacing were checked using the FDOT Prestressed Beam Program V3.2. It was determined that Bars '4L' are ineffective in helping meet AASHTO requirements for longitudinal steel in FIBs. Even with larger-than-practical spans and far less-than-practical strand patterns, Bars '4L' were not required to meet longitudinal steel requirements in their effective distance from the end of the beams. For that reason, those bars were completely removed from the Florida-I Beam Standards.

It was suggested by prestressed beam manufacturers that the beveled bearing plate shown on Index 20511 be revised to be a parallelogram shape in order to eliminate the double bevel as a cost saving measure. This change was made, along with several revisions to the dimensions shown on the Standard to create more uniformity in steel plate overhang. In order to eliminate confusion between the revised and old

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Standard, the revised Standard was given a new number of 20512. Standard 20511 will be retired at a later date.

Although end diaphragms will not be necessary for most projects, there may be some projects where significant lateral loads are present and end diaphragms will be necessary. The need for diaphragms in these areas will be evaluated as part of the design, and when diaphragms are necessary, designers are encouraged to use partial-depth diaphragms wherever possible. Partial depth diaphragm details are included in the *Structures Detailing Manual* to provide designers with minimum reinforcing and dimensions. There may be some cases such as widening projects or projects with large lateral loads for which diaphragms and/or skewed end beams are required. The use of these details for these projects is left to the District Structures Design Engineer.

For bridges without full depth end diaphragms, a transverse thickened slab will be necessary to support the free edges of slabs between girders at discontinuities such as bridge expansion joints. The thickened slab is to be cast monolithically with the slab and designed in accordance with the AASHTO LRFD Bridge Design Specifications, Section 4.6.2.1.4. As part of the development of these improvements, the forces and related effects at a slab discontinuity were examined and a thickened slab design was completed. Transverse thickened slab details are included in the *Structures Detailing Manual* to provide designers with minimum reinforcing and dimensions.

Without the presence of end diaphragms, an aesthetic treatment will be necessary so that girder ends are not visible at intermediate piers. The most economical aesthetic treatment was determined to be a precured silicone sealant which will be adhered to the exterior face of the concrete girders and will span the horizontal gap between beams. Pre-cured sealant systems consist of approximately 1/16 inch thick silicone membrane that is bonded to the surface of the concrete with a compatible silicone based adhesive to create a weatherproof or visual seal. The sealant systems have been successfully utilized in building applications for many years, providing relatively inexpensive, durable, and easily replaceable sealant systems for vertical applications. The silicone sealant is available in a variety of colors and widths for sealing both fixed and expansion joints, and the low profile height creates an almost seamless finish on concrete surfaces with Class 5 applied coatings. Proposed specification language has been developed for approval of this new type of sealant system under Section 932 for implementation with the January 2011 Specifications Workbook.

At intermediate bents, where the beam crosses the joint between subsequent spans, a bond breaker will be required between the top flange of the beam and the bottom of the bridge deck so that the beam is not inhibited from rotating, expanding or contracting. The material selected as a bond breaker was Expanded Polystyrene (EPS). EPS is a very stable, lightweight and inexpensive joint filler that provides minimum resistance to compression and shear forces resulting from thermal movements and live load rotation of the bridge girders. This product has been successfully used for eliminating concrete spalling on retaining wall and approach slab copings for many years (see Index Nos. 20900 & 20910). The compressive stiffness is adequate to support the wet concrete during installation with negligible deformation, but allows for deformation under in-service conditions.

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#### **IMPLEMENTATION**

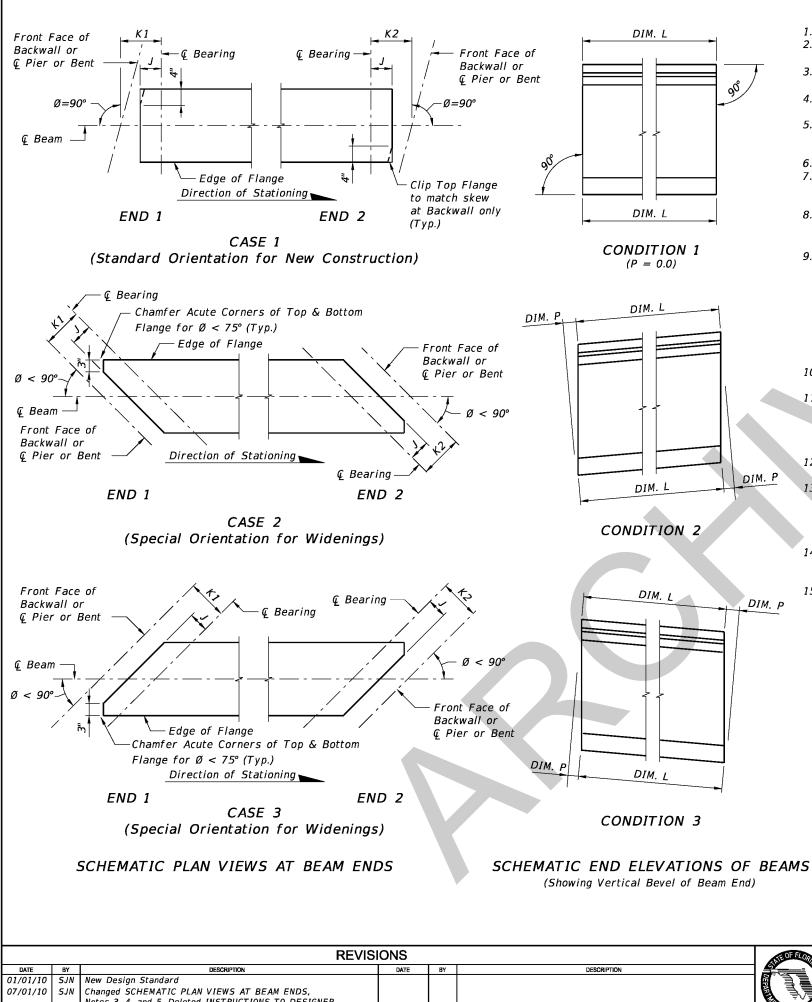
The changes detailed in this bulletin will be used on all Design-Bid-Build projects having a design start date on or after May 19, 2010, the date of implementation of Structures Design Bulletin SDB C10-04.

The changes detailed in this bulletin could be used on design-build projects having a Technical Proposal due date on or after May 19, 2010. Design-build projects which have already submitted Technical Proposals as of the date of this bulletin may incorporate this bulletin as a cost saving proposal at the discretion of the District Structures Design Engineer.

No redesign of on-going projects is required as a result of this bulletin, but districts may elect to revise present or completed designs at their discretion. Any bridge designed prior to the issuance of the revised Design Standards will require the Engineer of Record to complete the design.

#### **CONTACT**

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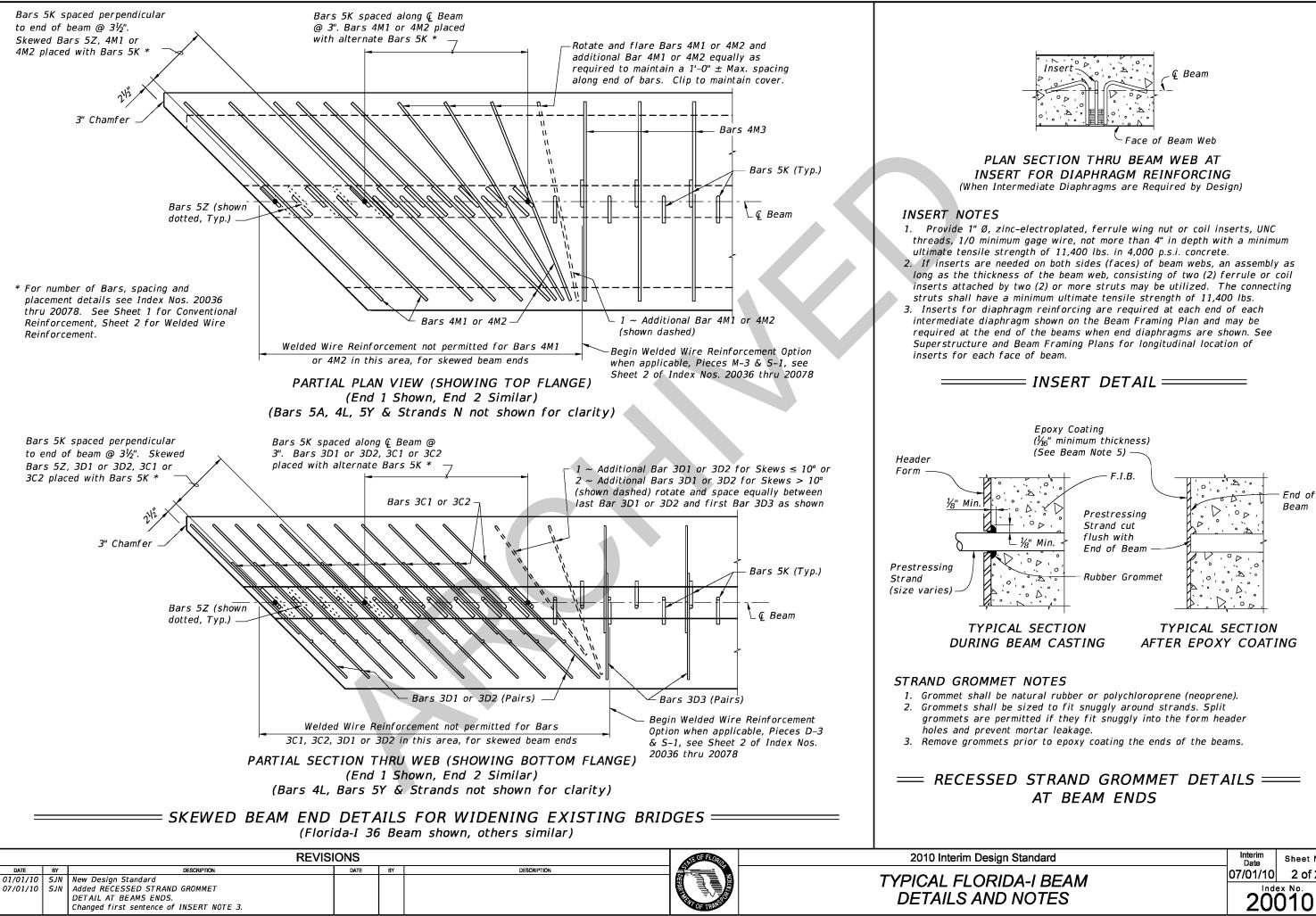
#### BEAM NOTES

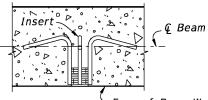
- 1. All bar dimensions are out-to-out.
- 3. Strands N shall be either ASTM A416, Grade 250 or Grade 270, seven-wire strands ¾" Ø or larger, stressed to 10,000 lbs. each.
- 4. Cut all Prestressing Strands flush with the end of the beam after detensioning and remove recessed strand grommets without damaging the surrounding concrete.
- 5. Epoxy coat ends of beams, including clipped and chamfer surfaces, with two layers of Type F-1 epoxy compound within 7 days of detensioning. Prepare concrete surface and apply in accordance with the manufacturer's recommendations. The finish thickness of the epoxy coating must be a minimum  $\frac{1}{16''}$ .
- 6. Unless otherwise noted, the minimum concrete cover for reinforcing steel shall be 2".
- 7. At the Contractor's option, welded deformed wire reinforcement may be used in lieu of Bars 3D, 5K, 4M, and 5Z as shown on the Standard Details for each beam size. Welded deformed wire reinforcement shall conform to AASHTO M221, with a minimum yield strength of 75 ksi.
- 8. Install Safety Sleeves approximately 2'-0" from ends of beam and spaced on 8'-0" (Max.) centers. Safety Sleeves shall be 21/2" NPS x 5" Sch. 40 PVC Pipe with Cap. Holes shall be free of debris and water prior to casting deck.
- 9. For beams with skewed end conditions, the end reinforcement, defined as Bars 3C1, 3C2, 3D1, 3D2, 5K, 4M1, 4M2, 5Y and 5Z placed within the limits of the spacing for Bars 3C in "ELEVATION AT END OF BEAM", shall be placed parallel to the skewed end of the beam. Bars 3D3, 5K and 4M3 located beyond the limits of Bars 3C shall be placed perpendicular to the longitudinal axis of the beam. Fan Bars as needed to avoid overlapping bars at the transition to Bars 3D3 and 4M3, and field cut to maintain minimum cover. Provide additional Bars 4M1, 4M2, 3D1 and 3D2 as required; additional bars are not included in the Number Required on the "BILL OF REINFORCING STEEL". For placement locations, see "SKEWED BEAM END DETAILS". Adjust the dimensions of Bars 3C1, 3C2, 3D1, 3D2, 4M1 and 4M2 as shown on the "BENDING DIAGRAM" for skewed end conditions.
- 10. Placement of Bars 3C1, 3D1 and 4M1 correspond to END 1, and Bars 3C2, 3D2 and 4M2 correspond to END 2. END 1 and END 2 are shown on the beam "ELEVATION".
- 11. For Beams with vertically beveled end conditions, place first row of Bars 3C1, 3C2, 3D1, 3D2, 5K, 5Y and 5Z parallel to the end of the beam. Progressively rotate remaining bars within the limits of Bars 5Z until vertical by adjusting the spacing at the top of beam up to a maximum of 1". For welded deformed wire reinforcement, cut top cross wire and rotate bars as required or reduce end cover at top of the beam to minimum 1".
- 12. For beams with skewed end conditions, welded deformed wire reinforcement shall not be used for end reinforcement (Bars 3D1, 3D2, 4M1 and 4M2).
- 13. Bars 5K and 5Z shall be placed and tied to the fully bonded strands in the bottom or center row (see "STRAND PATTERN" on the Table of Beam Variables in Structures Plans). At the Contractor's option the length of the bottom legs of Bars 5K and 5Z may be extended to facilitate tying to the exterior strands. For welded deformed wire reinforcement, supplemental transverse #4 bars are permitted to support Pieces K & S under the cross wires on the bottom row of strands.
- 14. At the Contractor's option, Bars 3D1, 3D2 and 3D3 may be fabricated as a single bar with a 1'-0" minimum lap splice of the top legs, or the length of the bottom legs may be extended to facilitate tying to the exterior strands.
- 15. For referenced Dimensions, Angles and Case Numbers, see the Table of Beam Variables in Structures Plans.

2010 Interim Desi TYPICAL FLOR DETAILS AN Notes 3, 4, and 5. Deleted INSTRUCTIONS TO DESIGNER.

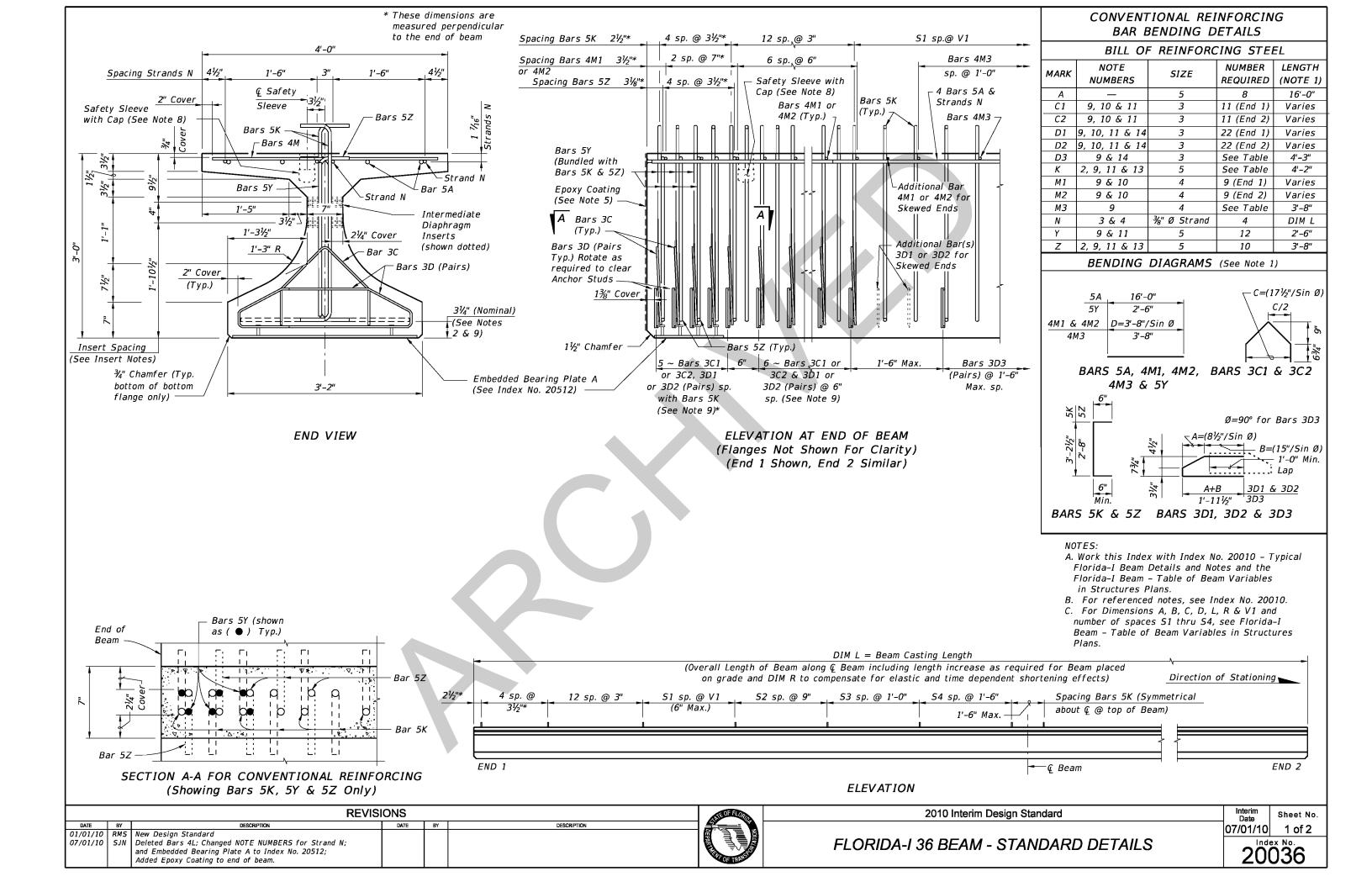
2. Place one (1) Bar 5K or 5Z at each location as detailed alternating the direction of the ends for each bar (see "ELEVATION AT END OF BEAM", Index Nos. 20036, 20045, 20054, 20063, 20072 and 20078).

ign Standard	Interim Date	Sheet No.
RIDA-I BEAM	07/01/10	1 of 2
D NOTES		<sup>ex №.</sup>

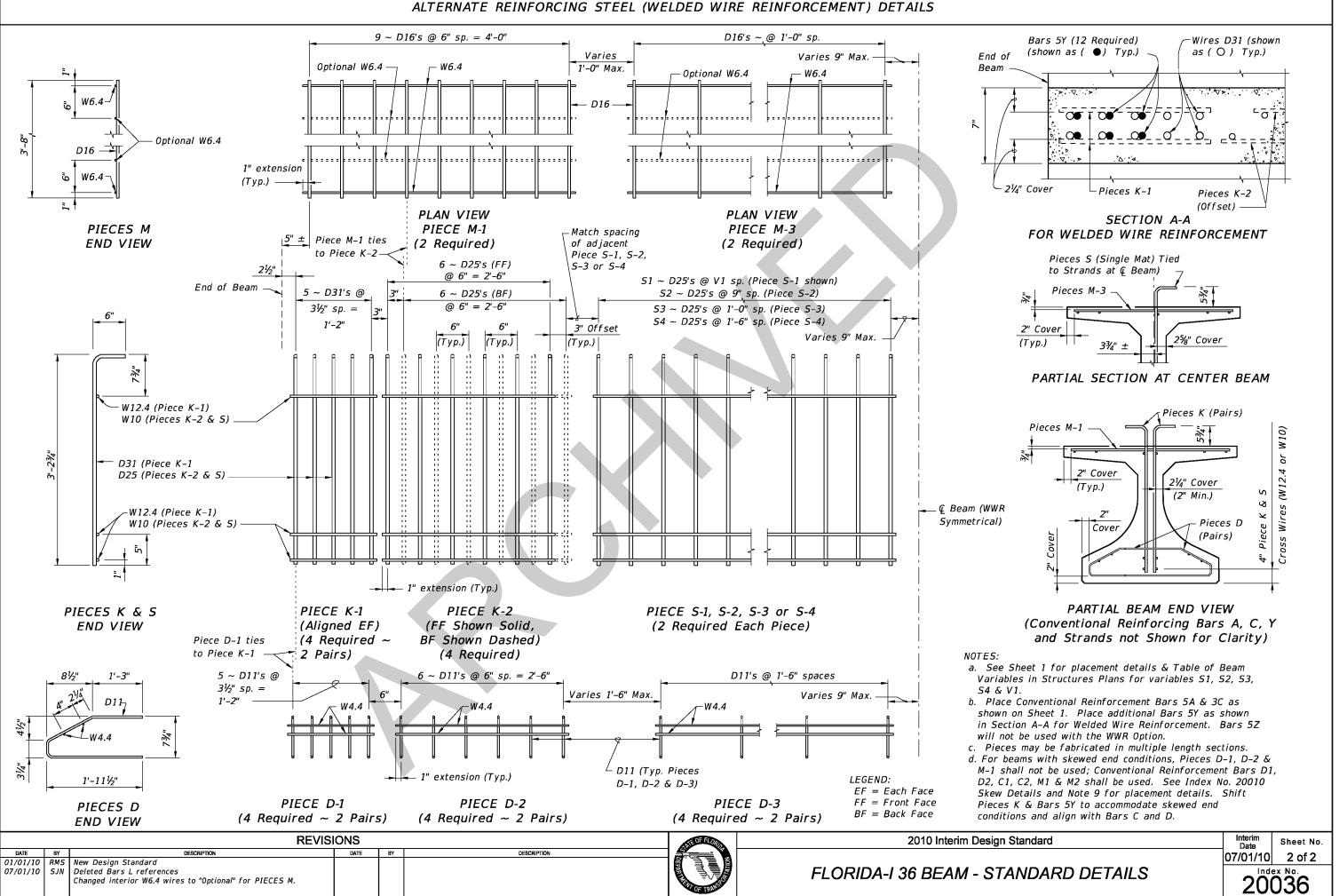


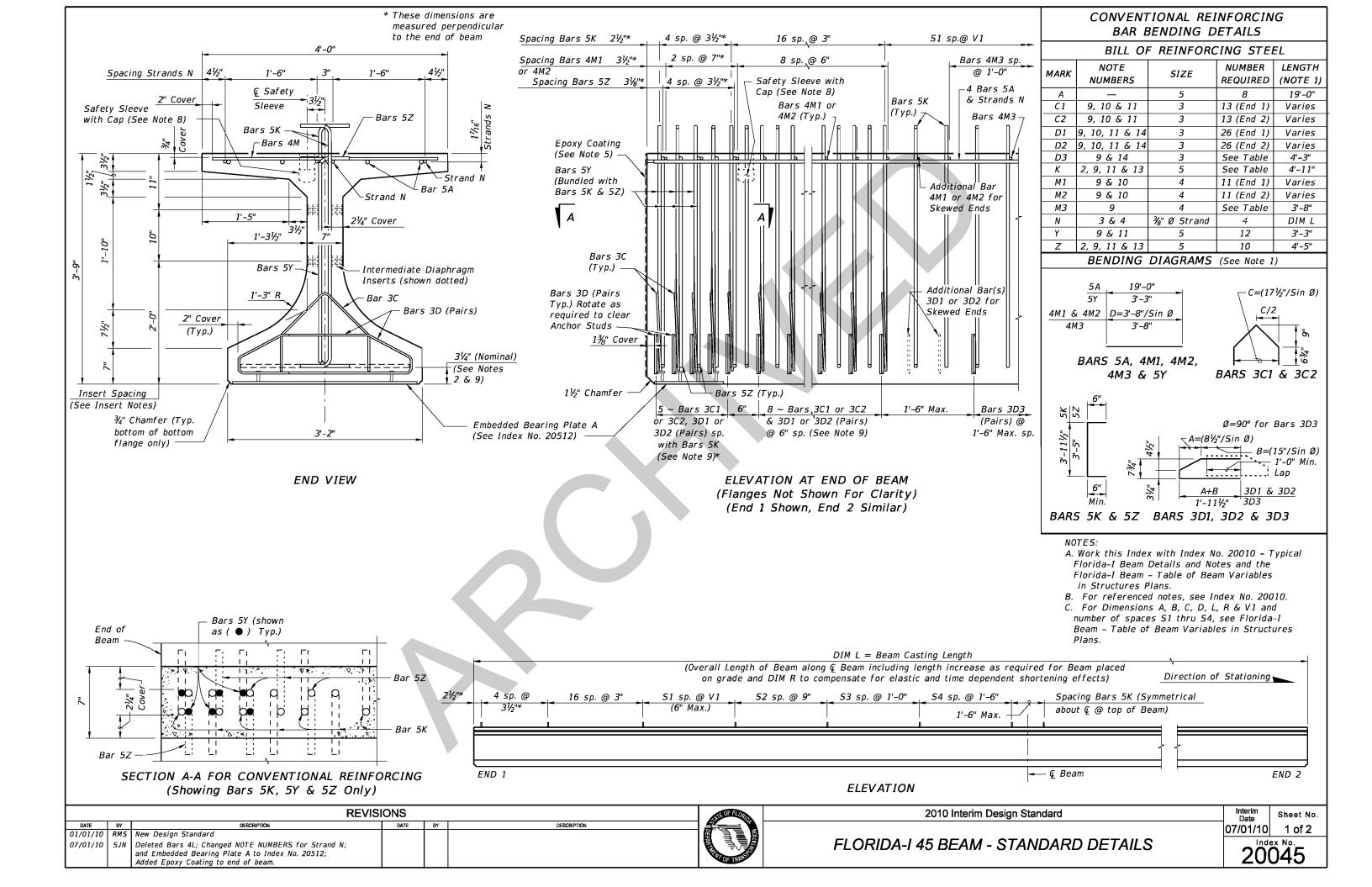


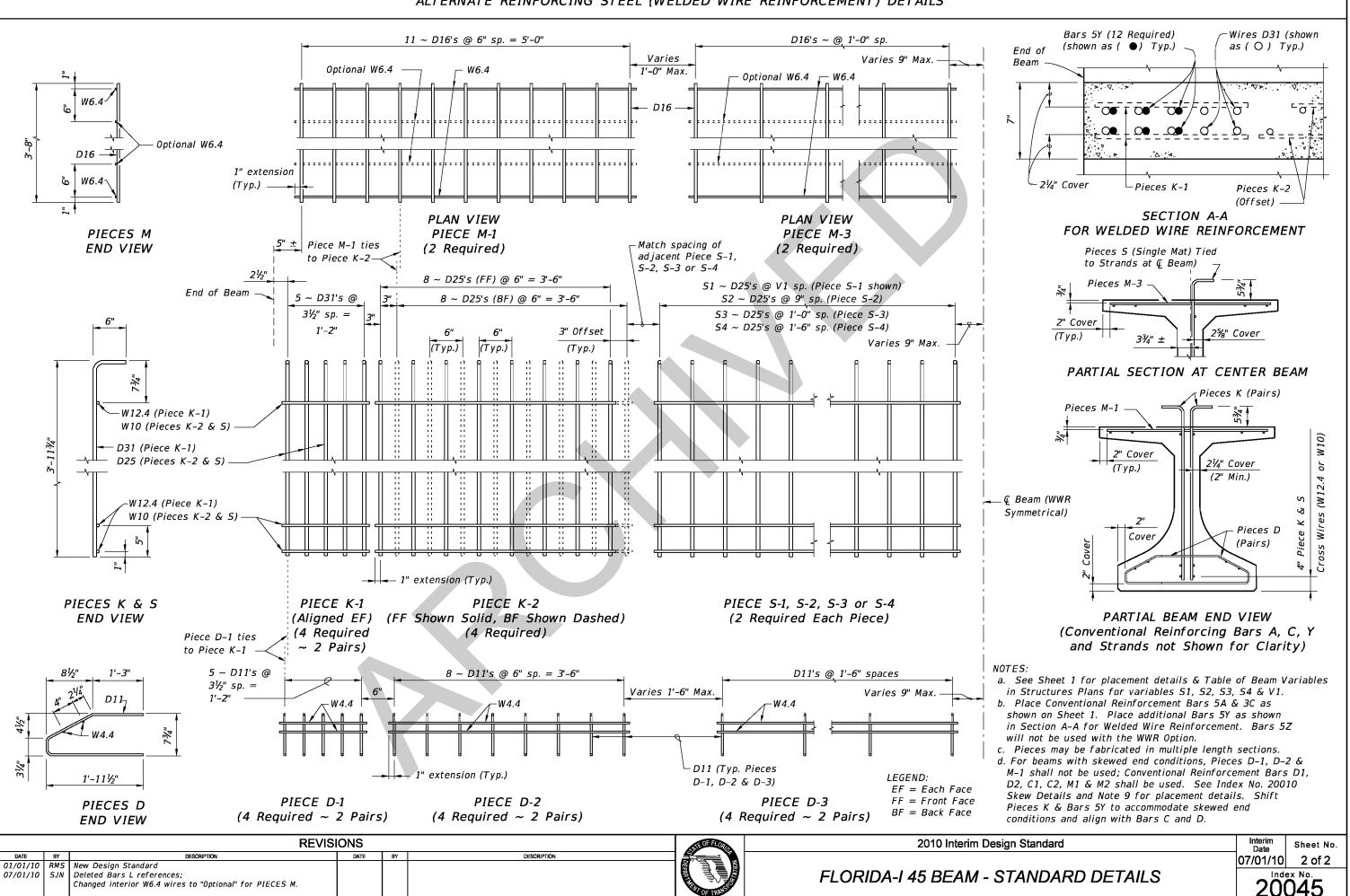
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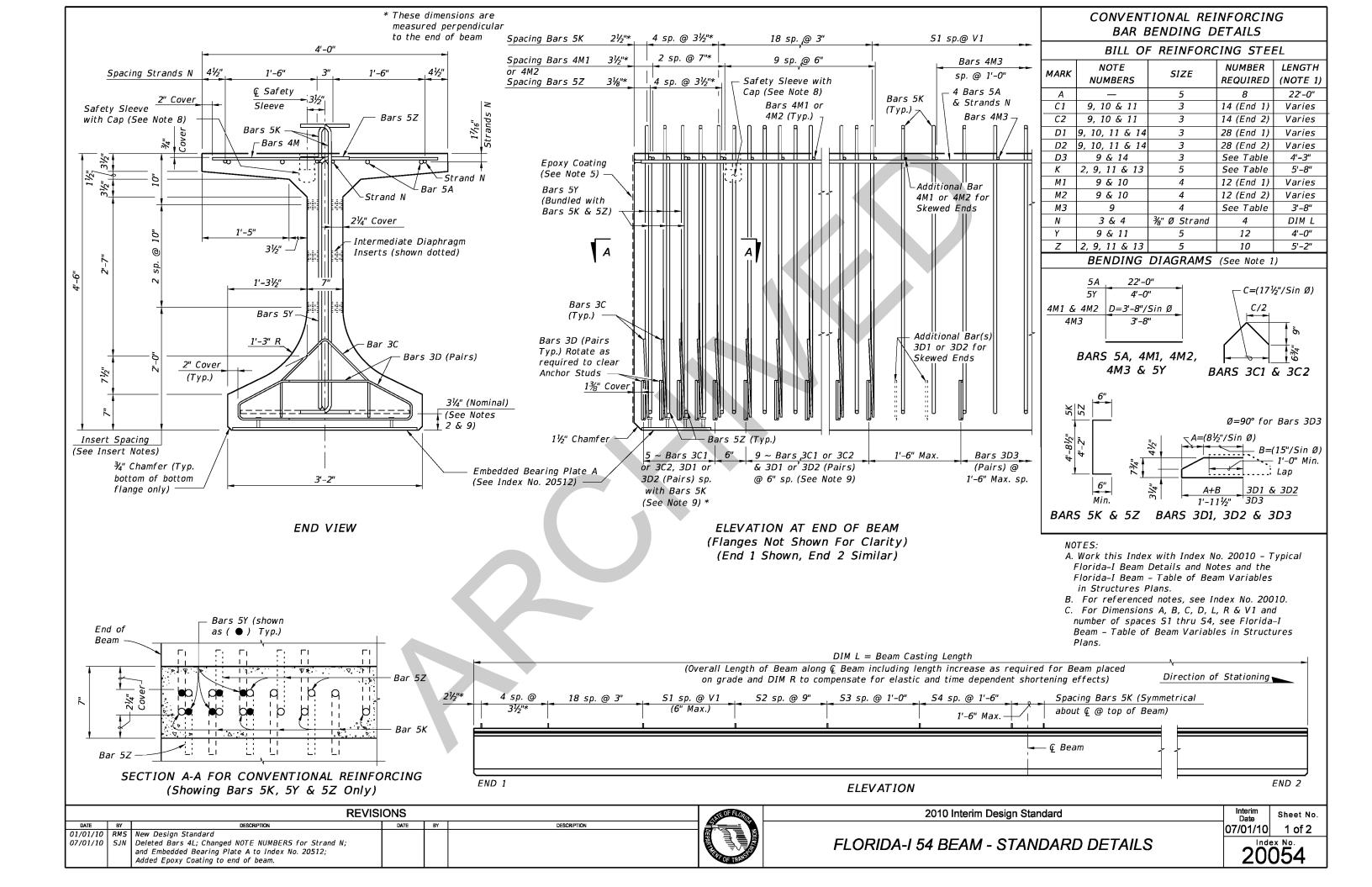


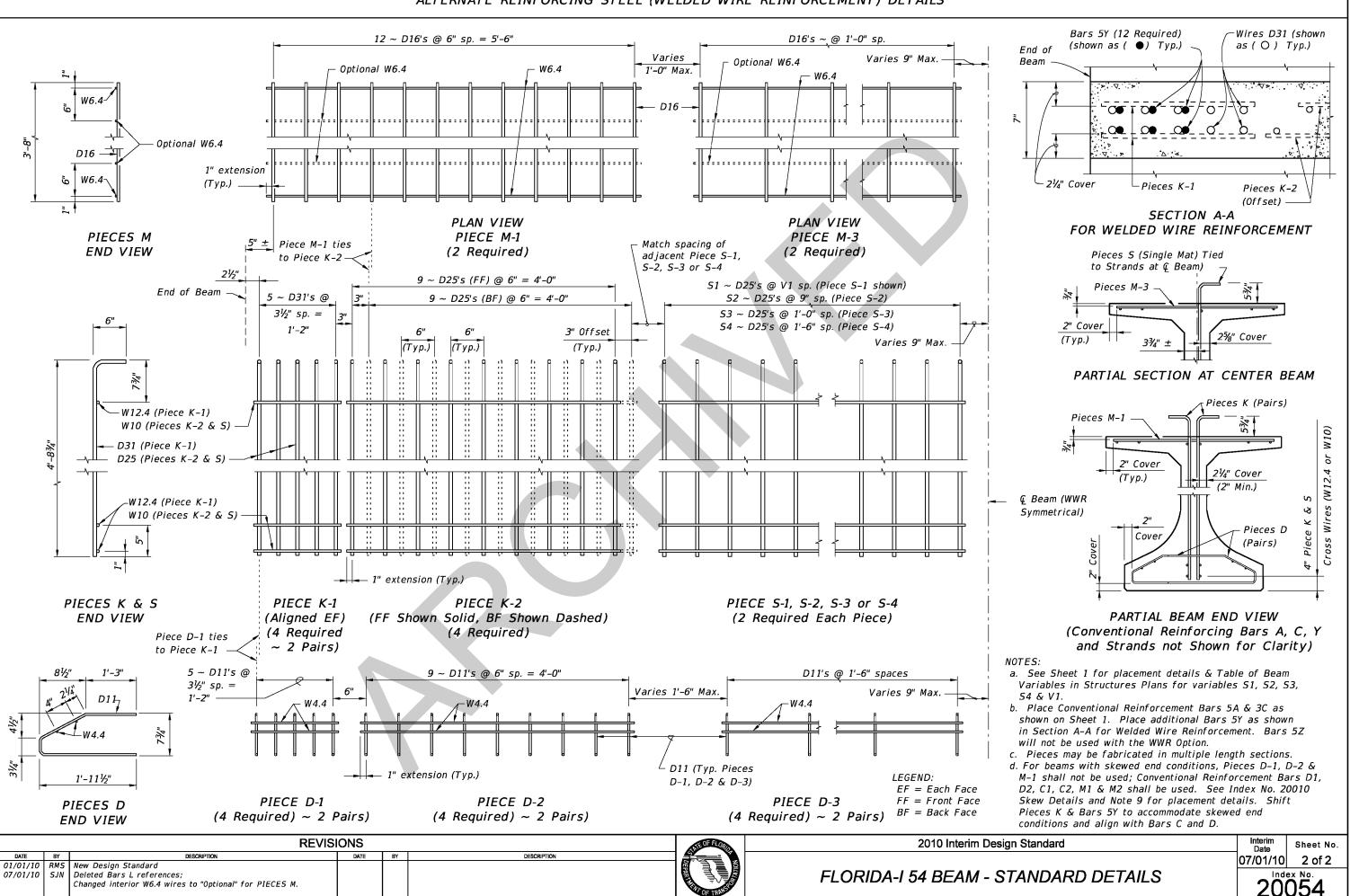


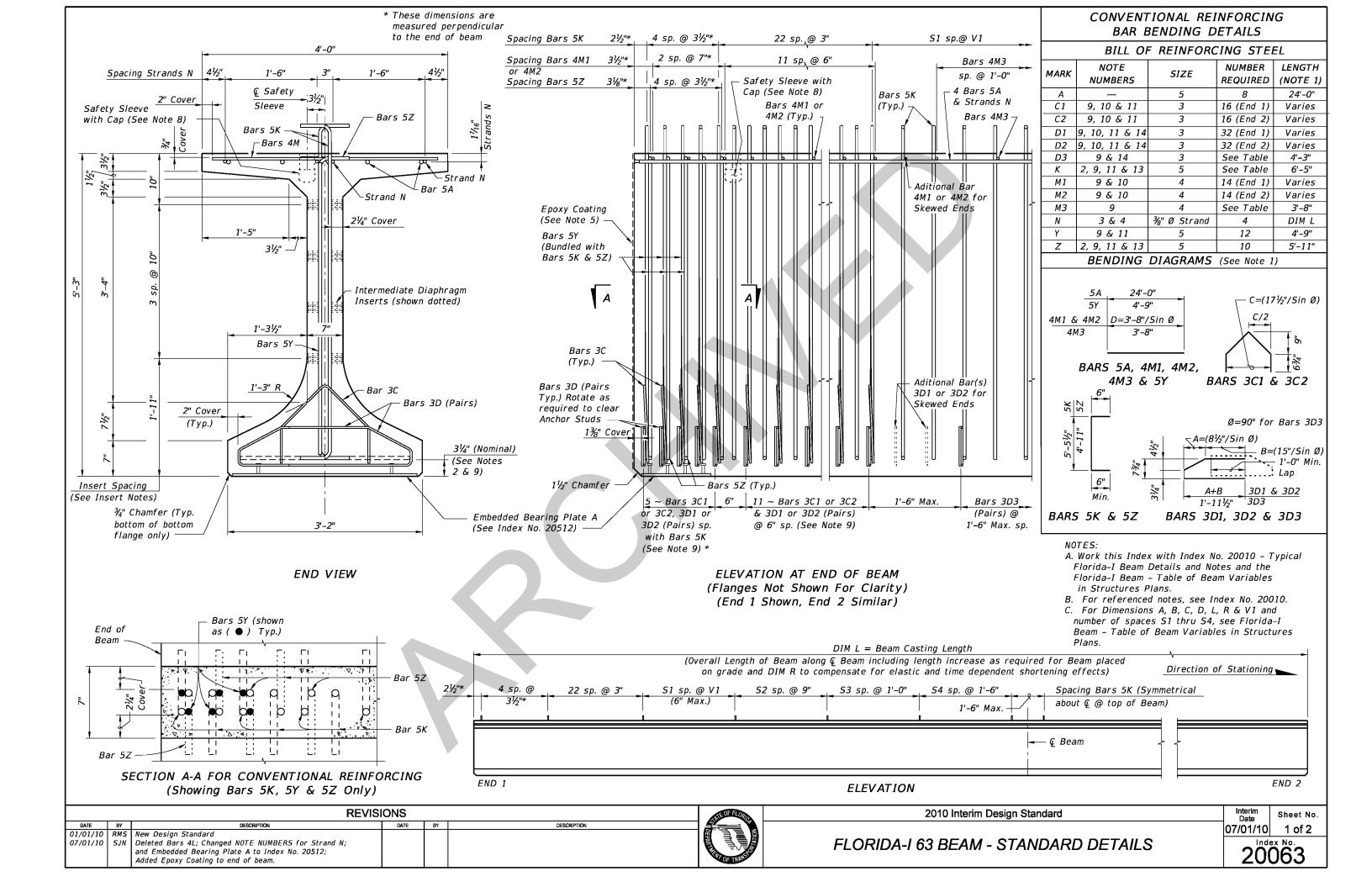


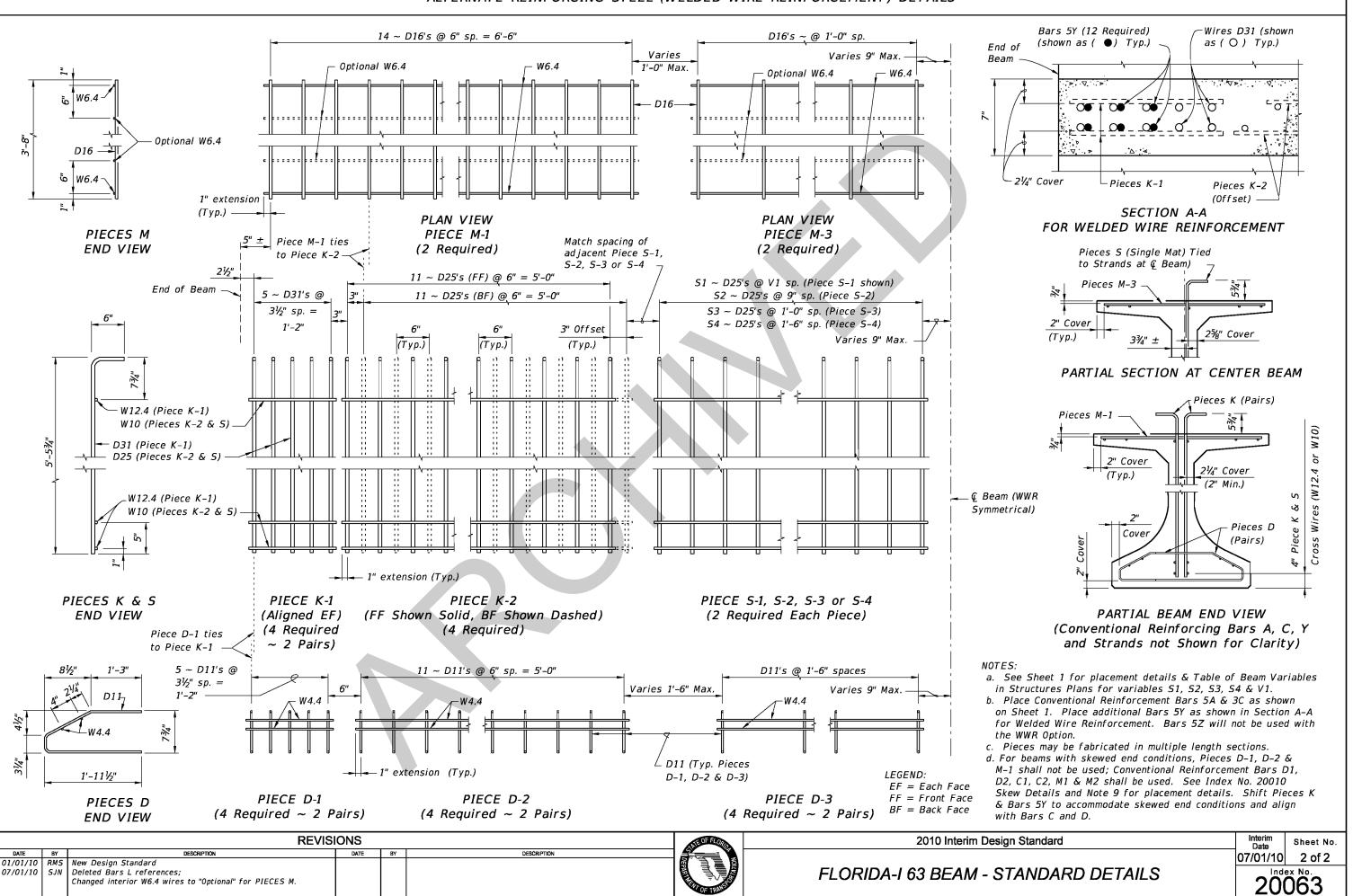


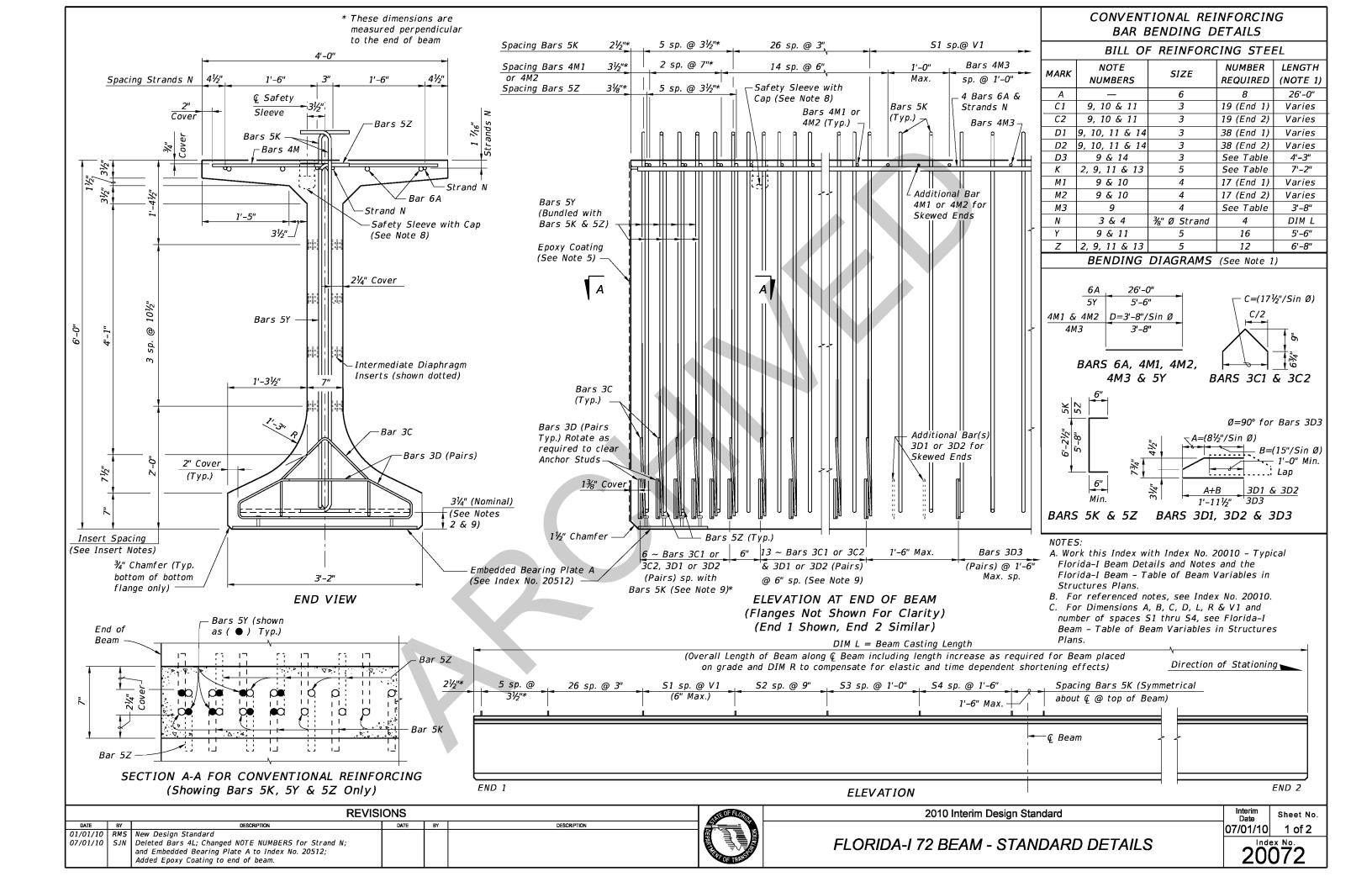


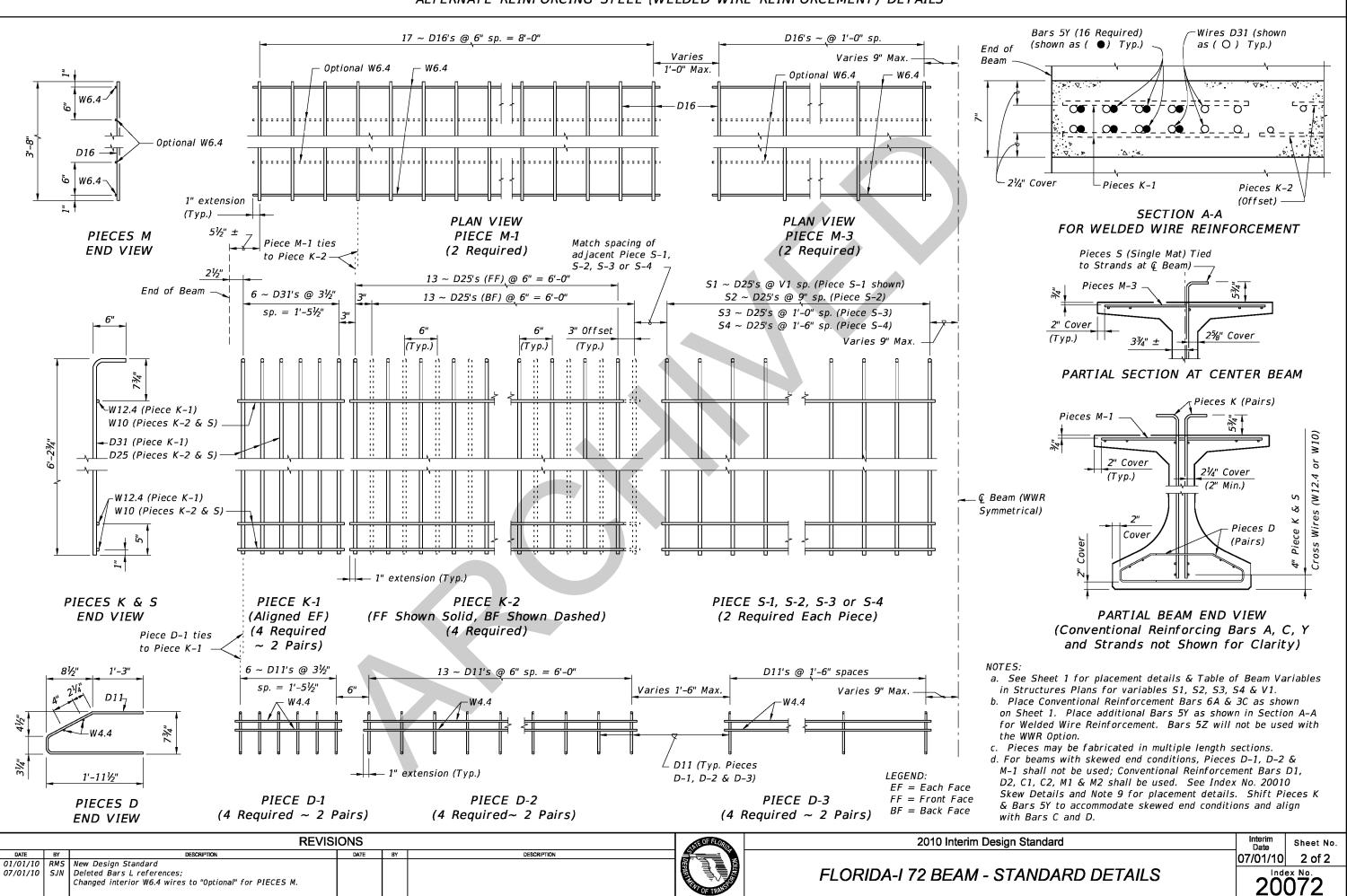


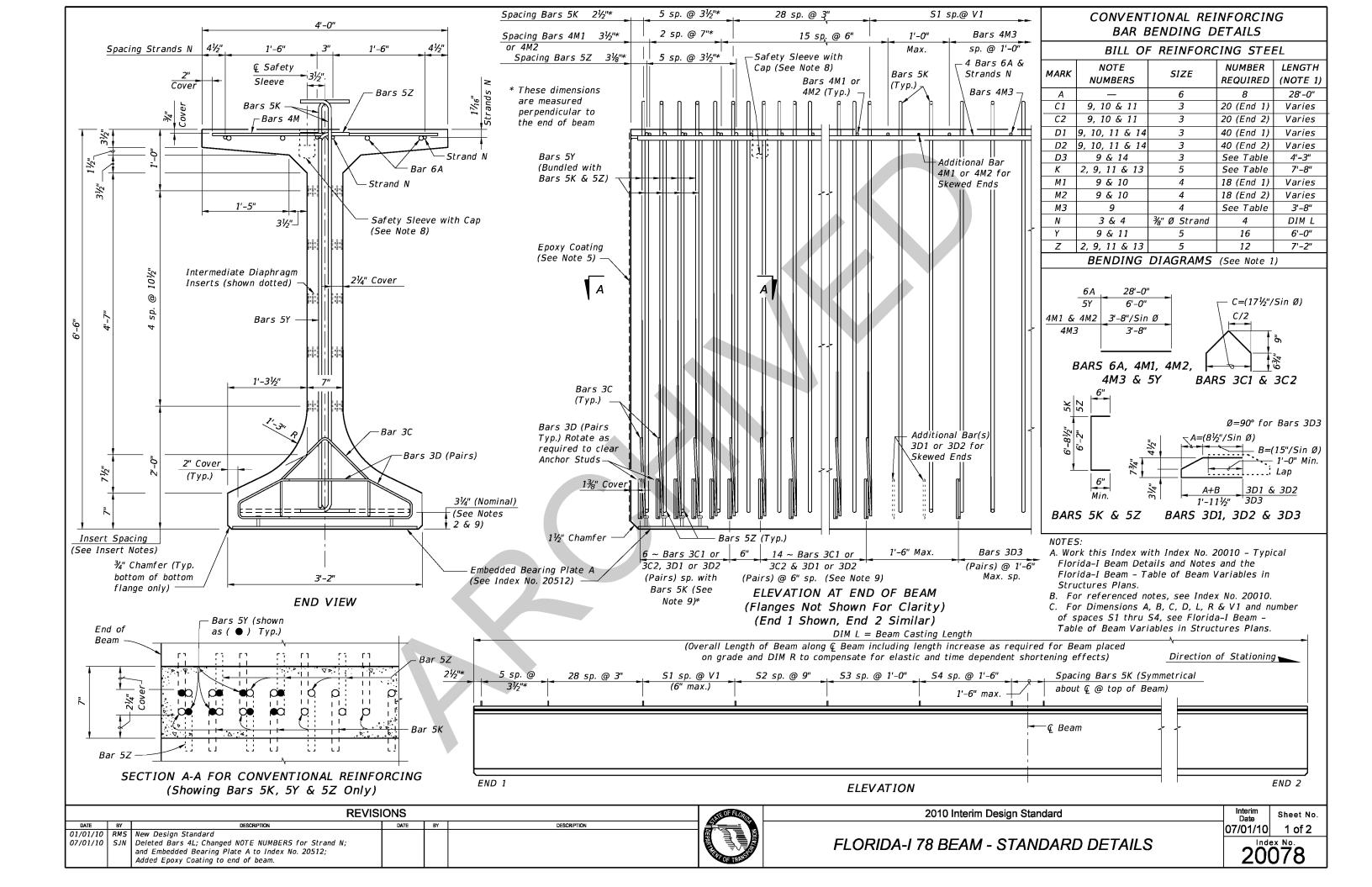


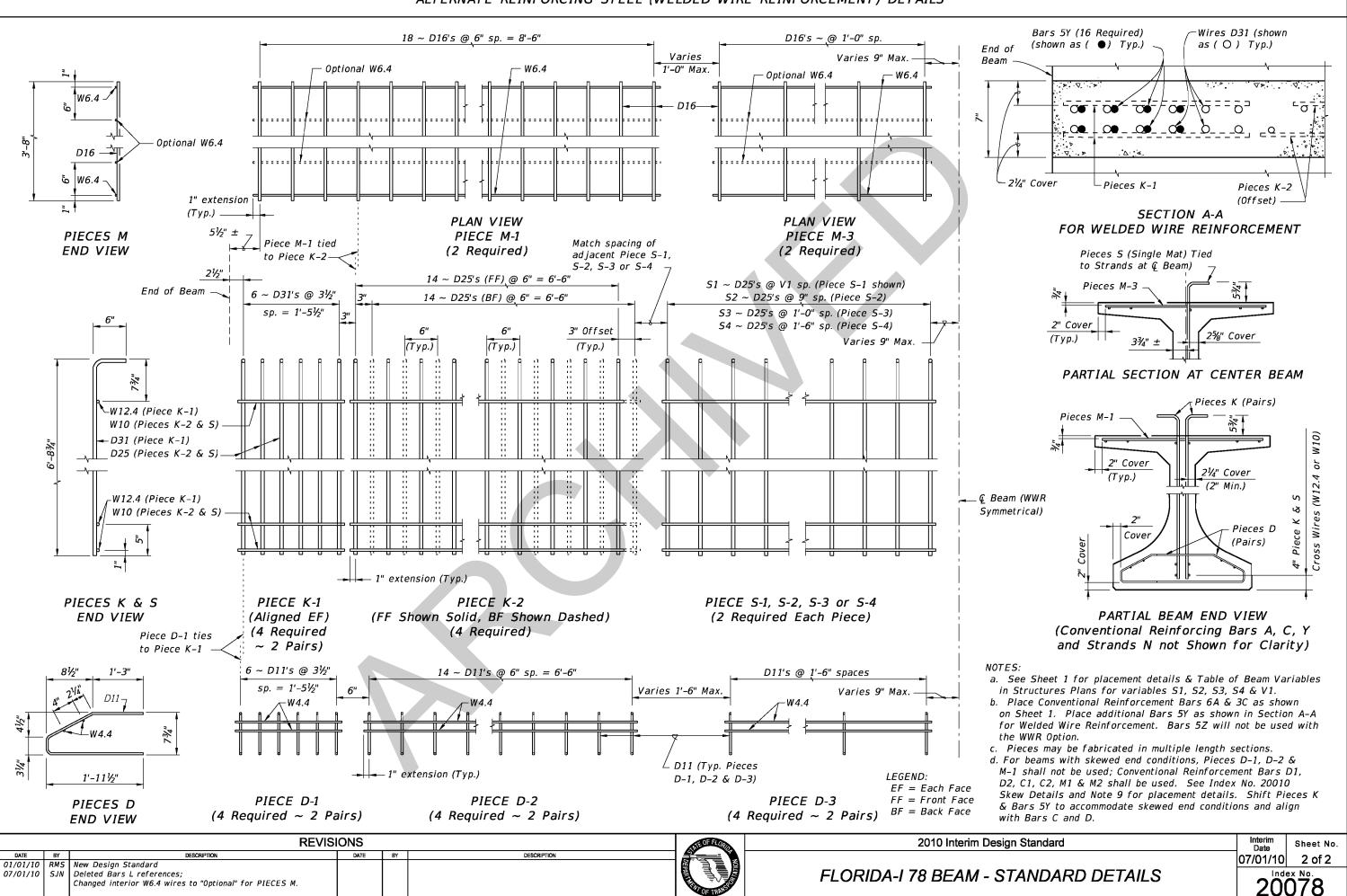


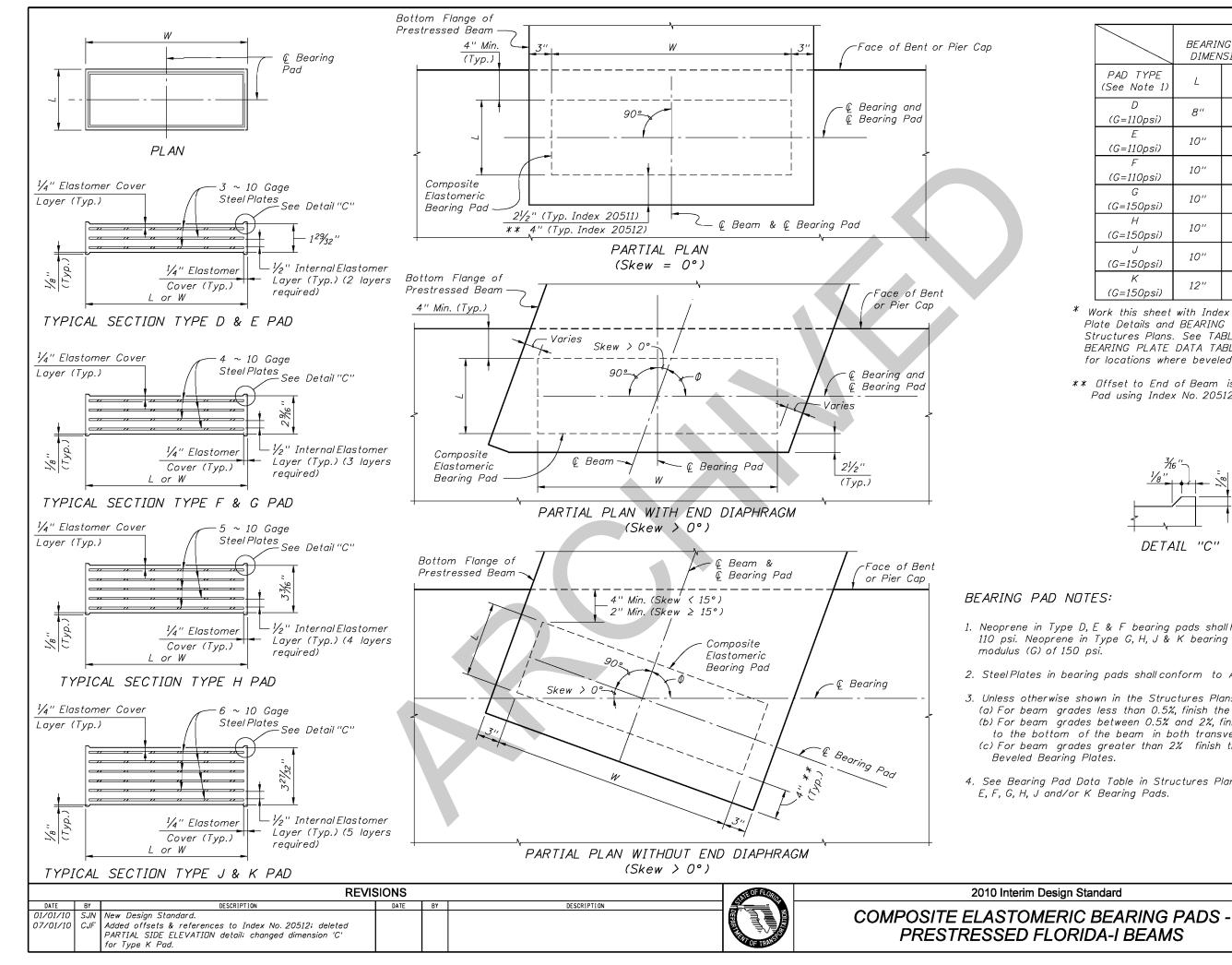








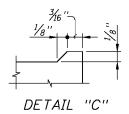




	BEARING PAD DIMENSIDNS		*BEVELED BEARING PLATE DIMENSIONS	
PAD TYPE (See Note 1)	L	W	С	D
D (G=110psi)	8''	32''	12''	36''
E (G=110psi)	10''	32''	12"	36"
F (G=110psi)	10''	32''	12"	36"
G (G=150psi)	10''	32''	12"	36"
H (G=150psi)	10''	32''	12''	36"
J (G=150psi)	10''	32''	12''	36"
K (G=150psi)	12"	32''	1 <i>3<sup>1</sup>/2</i> ''	36"

\* Work this sheet with Index No. 20511 or 20512 - Bearing Plate Details and BEARING PAD DATA TABLE in the Structures Plans. See TABLE OF BEAM VARIABLES and BEARING PLATE DATA TABLE in the Structures Plans for locations where beveled bearing plates are required.

\*\* Offset to End of Beam is reduced to 2" for Type K Pad using Index No. 20512.



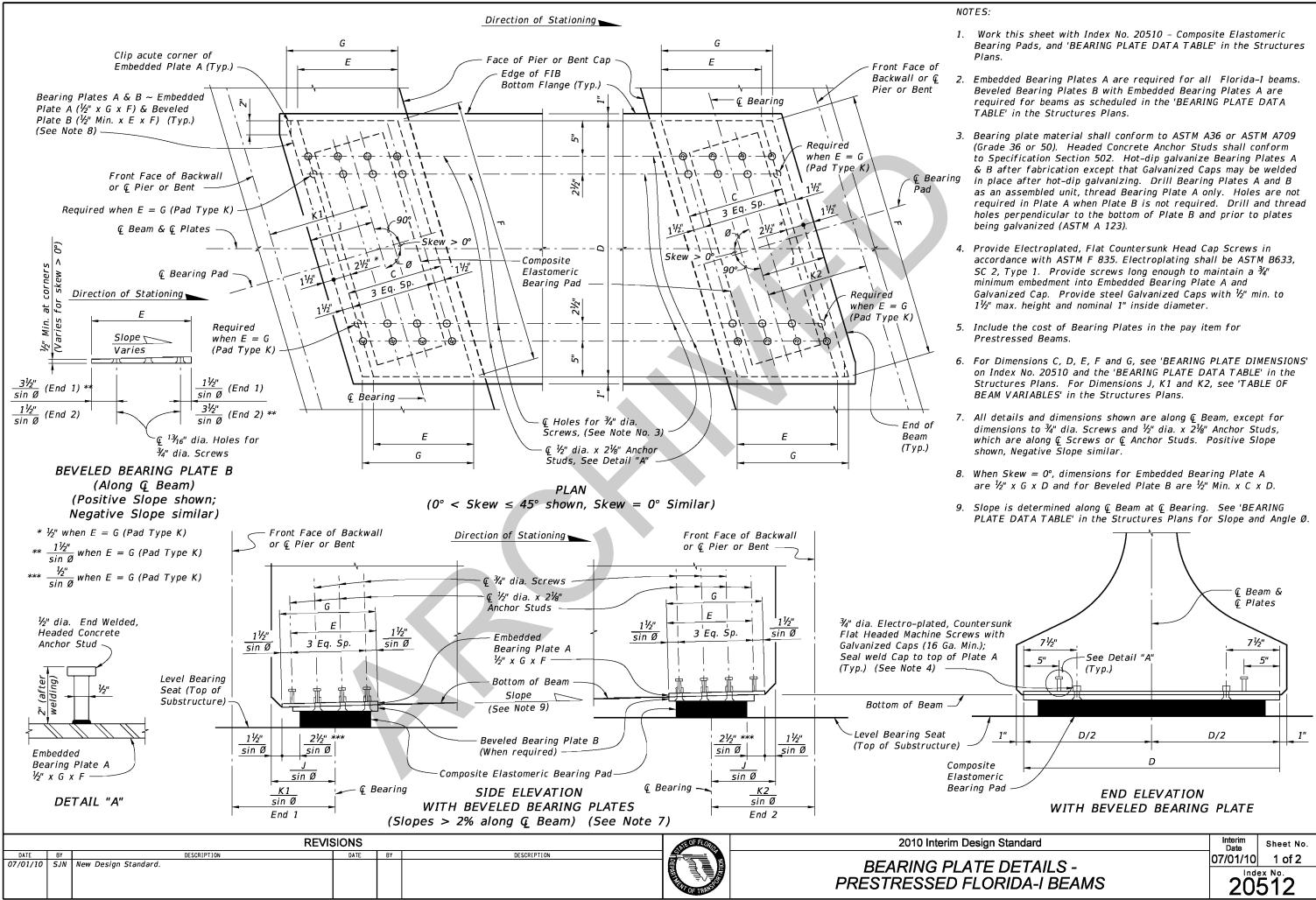
1. Neoprene in Type D, E & F bearing pads shall have a shear modulus (G) of 110 psi. Neoprene in Type G, H, J & K bearing pads shall have a shear

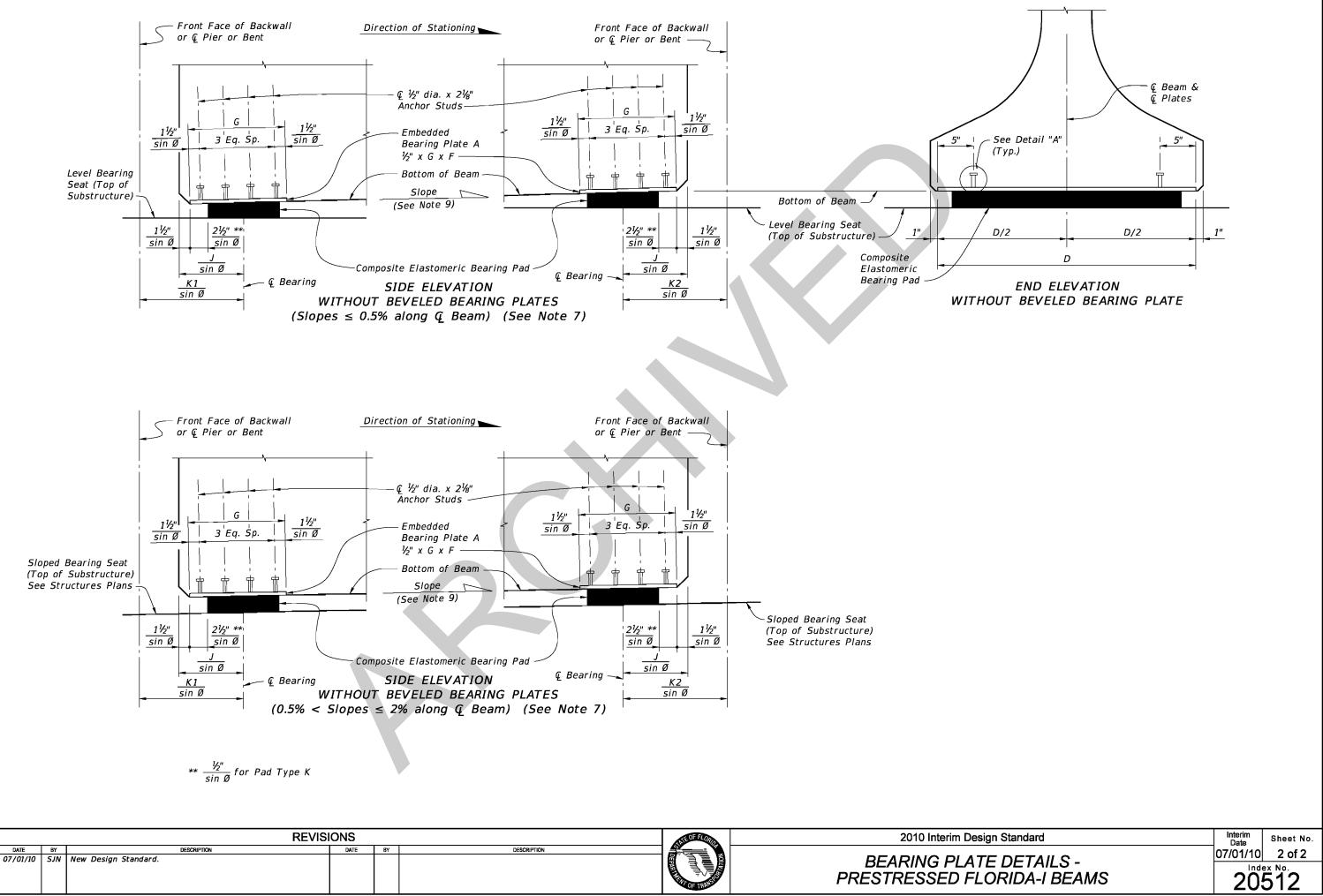
2. Steel Plates in bearing pads shall conform to ASTM A1011 Grade 36, Type 1.

3. Unless otherwise shown in the Structures Plans: (a) For beam grades less than 0.5%, finish the Beam Seat level. (b) For beam grades between 0.5% and 2%, finish the Beam Seat parallel to the bottom of the beam in both transverse and longitudinal directions. (c) For beam grades greater than 2% finish the Beam Seat level and provide

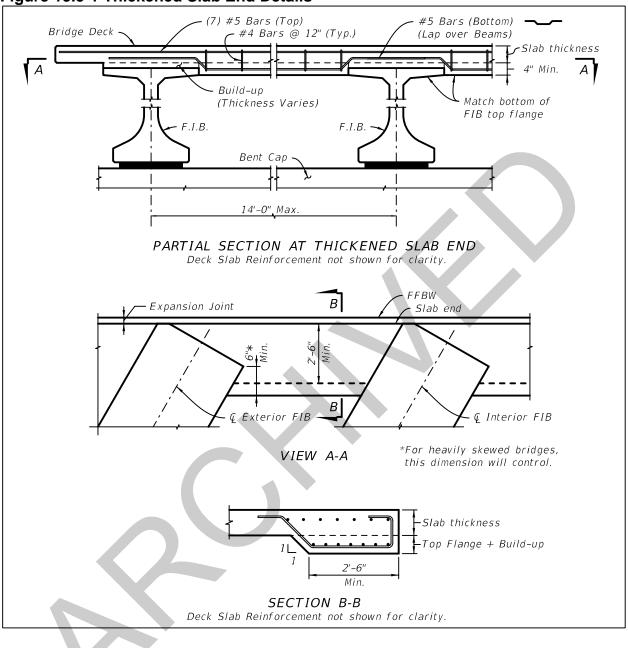
4. See Bearing Pad Data Table in Structures Plans for quantities of Type D, E, F, G, H, J and/or K Bearing Pads.



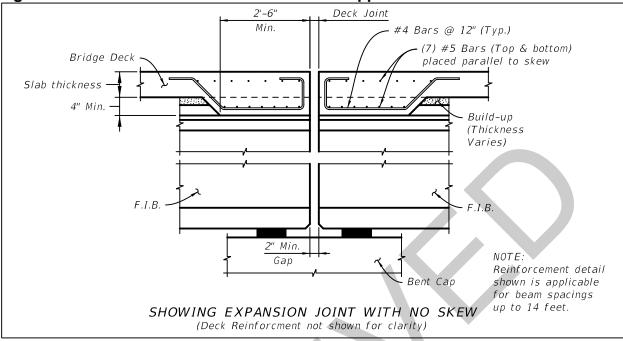




ATTACHMENT B



### Figure 15.5-1 Thickened Slab End Details



## Figure 15.5-2 Thickened Slab End at Interior Support

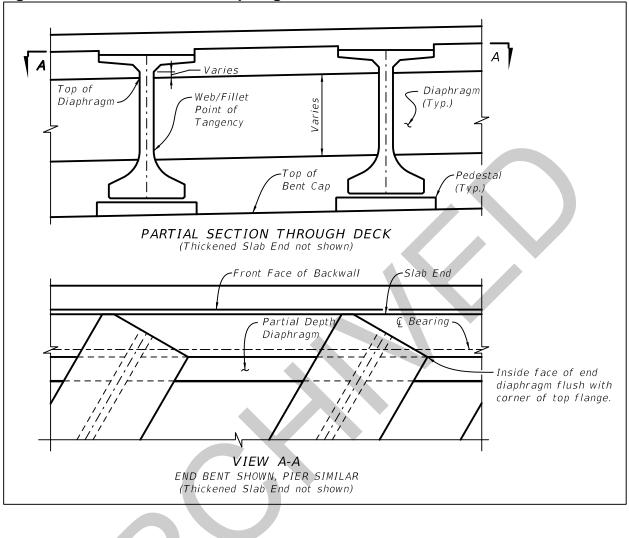


Figure 15.8-1 Concrete End Diaphragm Details

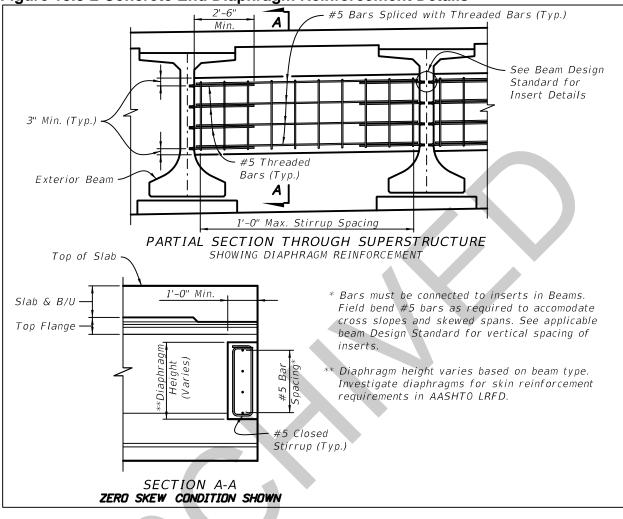


Figure 15.8-2 Concrete End Diaphragm Reinforcement Details

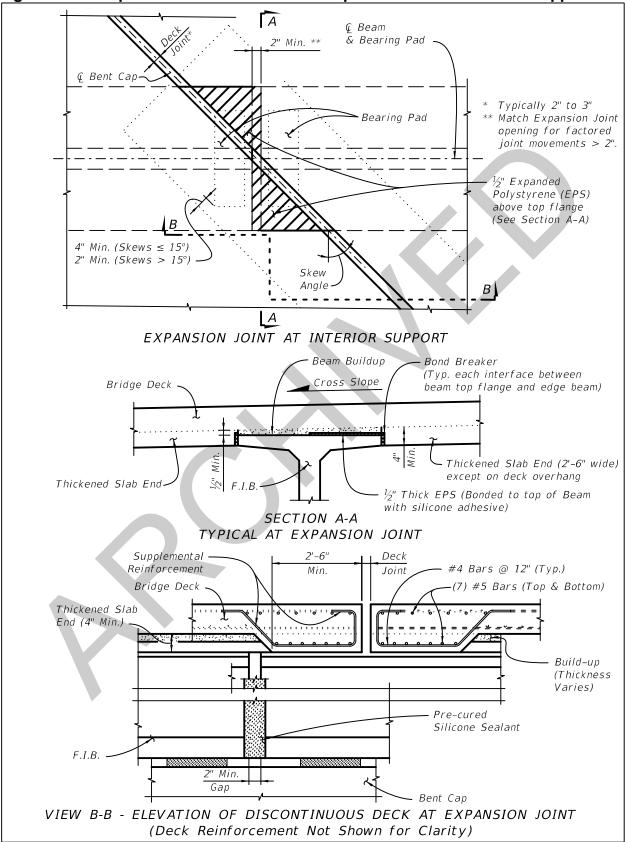


Figure 15.8-4 Squared Beam End Details – Expansion Joint at Interior Support

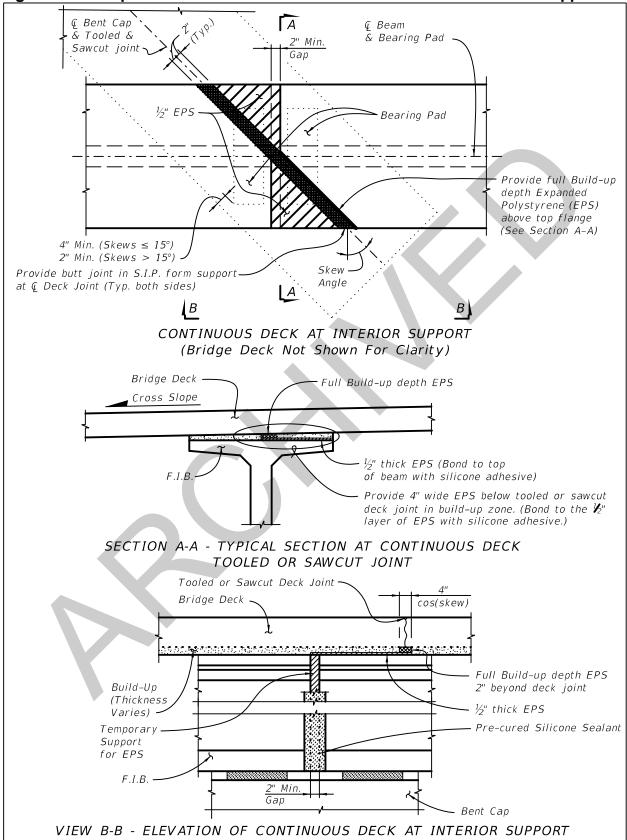


Figure 15.8-5 Squared Beam End Details – Continuous Deck at Interior Support

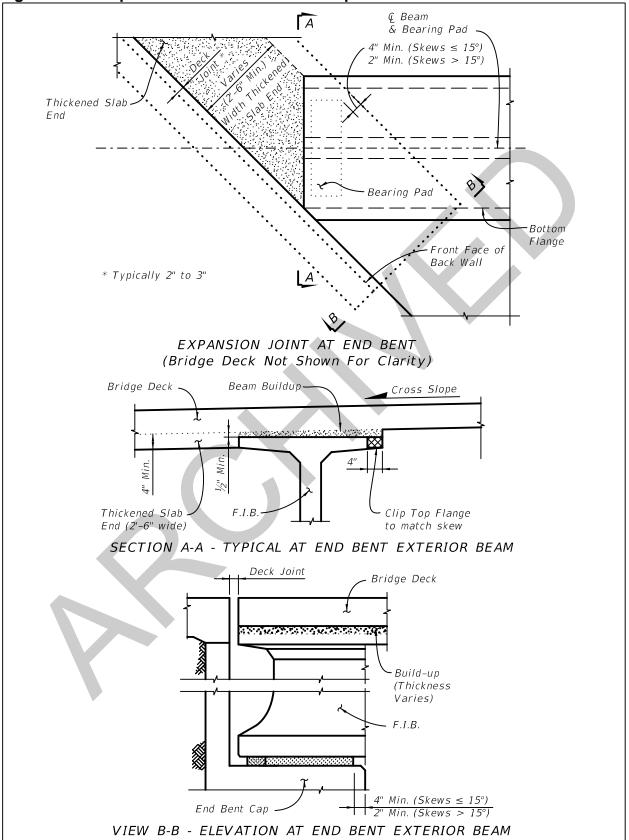


Figure 15.8-6 Squared Beam End Details – Expansion Joint at End Bent

ATTACHMENT C

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# Index 20010 Series Prestressed Florida-I Beams (Rev. 07/10)

## **Design Criteria**

AASHTO LRFD Bridge Design Specifications, 4th Edition; Structures Detailing Manual (SDM); Structures Design Guidelines (SDG)

## **Design Assumptions and Limitations**

Index 20010 is the lead standard for the Prestressed Florida-I Beam standard series which includes Indexes 20010 through 20096. Use this standard with Indexes 20005, 20036, 20045, 20054, 20063, 20072, 20078, 20084, 20096, 20199, 20510 and 20511.

These standards must be supplemented with project specific information including a Table of Beam Variables, Strand Pattern Details and a Strand Debonding Legend which must be completed and included in the Structures Plans. These standards and the supplemental project specific information that is included in the plans provide sufficient information to permit beam fabrication without the submittal of shop drawings.

Data tables for associated Indexes 20005, 20199, 20510 and 20511 must also be completed and included in the plans.

A Framing Plan is required for bridges meeting the criteria stated in the SDM.

The use of End Diaphragms is not preferred on simple span, pretensioned, Florida-I Beam structures. In lieu of End Diaphragms, the preferred detail is a Thickened Slab End at all locations of slab discontinuity. Where End Diaphragms are required by design or for widening projects, partial depth diaphragms are preferred. See *Structures Design Bulletin C10-05* for suggested details.

Except for widening projects where special details may be required, squared beam ends are preferred on all Florida-I Beam structures.

The prestressed beams in these Standard Drawings are generally assumed to act as simple spans under both Dead Load and Live Load even where the deck is detailed to be continuous across the intermediate supports or back-to-back diaphragms are present. For detailing purposes, Prestressed Florida-I Beams are assumed to be erected plumb.

When the total initial tensioning force of the fully bonded strands required by design exceeds the values shown below, shield additional strands at the end of the beam when possible. The end reinforcement may only be redesigned to accommodate an increased vertical splitting force when approved by the State Structures Design Office. If approval is granted, Index 20010 and the appropriate Standard Detail Drawings must then be modified for inclusion in the contract documents and signed and sealed by the EOR.

To limit vertical splitting forces in the webs of beams, the maximum prestress force at the beam ends from fully bonded strands must be limited to the following:

Index No.	Beam Type	Max. Bonded Prestress Force	Last Revision Date
20036	Florida-I 36	1450 Kips	07/01/09
20045	Florida-I 45	1670 Kips	07/01/09
20054	Florida-I 54	1740 Kips	07/01/09
20063	Florida-I 63	1740 Kips	07/01/09
20072	Florida-I 72	1980 Kips	07/01/09
20078	Florida-I 78	2230 Kips	07/01/09
20084	Florida-I 84	2375 Kips	07/01/10
20096	Florida-I 96	2375 Kips	07/01/10

Do not apply losses when calculating the Bonded Prestress Force.

Embedded Bearing Plates are required for all beams. If the beam grade exceeds 2%, provide Beveled Bearing Plates at each end of the beam as shown in Index 20511.

Prestressed Beam Suppliers typically utilize side forms for casting which are not easily or economically modified. If modifications to beam cross-sections are required for any reason other than haunched sections, maintain profile dimensions of the form. For example: To thicken the web, increase the spacing between side forms. To increase the beam height, increase the thickness of the top flange. In any case, do not reduce the standard thickness of either the top or bottom flange.

See additional instructions in the SDG.

## **Plan Content Requirements**

In the Structures Plans:

Complete the following "FLORIDA-I BEAM - TABLE OF BEAM VARIABLES" and include it in the plans. Use additional sheets when the actual number of beams or strand patterns exceeds the capacity of a single plan sheet using the standard table. Supplemental details and modifications are permitted if special conditions require dimensions, details or notes. However, the "FLORIDA-I BEAM - TABLE OF BEAM VARIABLES" itself should not be modified. See Introduction I.3 for more information regarding use of Data Tables.

Report elastic and time dependent shortening effects (DIM R) at mid-height of the beam @ 120 days. The average of the calculated values for the top and bottom of the beam may be used.

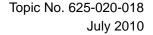
Show strands in the outermost positions of the two lowest rows to support Bars D.

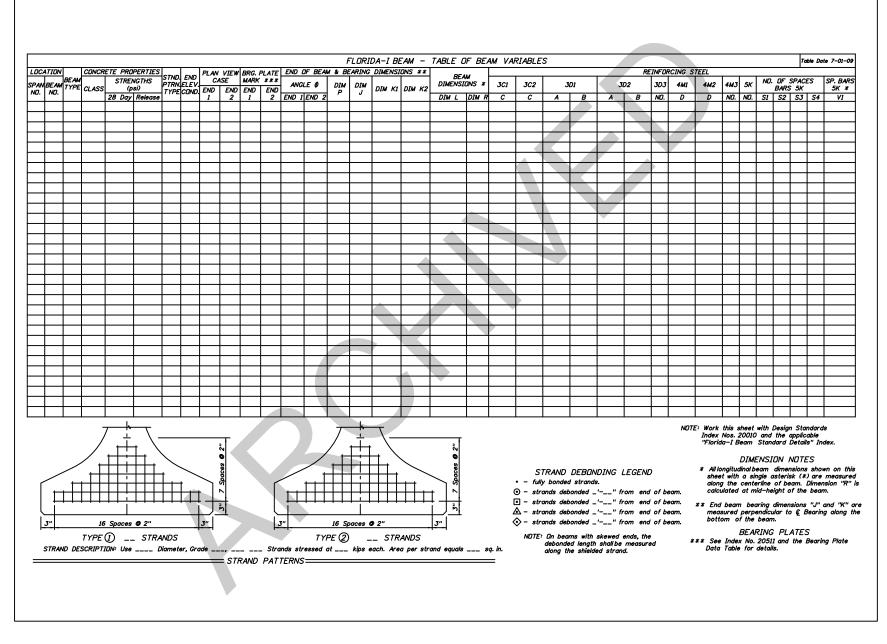
Round Angle  $\Phi$  up to the nearest degree.

Specify shear stirrup spacing V1 for Bars 5K to the nearest inch.

Prepare a Framing Plan for bridges meeting the criteria stated in the **SDM**.

When diaphragms are required by design, show them on the Framing Plan. Tabulate insert locations with respect to the beam ends and beam faces. Include length adjustments for beams placed on grade and for elastic and time dependent shortening effects. See *Structures Design Bulletin C10-05* for diaphragm and reinforcing details.





## Payment

Item number	Item description	Unit Measure
450-2-AAA	Prestressed Beams: Florida-IBeam	LF

## Example Problem

The following example shows the data required for completion of a Florida-I Beam Table of Beam Variables. The example assumes a three span bridge with Florida-I 45 Beams designed for the following conditions:

Live Load: HL-93

No intermediate Diaphragms

Stay-in-Place Metal Forms:

Allowance of 20 PSF non-composite dead load over the projected plan area of the forms (this includes the unit weight of metal forms and the concrete required to fill the form flutes).

Environment (Superstructure): Moderately Aggressive

Bridge Characteristics:

Length: 276 ft. Width: 51'-1" (out-to-out) Clear Roadway: 48 ft.

Superstructure:

Three simple spans of prestressed concrete beams with 8-inch composite deck slab (plus <sup>1</sup>/<sub>2</sub>" sacrificial deck thickness)

Span: 87'-0", 102'-0", 87'-0"

Sidewalk: None

Horizontal Alignment: Straight

Vertical Alignment: 0.00% Grade

Skew Angle: 15 degrees (Right)

Beam Design:

Beam: Florida-I 45 Beam

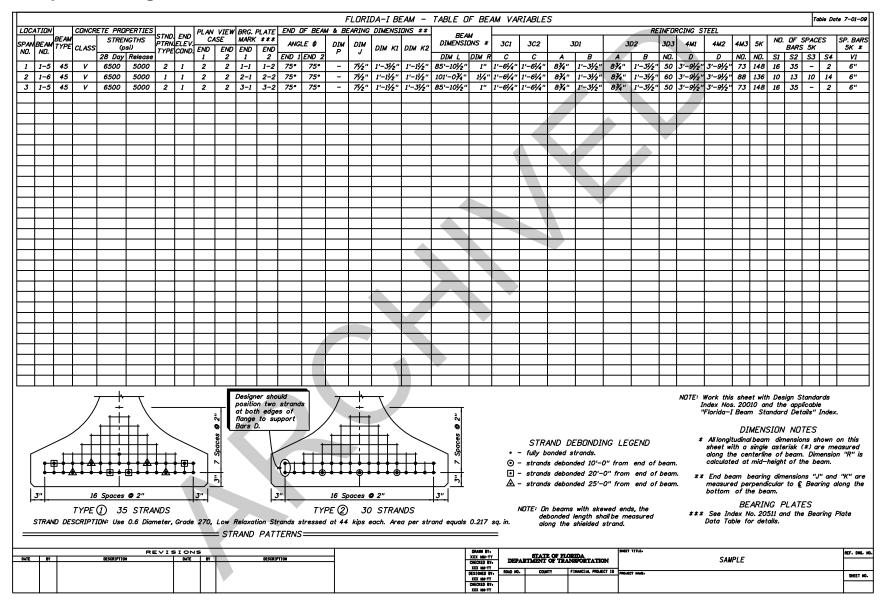
Spacing:

11'-3", 87' Span (5 Beams) 9'-0", 102' Span (6 Beams)

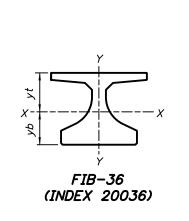
Design Span Length:

84'-6" (Spans 1 & 3) 99'-8" (Span 2)

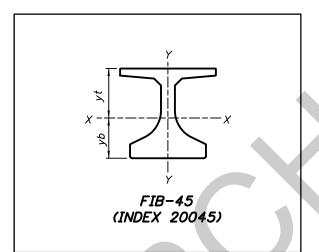
## **Sample Drawing**



# **Design Aids**



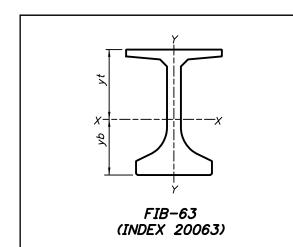
FIB-36 SECTION PROPERTIES		
Area (in. <sup>2</sup> )	806.58	
Perimeter (in.)	206.57	
Ixx (in. <sup>4</sup> )	127,545	
lyy (in. <sup>4</sup> )	81,070	
yt (in.)	19.51	
yb (in.)	16.49	



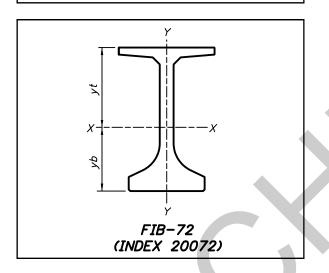
FIB- (INDEX 2	

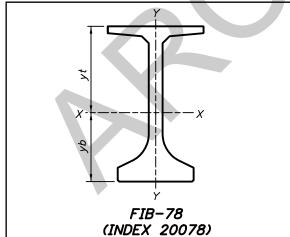
FIB-45 SECTION PROPERTIES			
Area (in. <sup>2</sup> )	869.58		
Perimeter (in.)	224.57		
Ixx (in. <sup>4</sup> )	226,581		
lyy (in. <sup>4</sup> )	81,327		
yt (in.)	24.79		
yb (in.)	20.21		

FIB-54 SECTION PROPERTIES		
Area (in. <sup>2</sup> )	932.58	
Perimeter (in.)	242.57	
Ixx (in. <sup>4</sup> )	359,929	
lyy (in. <sup>4</sup> )	81,584	
yt (in.)	29.96	
yb (in.)	24.04	



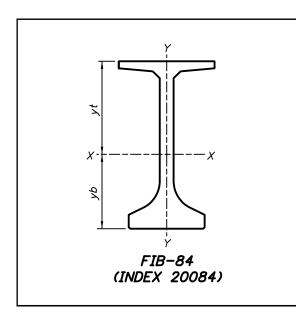
FIB-63 SECTION PROPERTIES		
Area (in. <sup>2</sup> )	995.58	
Perimeter (in.)	260.57	
Ixx (in. <sup>4</sup> )	530,313	
lyy (in. <sup>4</sup> )	81,842	
yt (in.)	35.04	
yb (in.)	27.96	



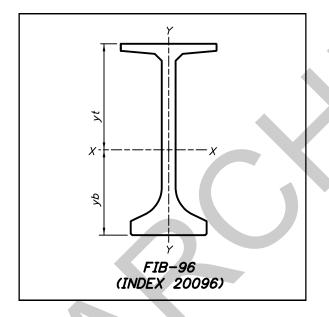


FIB-72 SECTION PROPERTIES		
Area (in. <sup>2</sup> )	1,058.58	
Perimeter (in.)	278.57	
Ixx (in. <sup>4</sup> )	740,416	
lyy (in. <sup>4</sup> )	82,099	
yt (in.)	40.06	
yb (in.)	31.94	

FIB-78 SECTION PROPERTIES		
Area (in. <sup>2</sup> )	1,100.58	
Perimeter (in.)	290.57	
Ixx (in. <sup>4</sup> )	903,861	
lyy (in. <sup>4</sup> )	82,270	
yt (in.)	43.37	
yb (in.)	34.63	



FIB-84 SECTION PROPERTIES		
Area (in. <sup>2</sup> )	1,142.58	
Perimeter (in.)	302.57	
Ixx (in. <sup>4</sup> )	1.087 x 10 <sup>6</sup>	
Tyy (in. <sup>4</sup> )	82,442	
yt (in.)	46.66	
yb (in.)	37.34	



FIB-96 SECTION PROPERTIES		
Area (in. <sup>2</sup> )	1,226.58	
Perimeter (in.)	326.57	
Ixx (in. <sup>4</sup> )	1.515 x 10 <sup>6</sup>	
lyy (in. <sup>4</sup> )	82,785	
yt (in.)	53.18	
yb (in.)	42.82	

# Index 20512 Bearing Plate Details Prestressed Florida-I Beams (Rev. 07/10)

## **Design Criteria**

AASHTO LRFD Bridge Design Specifications, 4th Edition; Structures Design Guidelines (SDG)

## **Design Assumptions and Limitations**

This Design Standard has been developed as a more economical option than Index 20511 and may be used at the designer's discretion.

This standard contains generic details and notes for beveled and embedded bearing plates for prestressed concrete Florida-I Beams with or without skewed end conditions.

Use this standard with Indexes 20010, 20036, 20045, 20054, 20063, 20072, 20078, 20084, 20096 and 20510.

Embedded Bearing Plates A are required for all Florida-I Beams. Embedded Bearing Plates A and Beveled Bearing Plates B are required for beams on grades greater than 2%.

## Plan Content Requirements

In the Structures Plans:

Bearing seats (pedestals) may be finished level for beam grades less than 0.5%. Use Embedded Bearing Plates A but do not use Beveled Bearing Plates B.

For beam grades between 0.5% and 2%, show the bearing seats (pedestals) to be finished parallel to the beam grade with no allowance for beam camber or deflection. Use Embedded Bearing Plates A but do not use Beveled Bearing Plates B.

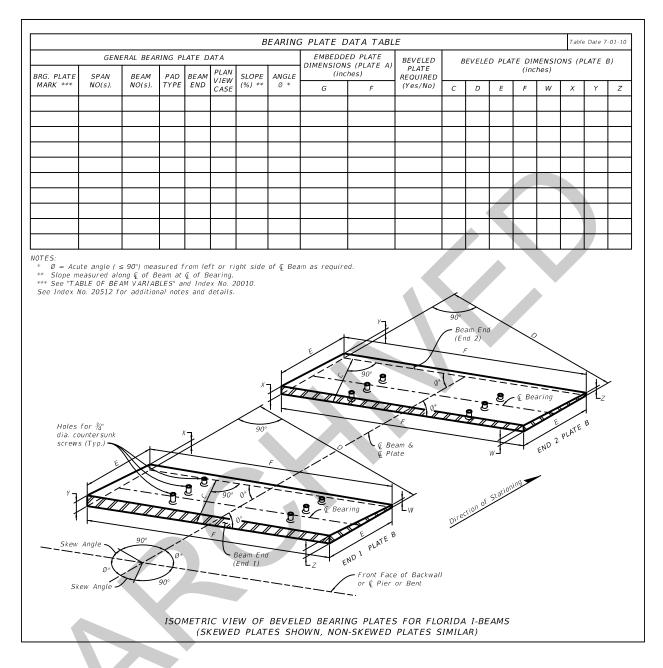
For beam grades greater than 2%, show the bearing seats (pedestals) to be finished level and use Bearing Plates A and B.

See also instructions for Index 20510.

Complete the following "BEARING PLATE DATA TABLE" and include it in the plans. Fill in the table to correspond with data on the "FLORIDA-I BEAM TABLE OF BEAM VARIABLES" using inch units for Beveled Plate dimensions 'W', 'X', 'Y' & 'Z' rounded to 1/16th of an inch. If Beveled Bearing Plates B are not required, fill in the corresponding columns with "N/A". See Introduction I.3 for more information regarding use of Data Tables.

Use the following equations to determine the Beveled Bearing Plate B thicknesses for "PLAN VIEW CASES" and "END ELEVATION CONDITIONS" corresponding to those shown on Index 20010. The Slope parameter in these equations requires decimal units and correct sign convention:

END 1	END 2		
(I) PLAN VIEW CASE 1:			
(a) END ELEVATION CONDITION 1 or 2 (F	(a) END ELEVATION CONDITION 1 or 2 (Positive Slope)		
$W = X = 0.5" + (C) \times Slope$	W = X = 0.5"		
Y = Z = 0.5"	$Y = Z = 0.5" + (C) \times Slope$		
(b) END ELEVATION CONDITION 1 or 3 (1	Negative Slope)		
W = X = 0.5"	W = X = 0.5" - (C) x Slope		
Y = Z = 0.5" - (C) x Slope	Y = Z = 0.5"		
(II) PLAN VIEW CASE 2:			
(a) END ELEVATION CONDITION 1 or 2 (Positive Slope)			
W = 0.5" + (C / sin $\Phi$ + D / tan $\Phi$ ) x Slope	W = 0.5" + (D / tan $\Phi$ ) x Slope		
$X = 0.5" + (C / \sin \Phi) \times Slope$	X = 0.5"		
Y = 0.5"	$Y = 0.5" + (C / \sin \Phi) \times Slope$		
$Z = 0.5" + (D / \tan \Phi) \times Slope$	$Z = 0.5" + (C / \sin \Phi + D / \tan \Phi) \times Slope$		
(b) END ELEVATION CONDITION 1 or 3 (I	Negative Slope)		
W = 0.5"	$W = 0.5$ " - (C / sin $\Phi$ ) x Slope		
X = 0.5" - (D / tan Φ) x Slope	X = 0.5" - (C / sin $\Phi$ + D / tan $\Phi$ ) x Slope		
Y = 0.5" - (C / sin $\Phi$ + D / tan $\Phi$ ) x Slope	Y = 0.5" - (D / tan Φ) x Slope		
Z = 0.5" - (C / sin Φ) x Slope	Z = 0.5"		
(III) PLAN VIEW CASE 3:			
(a) END ELEVATION CONDITION 1 or 2 (F	Positive Slope)		
$W = 0.5"+ (C / \sin \Phi) \times Slope$	W = 0.5"		
$X = 0.5" + (C / \sin \Phi + D / \tan \Phi) \times Slope$	$X = 0.5" + (D / \tan \Phi) \times Slope$		
$Y = 0.5" + (D / \tan \Phi) \times Slope$	$Y = 0.5" + (C / \sin \Phi + D / \tan \Phi) \times Slope$		
Z = 0.5"	Z = 0.5" + (C / sin Φ) x Slope		
(b) END ELEVATION CONDITION 1 or 3 (Negative Slope)			
W = 0.5" - (D / tan Φ) x Slope	W = 0.5" - (C / sin $\Phi$ + D / tan $\Phi$ ) x Slope		
X = 0.5"	X = 0.5" - (C / sin Φ) x Slope		
Y = 0.5" - (C / sin Φ) x Slope	Y = 0.5"		
Z = 0.5" - (C / sin $\Phi$ + D / tan $\Phi$ ) x Slope	$Z = 0.5$ " - (D / tan $\Phi$ ) x Slope		



## Payment

The cost of beveled and embedded bearing plates is incidental to the cost of the prestressed beams they are used with. No separate payment is made.