

Florida Department of Transportation

CHARLIE CRIST GOVERNOR

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TEMPORARY DESIGN BULLETIN C09-03

DATE:

June 2, 2009

TO:

District Directors of Production, District Design Engineers, District Structures

Design Engineers, District Construction Engineers

FROM:

Robert Robertson, P. F., State Structures Design Engineer

COPIES:

Lora Hollingsworth, Brian Blanchard, Ghulam Mujtaba, Tom Malerk, Jeffrey

Ger (FHWA)

SUBJECT:

Implementation of New Florida-I Beam Design Standards Including Related

Data Tables and Structures Manual Revisions

REQUIREMENTS

1. Design Standards

The Florida-I Beam and related Design Standards Index Sheets will be released for implementation with the July 2009 Interim Design Standards. Copies of these sheets and their associated data tables are included with Attachments 'A' & 'B' as listed below.

Attachment 'A', Florida-I Beam and Related Design Standards:

- Index No. 20010 (2 Sheets): Typical Florida-I Beam Details and Notes
- Index No. 20036 (2 Sheets): Florida-I 36 Beam Standard Details
- Index No. 20045 (2 Sheets): Florida-I 45 Beam Standard Details
- Index No. 20054 (2 Sheets): Florida-I 54 Beam Standard Details
- Index No. 20063 (2 Sheets): Florida-I 63 Beam Standard Details
- Index No. 20072 (2 Sheets): Florida-I 72 Beam Standard Details
- Index No. 20078 (2 Sheets): Florida-I 78 Beam Standard Details
- Index No. 20199 (1 Sheet): Build-Up and Deflection Data
- Index No. 20510 (1 Sheet): Composite Elastomeric Bearing Pads for Florida-I Beams
- Index No. 20511 (2 Sheets): Bearing Plate Details for Florida-I Beams

Attachment 'B', Florida-I Beam Related Data Tables (CADD Cells):

- Cell No. 20010: Florida-I Beam Table of Beam Variables
- Cell No. 20199: Build-up & Deflection Data Table
- Cell No. 20510: Bearing Pad Data Table (Florida-I Beam)
- Cell No. 20511: Bearing Plate Data Table (Florida-I Beam)

2. Structures Manual – January 2009

- a. Volume 1 Structures Design Guidelines
 - i. Replace Section 2.3.1A with the following:

"The majority of Florida bridges will be exempt from seismic or restrainer design requirements. For exempted bridges, only the minimum bearing support dimensions need to be satisfied as required by LRFD [4.7.4.4]. Exempted bridges include those with superstructures comprising simple-span or continuous flat slabs, simple-span prestressed slabs or double-tees, and simple-span AASHTO, Florida Bulb-T, Florida-I, or steel girders."

ii. In Section 2.5, insert the following into Table 2.1 under Prestressed Beams:

Florida-I 36 Beam (Index No. 20036)	Lb/ft	840
Florida-I 45 Beam (Index No. 20045)	Lb/ft	906
Florida-I 54 Beam (Index No. 20054)	Lb/ft	971
Florida-I 63 Beam (Index No. 20063)	Lb/ft	1037
Florida-I 72 Beam (Index No. 20072)	Lb/ft	1103
Florida-I 78 Beam (Index No. 20078)	Lb/ft	1146

iii. Replace the text of Section 4.1.3 – Girder Transportation with the following:

"Coordinate the transportation of heavy and/or long girders with the Department's Permit Office and the appropriate industry representatives during the design phase of the project."

Commentary: Longer beams may require evaluation of delivery routes by the appropriate industry representative to ensure turns can be made safely, particularly in urban areas."

iv. Renumber Sections 4.3.1A through 4.3.1F to Sections 4.3.1B through 4.3.1G respectively. Insert the following as the new Section 4.3.1A:

"The Florida-I Beams are the Department's standard prestressed concrete beams and will be used in the design of all new bridges and bridge widenings as applicable.

AASHTO Beams and Florida Bulb-T Beams will not be used in new designs."

v. Replace item 1 of renumbered Section 4.3.1E with the following:

"Strand patterns utilizing an odd number of strands per row (a strand located on the centerline of beam) and a minimum side cover (centerline of strand to face of concrete) of 3-inches are required for all Florida-I, AASHTO, and Bulb-T beam sections except AASHTO Type V and VI beams for which a strand pattern with an even number of strands per row must be utilized."

vi. Replace item 8 of renumbered Section 4.3.1E with the following:

"For wide-top beams such as Florida-I, Bulb-T, and AASHTO Types V & VI beams, evaluate the top flanges of those beams to safely and adequately support the self-weight of the forms, concrete, and construction load specified in Section 400 of the FDOT Standard Specifications for Road and Bridge Construction.

For the Florida-I Beam, the Standard top flange reinforcing allows for a beam spacing up to 14 feet with an 8½" deck."

vii. Replace renumbered Section 4.3.1F with the following:

"The maximum prestressing force (P_u) from fully bonded strands at the ends of prestressed beams must be limited to the values shown on the Standard Drawings. For non-standard single web prestressed beam designs, modify the requirements of LRFD 5.10.10.1 to provide vertical reinforcement in the ends of pretensioned beams with the following splitting resistance:

- 3% P_u from the end of the beam to h/8, but not less than 10";
- 5% P_u from the end of the beam to h/4, but not less than 10";
- 6% P_u from the end of the beam to 3h/8, but not less than 10".

Do not apply losses to the calculated prestressing force (P_u) . The minimum length of debonding from the ends of the beams is half the depth of the beam (h/2). Do not modify the reinforcing in the ends of the beams shown in the Standard Drawings without the approval of the State Structures Design Office.

Commentary: To minimize horizontal and diagonal web cracks and compensate for the longer splitting force distribution length adopted by LRFD in 2002 (h/4), the maximum splitting force from bonded prestressing has been increased. An additional splitting zone from h/4 to 3h/8 has been added to control the length of potential cracks, consistent with previous standard FDOT designs."

viii. Replace renumbered Section 4.3.1.G with the following:

"Provide embedded bearing plates for all AASHTO & Florida Bulb-T beams with beam sections deeper than 60 inches. Provide embedded bearing plates for all Florida-I beams. For all beam designs where the beam grade exceeds 2%, include beveled bearing plates."

ix. Replace the heading of Section 4.3.3 with the following:

"Florida Bulb-T Beams and Florida-I Beams [5.14.1.2.2] The minimum web thicknesses for Florida-I and Florida Bulb-T beams are:"

x. Insert the following girder costs into Section 9.2.2.B.2 (Prestressed Concrete Girders; cost per linear foot.):

Florida-I; 36	\$190
Florida-I; 45	\$205
Florida-I; 54	\$220
Florida-I; 63	\$235
Florida-I; 72	\$250
Florida-I; 78	\$260

xi. Insert the following debris quantity estimations into Section 9.4 (Component; CY/LF):

36" Florida-I	0.207
45" Florida-I	0.224
54" Florida-I	0.240
63" Florida-I	0.256
72" Florida-I	0.272
78" Florida-I	0.283

- b. Volume 2 *Detailing Manual*
 - i. Replace item 2AA of Section 3.5A with the following:
 - "Bulb-T / Florida-I Beam Superstructure"
 - ii. Replace Section 13.11A with the following:

"See Design Standards Index Nos. 20500 (Bearing Pads - AASHTO & Florida Bulb-T Beams), 20510 (Bearing Pads – Florida-I Beams), 20501 (Bearing Plates - AASHTO & Florida Bulb-T Beams), 20502 (Bearing Plates - Florida U-Beams), and 20511 (Bearing Plates – Florida-I Beams). See *Volume 3, Instructions for Design Standards* for example drawings and general instructions."

c. Volume 3 – Examples, Details & Instructions

Add the following Instructions for Design Standards shown in Attachment 'C':

- Index 20000 Series (1 Sheet): Prestressed Florida-I Beam Instructions
- Index 20510 (1 Sheet): Composite Elastomeric Bearing Pad Instructions for Florida-I Beams
- d. Volume 7 Design Aids

Add the following Design Aids as shown in Attachment 'D':

- 'Florida-I Beam Section Properties' (1 Sheet)
- 'Florida-I Beam Estimated Maximum Span Lengths' charts (2 Sheets)

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COMMENTARY

This Temporary Design Bulletin (TDB) is a follow-up to TDB C09-01 released in January 2009. This TDB implements Florida-I Beam sizes 36" through 78" depth. Potential beams of deeper size will be addressed in the future.

HISTORY

See Temporary Design Bulletin C09-01.

IMPLEMENTATION

Florida I-Beams (FIB's) will be used on all new Design-Bid-Build projects having both a design start date of February 1, 2009 or later and a letting date of July 1, 2010 or later. The FIB's shall be used for preliminary design and estimates of projects with projected schedules falling on or after these dates.

AASHTO Beams and Florida Bulb-T Beams will no longer be used in Design-Bid-Build projects where the design start date is scheduled on or after February 1, 2009 with a letting date on or after July 1, 2010. Bridge Development Reports (BDR's) for these projects shall not include AASHTO Beams and Florida Bulb-T Beams in cost comparisons.

No currently designed projects will require a redesign as a result of this TDB, but Districts may elect to introduce FIB's into current designs at their discretion. For projects where the BDR already recommends an AASHTO or Florida Bulb-T beam design, FIB's may be substituted into the final design without issuing a BDR addendum.

For all projects requiring the use of FIB's as stated above, Value Engineering Change Proposals (VECP's) to use AASHTO and Florida Bulb-T beams will not be accepted.

New BDR's shall continue to consider the use of all viable structure types including the possibility of steel box and/or I-girders. Current policies stated in the Plans Preparation Manual Vol. 1 Section 26.9 still apply.

FIB's may be used on Design-Build projects effective immediately.

Current policies regarding the shipping of large girders remain in effect for FIB's. Allowable size limits for beams are limited to project-specific transportation considerations. As stated in Structures Design Guidelines Section 4.1.3, the transportation of heavy and/or long girders requires coordination with the Department's Permit Office and the appropriate industry representative during the design phase of the project.

Since implementation is dependent on the design start date, there will be a period of time where lettings have some projects with the new FIB's while others use the old AASHTO Beams and Florida Bulb-T Beams. For this transition period, the Design Standards will continue to include both the new FIB shapes and the old beam shapes.

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Changes to specifications and procedures are summarized as follows:

1. Structures Manual

SDG Vol. 7 Design Aids – 'BDR Bridge Cost Estimate': FIB Estimated Costs per Liner Foot have been added to the spreadsheet.

All other updates are included in the Requirements of this Bulletin.

2. Design Standards

All updates are included in the Requirements of this Bulletin.

3. Standard Specifications

Section 450 – 'Precast Prestressed Concrete Construction': All references and updates regarding the FIB will be included in the FDOT January, 2010 Specifications Workbook.

4. Basis of Estimates

New Pay Items will be added to the FDOT Basis of Estimates Manual for lettings beginning January, 2010.

5. Plans Preparations Manual

No changes are anticipated at this time.

6. Misc. Design Tool Updates

- a. CADD: New FIB cells and tables in MicroStation & PDF format will be released with the July 2009 Interims and posted on the Structures Design website. These Cells are shown in Attachment 'B', and they will be included in the MicroStation Structures Menu with the next Maintenance Release.
- b. Design Software: The new FIB's are included in Version 3.0 of the FDOT LRFD Prestressed Beam Program already released. Proprietary software vendors have been contacted and given the new FIB section properties to be included for use in their design programs.

CONTACT

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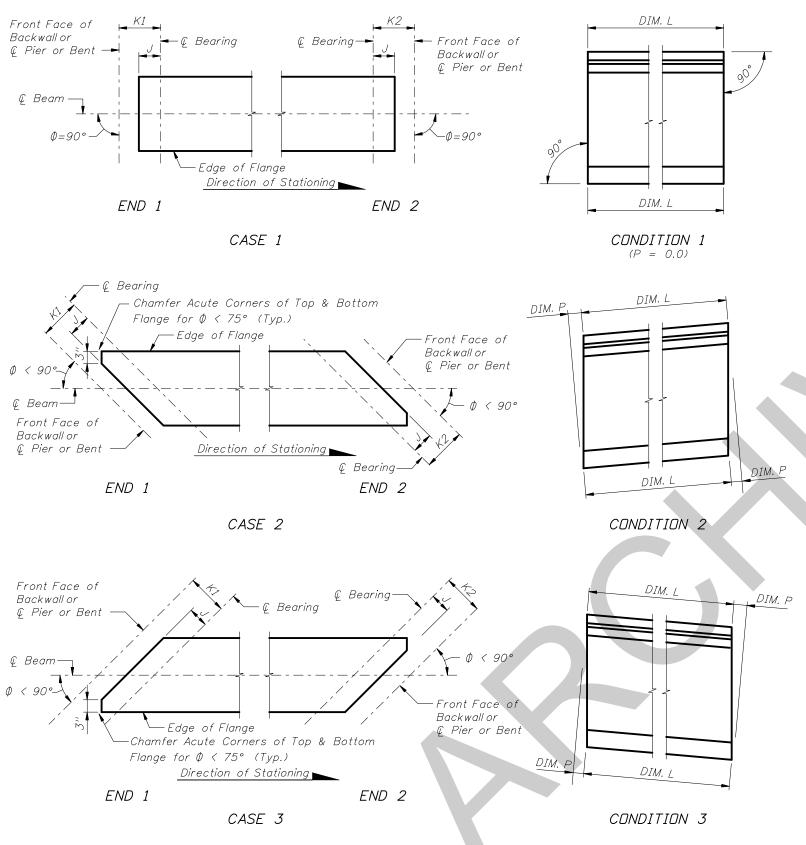
e-mail: sam.fallaha@dot.state.fl.us

RVR/rms Attachments

Attachment A

Florida-I Beam & Related Design Standards

- Index No. 20010 (2 Sheets): Typical Florida-I Beam Details and Notes
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BEAM NOTES

- 1. All bar dimensions are out-to-out.
- 2. Place one (1) Bar 5K or 5Z at each location as detailed alternating the direction of the ends for each bar (see "ELEVATION AT END OF BEAM", Index Nos. 20036, 20045, 20054, 20063, 20072 and 20078).
- 3. Bars 4L shall be bent prior to the beam leaving the prestressing yard. Bars 4L shall be bent parallel to the ends of the beams.
- 4. Caution should be used with Bars 4L in the ends of exterior beams to assure the bent portion of the bar is properly oriented so that the bar will be embedded in the diaphragm concrete.
- 5. Strands N shall be either ASTM A416, Grade 250 or Grade 270, seven-wire strands $\frac{3}{8}$ " \emptyset or larger, stressed to 10.000 lbs. each.
- 6. Unless otherwise noted, the minimum concrete cover for reinforcing steel shall be 2".
- 7. At the Contractors option, welded deformed wire reinforcement may be used in lieu of Bars 3D, 5K, 4M, and 5Z as shown on the Standard Details for each beam size. Welded deformed wire reinforcement shall conform to AASHTO M221, with a minimum yield strength of 75 ksi.
- 8. Install Safety Sleeves approximately 2'-0" from ends of beam and spaced on 8'-0" (Max.) centers. Safety Sleeves shall be $2^{1}/_{2}$ " NPS x 5" Sch. 40 PVC Pipe with Cap. Holes shall be free of debris and water prior to casting deck.
- 9. For beams with skewed end conditions, the end reinforcement, defined as Bars 3C1, 3C2, 3D1, 3D2, 5K, 4M1, 4M2, 5Y and 5Z placed within the limits of the spacing for Bars 3C in "ELEVATION AT END OF BEAM", shall be placed parallel to the skewed end of the beam. Bars 3D3, 5K and 4M3 located beyond the limits of Bars 3C shall be placed perpendicular to the longitudinal axis of the beam. Fan Bars as needed to avoid overlapping bars at the transition to Bars 3D3 and 4M3, and field cut to maintain minimum cover. Provide additional Bars 4M1, 4M2, 3D1 and 3D2 as required; additional bars are not included in the Number Required on the "BILL OF REINFORCING STEEL". For placement locations, see "SKEWED BEAM END DETAILS". Adjust the dimensions of Bars 3C1, 3C2, 3D1, 3D2, 4M1 and 4M2 as shown on the "BENDING DIAGRAM" for skewed end conditions.
- 10. Placement of Bars 3C1, 3D1 and 4M1 correspond to END 1, and Bars 3C2, 3D2 and 4M2 correspond to END 2. END 1 and END 2 are shown on the beam "ELEVATION".
- 11. For Beams with vertically beveled end conditions, place first row of Bars 3C1, 3C2, 3D1, 3D2, 5K, 5Y and 5Z parallel to the end of the beam. Progressively rotate remaining bars within the limits of Bars 5Z until vertical by adjusting the spacing at the top of beam up to a maximum of 1". For welded deformed wire reinforcement, cut top cross wire and rotate bars as required or reduce end cover at top of the beam to minimum 1".
- 12. For beams with skewed end conditions, welded deformed wire reinforcement shall not be used for end reinforcement (Bars 3D1, 3D2, 4M1 and 4M2) .
- 13. Bars 5K and 5Z shall be placed and tied to the fully bonded strands in the bottom or center row (see "STRAND PATTERN" on the Table of Beam Variables in Structures Plans). For welded deformed wire reinforcement, supplemental transverse #4 bars are permitted to support Pieces K & S under the cross wires on the bottom row of strands.
- 14. At the Contractor's option, Bars 3D1, 3D2 and 3D3 may be fabricated as a single bar with a 1'-0" minimum lap splice of the top leas.
- 15. For referenced Dimensions, Angles and Case Numbers, see the Table of Beam Variables in Structures Plans.

INSTRUCTIONS TO DESIGNER:

To limit vertical splitting forces in the webs of beams, the maximum prestress force at the beam ends from fully bonded strands must be limited to the following:

Beam Type	Max. Bonded Prestress Force	Index No.	Last Revision Date
Florida-I 36	1450 Kips	20036	07/01/09
Florida-I 45	1670 Kips	20045	07/01/09
Florida-I 54	1740 Kips	20054	07/01/09
Florida-I 63	1740 Kips	20063	07/01/09
Florida-I 72	1980 Kips	20072	07/01/09
Florida-I 78	2230 Kips	20078	07/01/09

No losses shall be applied when calculating the Bonded Prestress Force. The reinforcing in the ends of the beams must not be modified without the approval of the State Structures Design Engineer.

REVISIONS

DATE BY DESCRIPTION DATE BY DESCRIPTION

7/01/09 SJN New Design Standard

DESCRIPTION

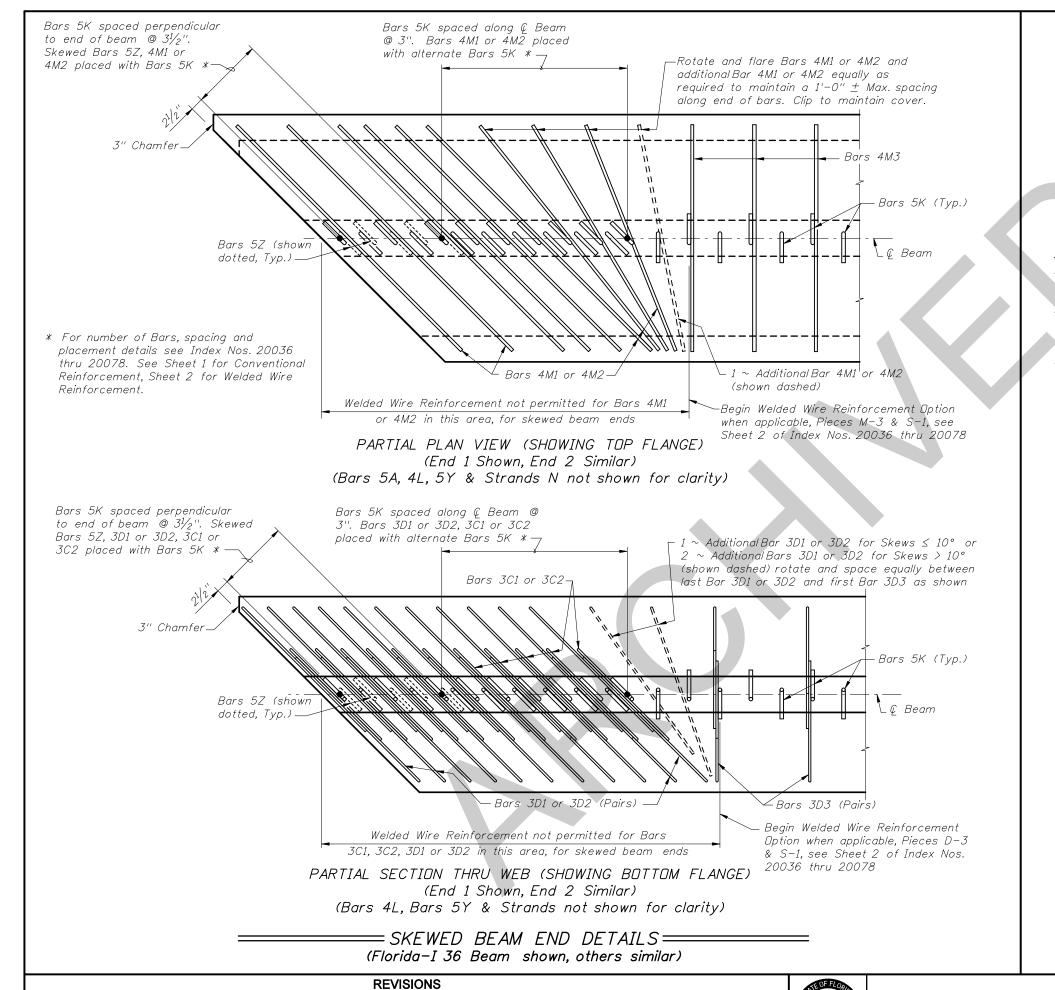
SCHEMATIC PLAN VIEWS AT BEAM ENDS



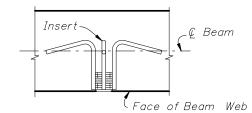
SCHEMATIC END ELEVATIONS OF BEAMS
(Showing Vertical Bevel of Beam End)

Sheet No.

1 of 2



07/01/09 SJN New Design Standard



PLAN SECTION THRU BEAM WEB AT INSERT FOR DIAPHRAGM REINFORCING

(When Intermediate Diaphragms are Required by Design)

INSERT NOTES

- 1. Provide 1" \emptyset , zinc-electroplated, ferrule wing nut or coil inserts, UNC threads, 1/0 minimum gage wire, not more than 4" in depth with a minimum ultimate tensile strength of 11,400 lbs. in 4,000 p.s.i. concrete.
- 2. If inserts are needed on both sides (faces) of beam webs, an assembly as long as the thickness of the beam web, consisting of two (2) ferrule or coil inserts attached by two (2) or more struts may be utilized. The connecting struts shall have a minimum ultimate tensile strength of 11,400 lbs.
- 3. Inserts for diaphragm reinforcing are required at each end of each intermediate diaphragm shown on the Beam Framing Plan. See Superstructure and Beam Framing Plans for longitudinal location of inserts for each face of beam.

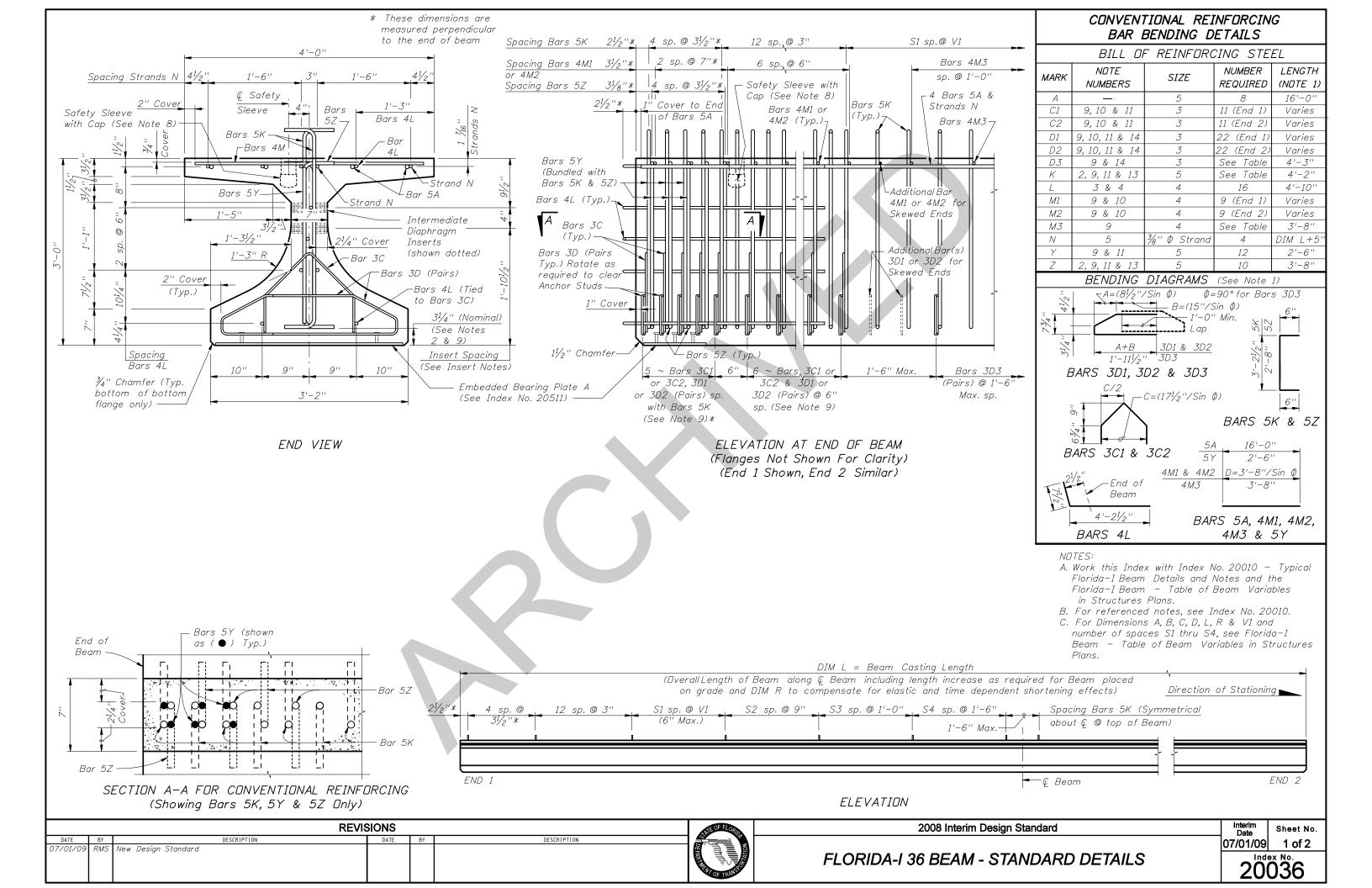
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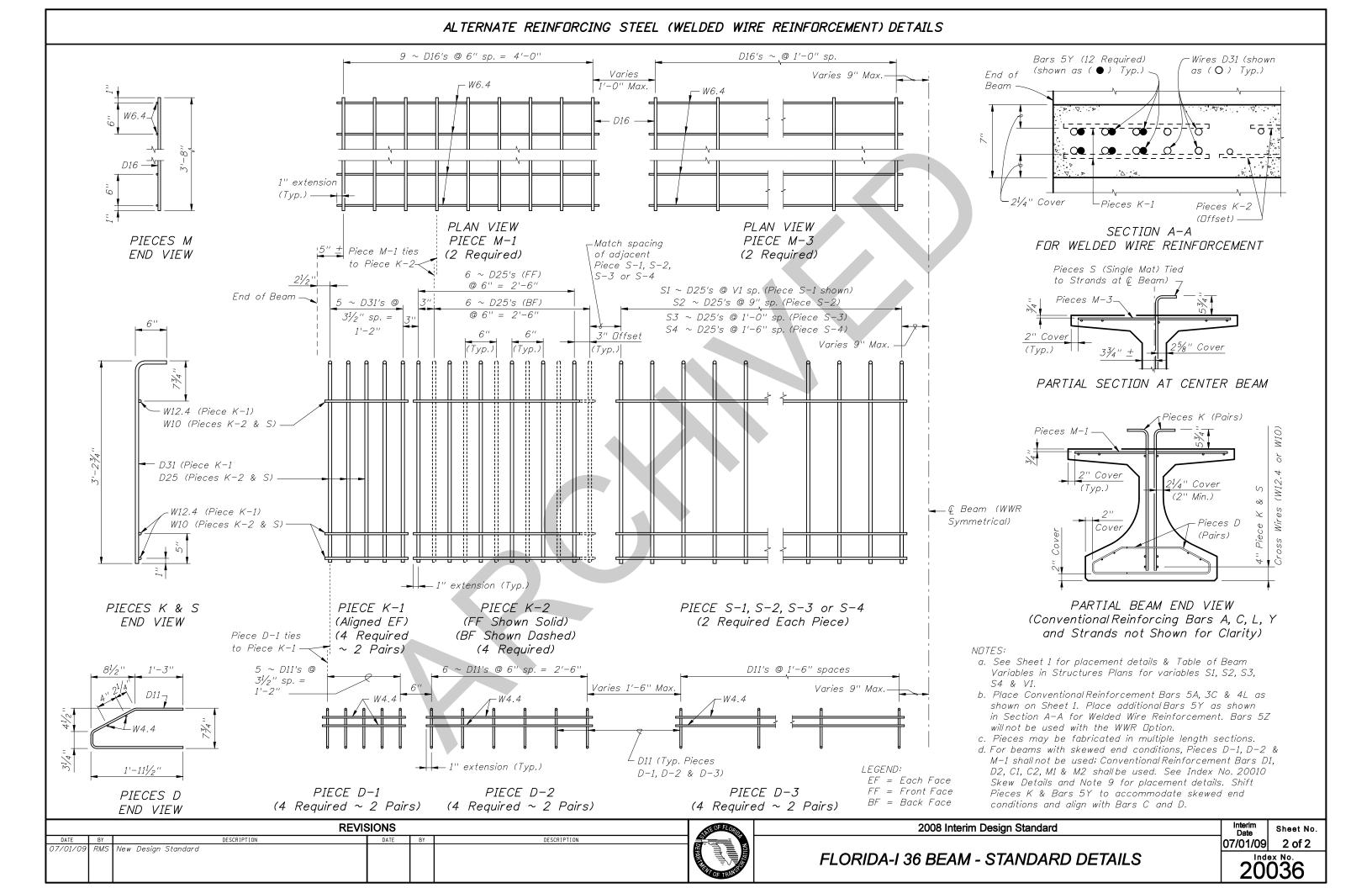
2008 Interim Design Standard

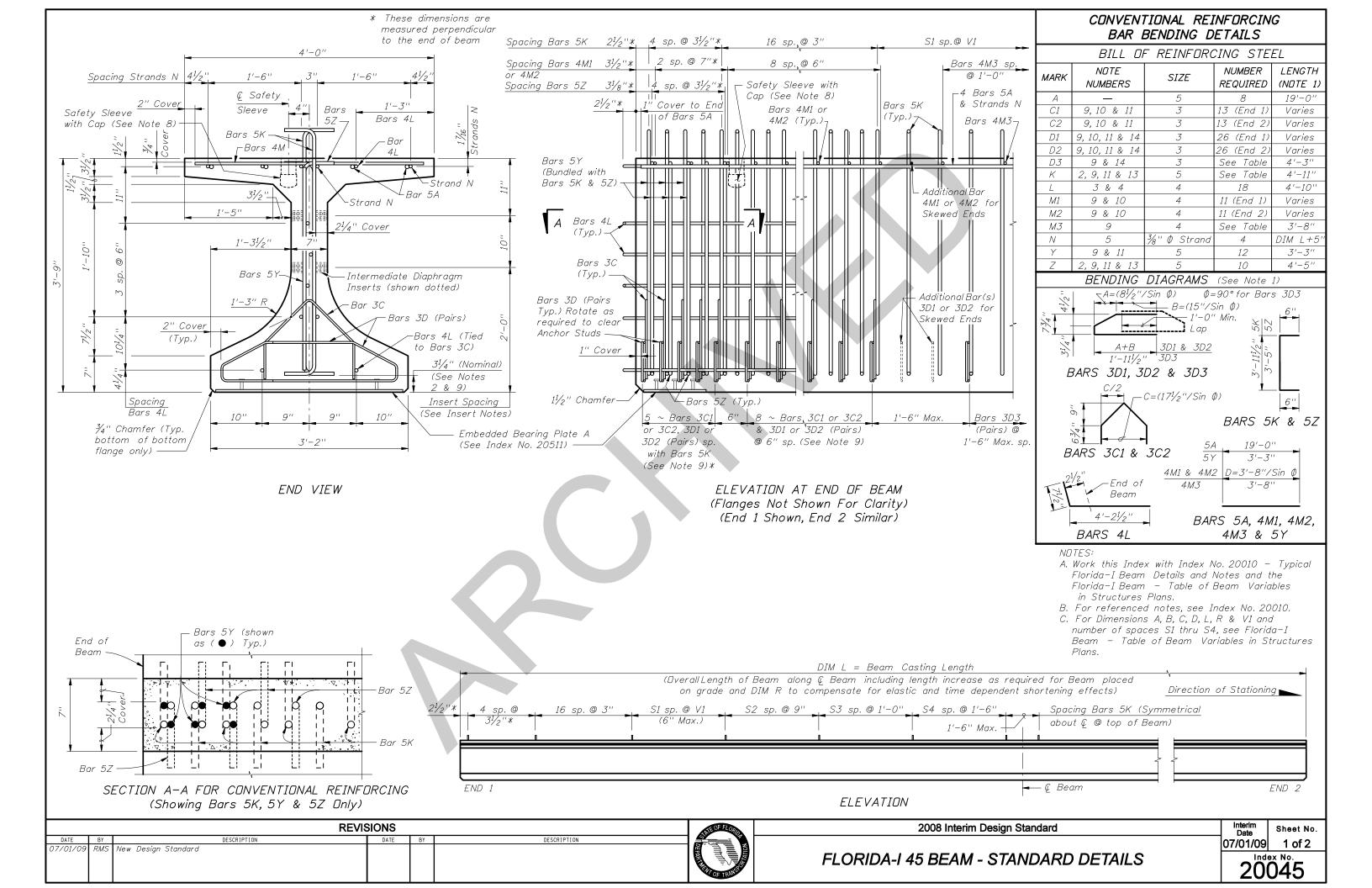
07/01/09 2 of 2

TYPICAL FLORIDA-I BEAM **DETAILS AND NOTES**

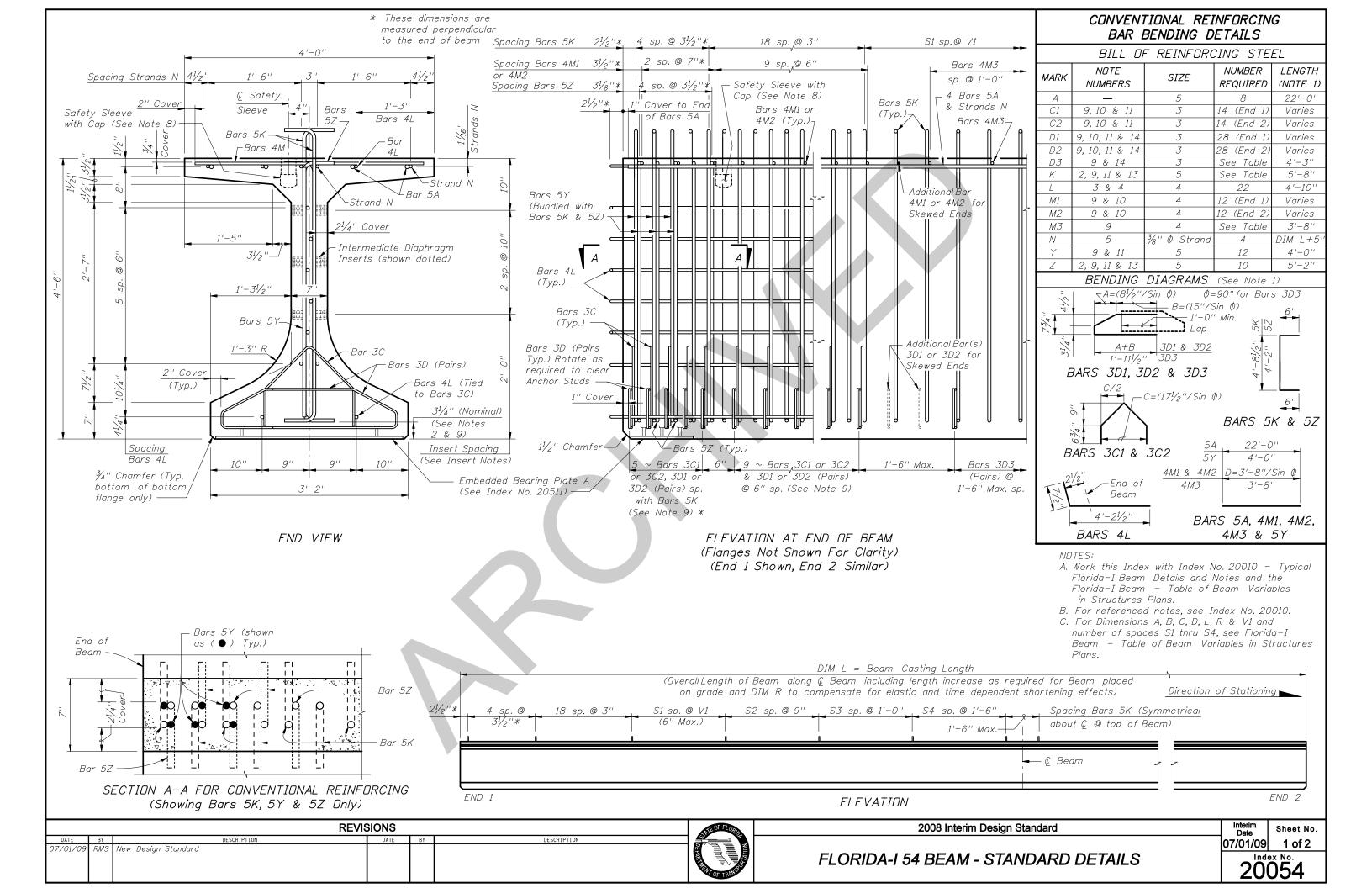
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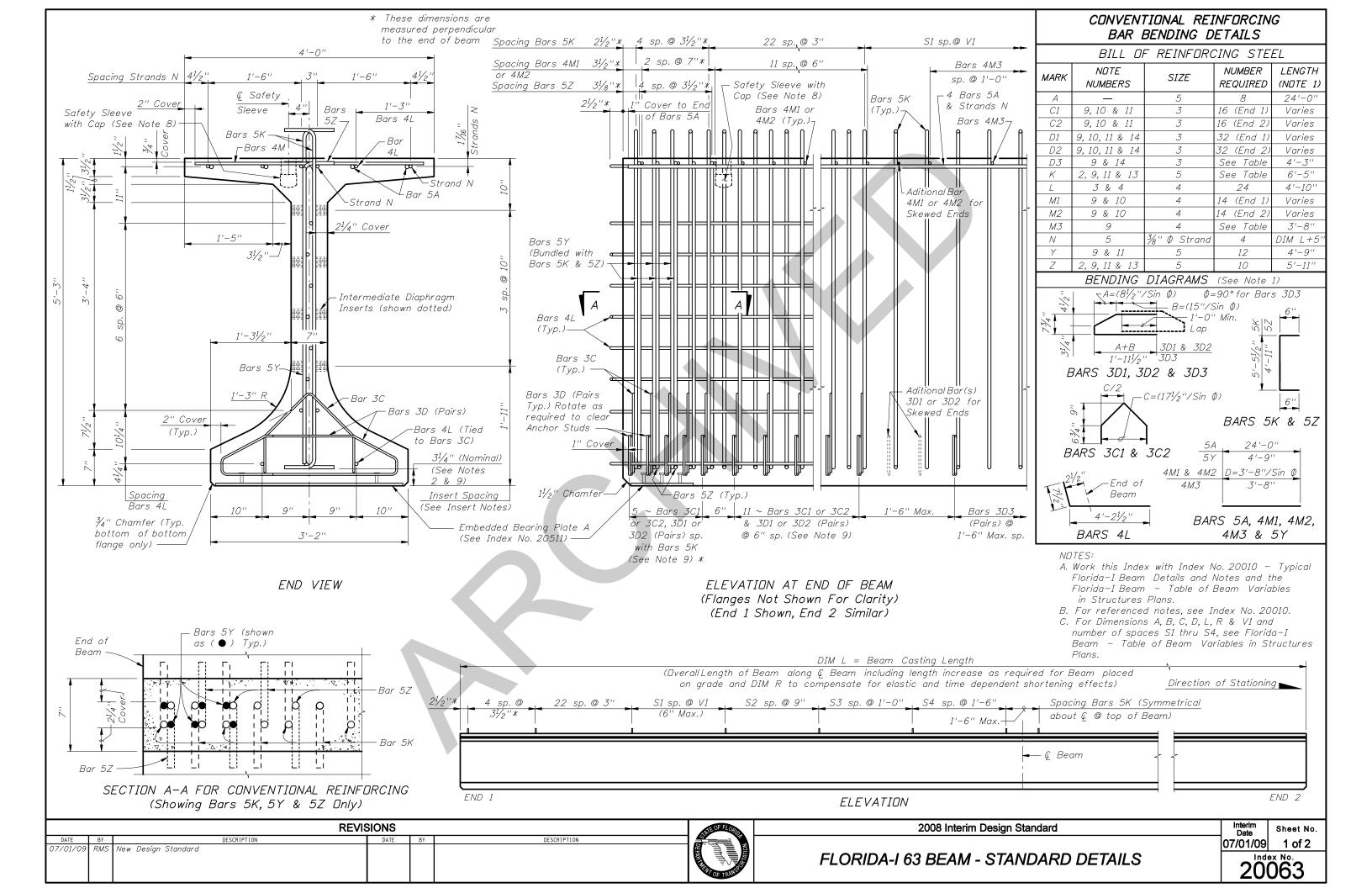




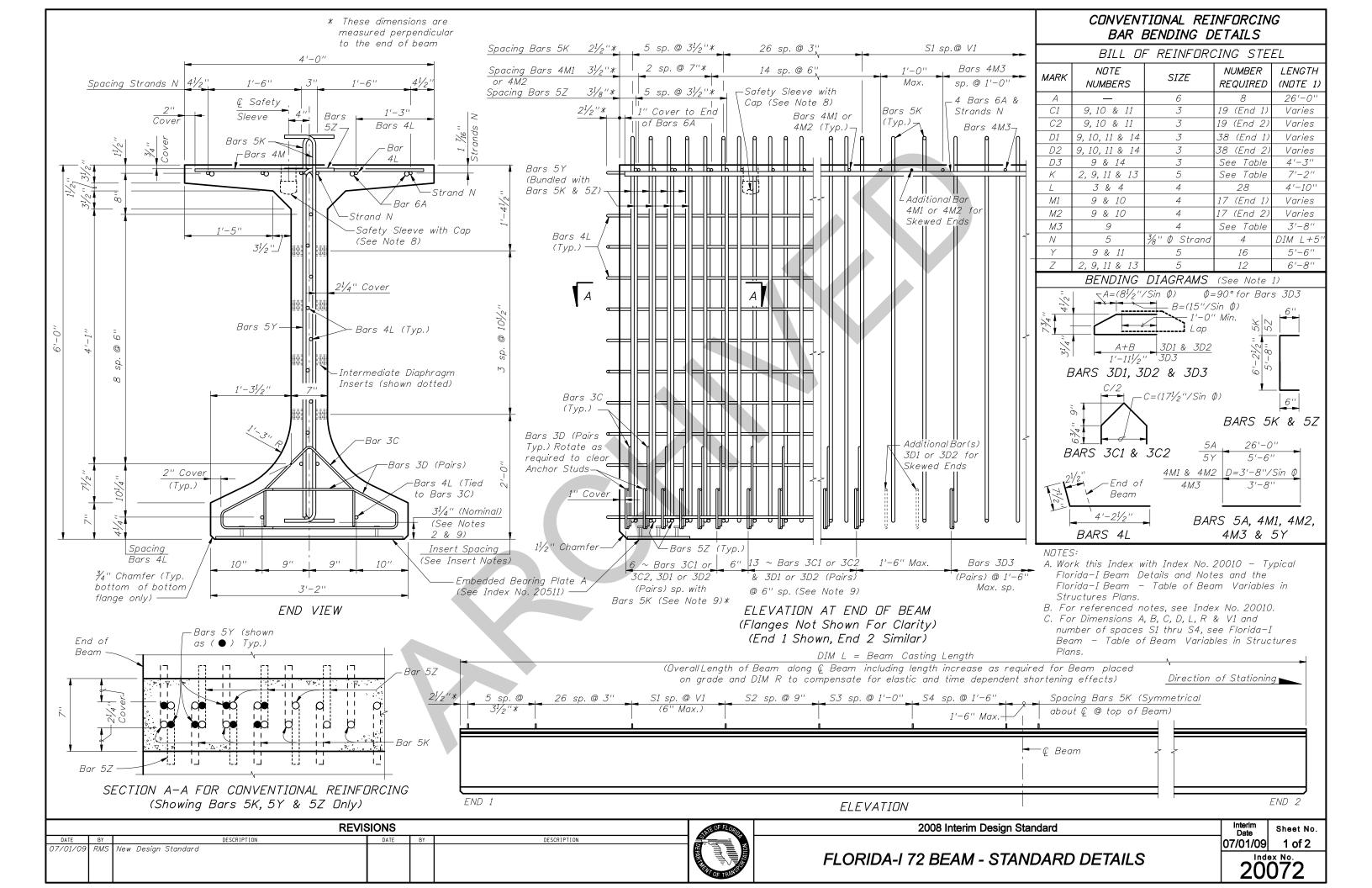
ALTERNATE REINFORCING STEEL (WELDED WIRE REINFORCEMENT) DETAILS Bars 5Y (12 Required) -Wires D31 (shown 11 ~ D16's @ 6" sp. = 5'-0" $D16's \sim @.1'-0'' sp.$ (shown as (ullet) Typ.) as (O) Typ.) End of Varies Varies 9" Max Beam - W6.4 1'-0'' Max. - W6.4 D16 1" extension -- 2¹/₄" Cover (Typ.) =Pieces K-1 Pieces K-2 (Offset) -SECTION A-A PLAN VIEW PLAN VIEW FOR WELDED WIRE REINFORCEMENT PIECES M PIECE M-3 PIECE M-1 Piece M-1 ties -Match spacing of END VIEW (2 Required) (2 Required) Pieces S (Single Mat) Tied adjacent Piece S-1, to Piece K-2to Strands at © Beam) S-2, S-3 or S-4 $8 \sim D25's$ (FF) @ 6'' = 3'-6''S1 ~ D25's @ V1 sp. (Piece S-1 shown, End of Beam — $8 \sim D25's (BF) @ 6'' = 3'-6'$ 5 ~ D31's @ S2 ~ D25's @ 9" sp. (Piece S-2) $S3 \sim D25$'s @ 1'-0" sp. (Piece S-3) $3^{1}/_{2}$ " sp. = 2" Cover S4 ~ D25's @ 1'-6" sp. (Piece S-4) 3" Offset 6" (Typ.) Varies 9" Max. (Typ.) (Typ.) PARTIAL SECTION AT CENTER BEAM Pieces K (Pairs) Pieces M--W12.4 (Piece K−1) W10 (Pieces K-2 & S) W10) .1134' -D31 (Piece K-1) Cover D25 (Pieces K-2 & S) 0 . (2" Min.) _ @ Beam (WWR -W12.4 (Piece K−1) Symmetrical) W10 (Pieces K-2 & S) Pieces D (Pairs) → | 1" extension (Typ.) PIECES K & S PIECE S-1, S-2, S-3 or S-4 PIECE K-1 PIECE K-2 PARTIAL BEAM END VIEW (FF Shown Solid) END VIEW (Aligned EF) (2 Required Each Piece) (4 Required (BF Shown Dashed) (Conventional Reinforcing Bars A, C, L, Y Piece D-1 ties ~ 2 Pairs) (4 Required) and Strands not Shown for Clarity) to Piece K-1 -NOTES: 5 ~ D11's @ $8 \sim D11's @ 6'' sp. = 3'-6''$ D11's @ 1'-6" spaces a. See Sheet 1 for placement details & Table of Beam Variables $3^{1/2}$ " sp. = Varies 1'-6" Max. in Structures Plans for variables S1, S2, S3, S4 & V1. b. Place Conventional Reinforcement Bars 5A, 3C & 4L as shown on Sheet 1. Place additional Bars 5Y as shown in Section A-A for Welded Wire Reinforcement. Bars 5Z will not be used with the WWR Option. c. Pieces may be fabricated in multiple length sections. d. For beams with skewed end conditions, Pieces D-1, D-2 & └─D11 (Typ. Pieces M−1 shall not be used; Conventional Reinforcement Bars D1, → | 1" extension (Typ.) 1'-111/2" LEGEND: D-1, D-2 & D-3) D2, C1, C2, M1 & M2 shall be used. See Index No. 20010 EF = Each FaceSkew Details and Note 9 for placement details. Shift PIECE D-2 FF = Front Face PIECE D-1 PIECE D-3 PIECES D Pieces K & Bars 5Y to accommodate skewed end BF = Back Face(4 Required ~ 2 Pairs) (4 Required ~ 2 Pairs) (4 Required ~ 2 Pairs) END VIEW conditions and align with Bars C and D. **REVISIONS** 2008 Interim Design Standard Sheet No. 07/01/09 2 of 2 RMS New Design Standard 20045 FLORIDA-I 45 BEAM - STANDARD DETAILS

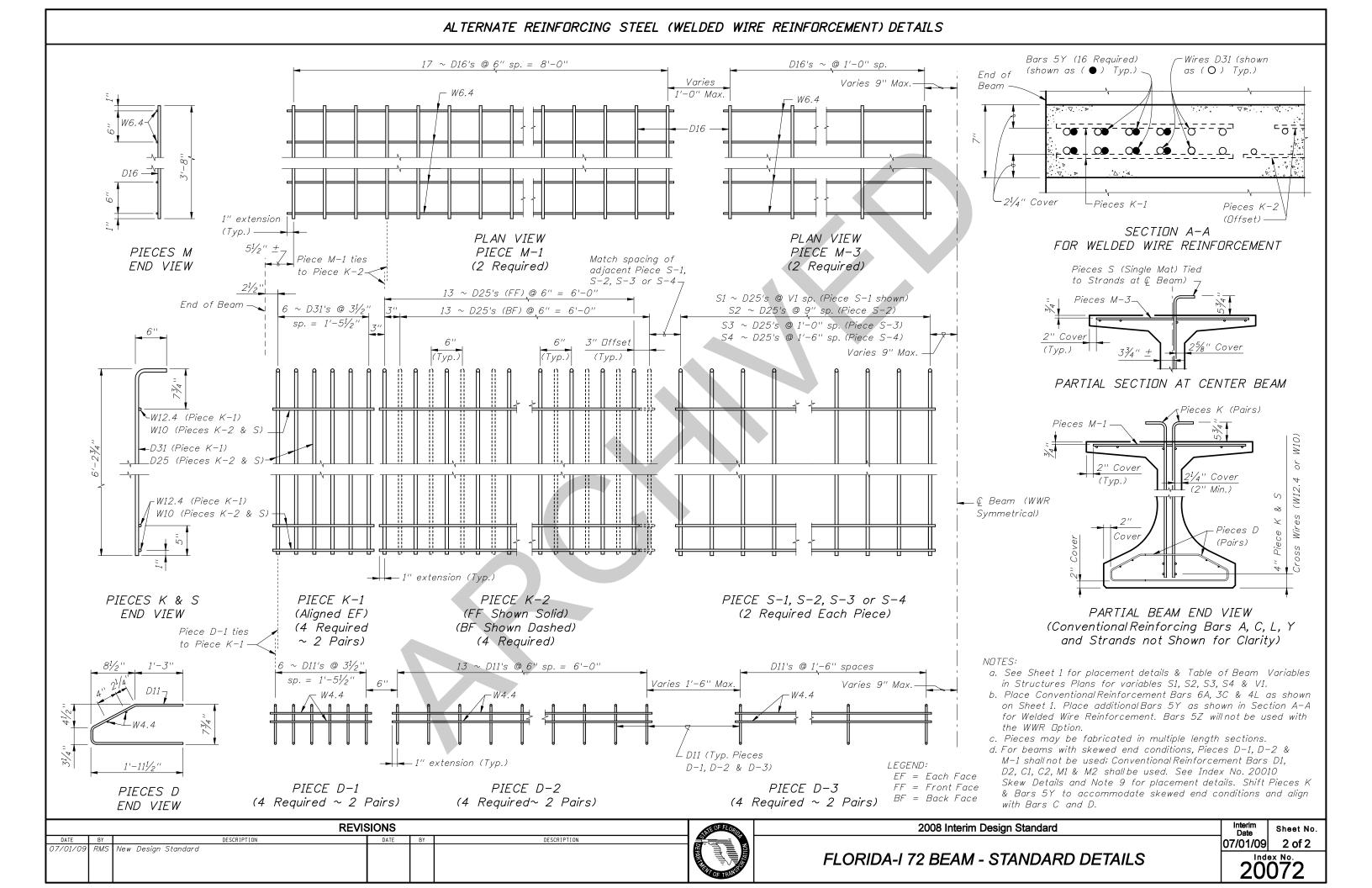


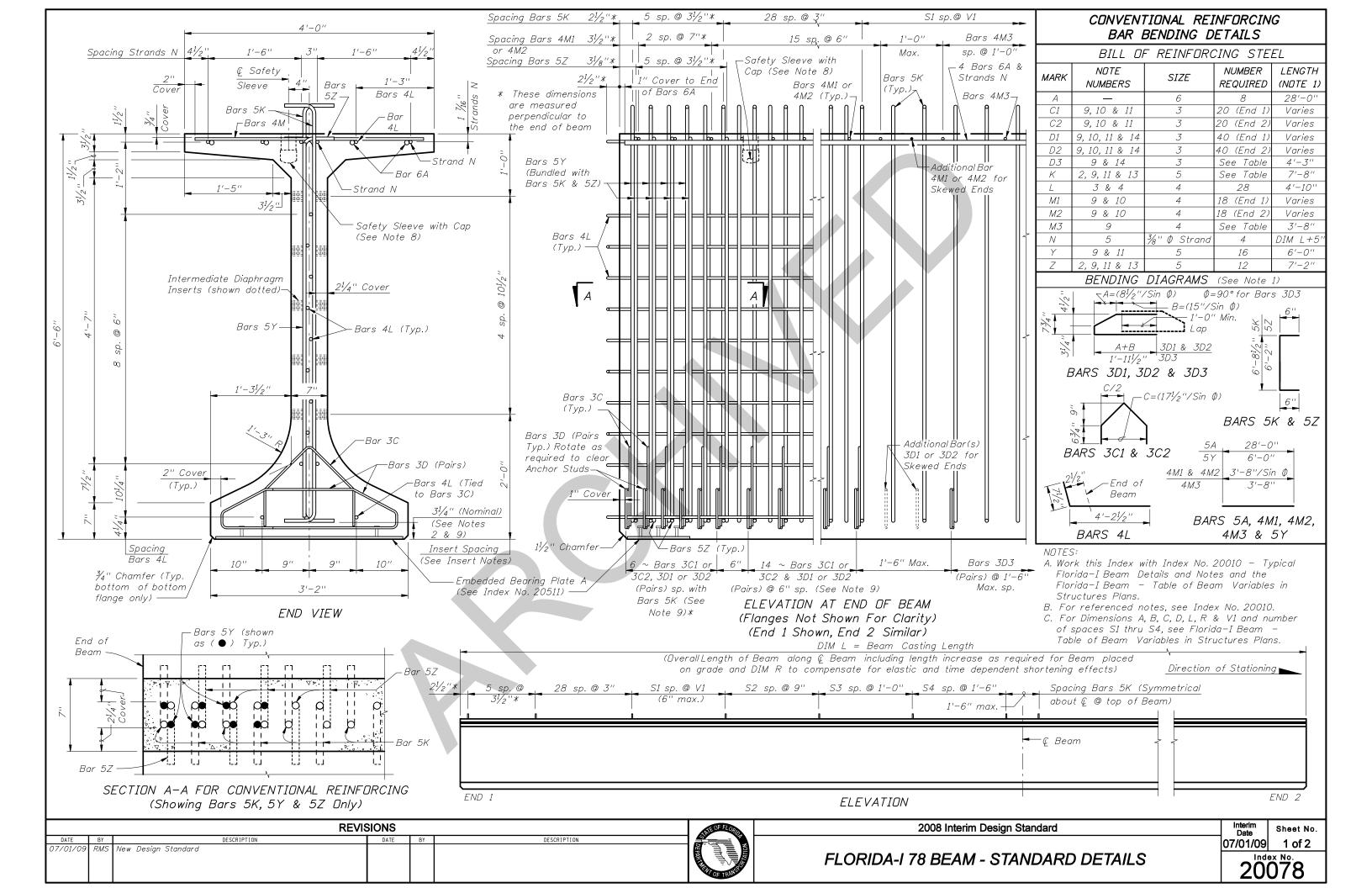
ALTERNATE REINFORCING STEEL (WELDED WIRE REINFORCEMENT) DETAILS Bars 5Y (12 Required) Wires D31 (shown 12 ~ D16's @ 6" sp. = 5'-6" D16's ~ @ 1'-0" sp. (shown as (\bullet) Typ.) as (**O**) Typ.) End of Varies Varies 9" Max. Beam W6.4 1'-0" Max. D16 1" extension (Typ.) =21/4" Cover Pieces K-1 Pieces K-2 (Offset) -SECTION A-A PLAN VIEW PLAN VIEW FOR WELDED WIRE REINFORCEMENT PIECE M-3 PIECES M PIECE M-1 Piece M-1 ties Match spacing of END VIEW (2 Required) (2 Required) Pieces S (Single Mat) Tied adjacent Piece S-1, to Piece K-2-S-2, S-3 or S-4to Strands at © Beam) $9 \sim D25$'s (FF) @ 6'' = 4'-0''S1 ~ D25's @ V1 sp. (Piece S-1 shown) Pieces M-3-End of Beam — S2 ~ D25's @ 9" sp. (Piece S-2) ~ D31's @ 9 ~ D25's (BF) @ 6" = 4'-0" S3 ~ D25's @ 1'-0" sp. (Piece S-3) $3^{1}/_{2}$ " sp. = S4 ~ D25's @ 1'-6" sp. (Piece S-4) 2" Cover 1'-2" 3" Offset (Typ.)Varies 9" Max. (Typ.) PARTIAL SECTION AT CENTER BEAM Pieces K (Pairs) -W12.4 (Piece K−1) Pieces M-W10 (Pieces K-2 & S) W10) 834 -D31 (Piece K-1) D25 (Pieces K-2 & S) € Beam (WWR -W12.4 (Piece K−1) Symmetrical) W10 (Pieces K-2 & S) Pieces D (Pairs) → | 1" extension (Typ. PIECES K & S PIECE K-2 PIECE S-1, S-2, S-3 or S-4 PIECE K-1 PARTIAL BEAM END VIEW (FF Shown Solid) END VIEW (Aligned EF) (2 Required Each Piece) (4 Required (BF Shown Dashed) (Conventional Reinforcing Bars A, C, L, Y Piece D-1 ties ~ 2 Pairs) (4 Required) and Strands not Shown for Clarity) to Piece K-1 - $9 \sim D11's @ 6'' sp. = 4'-0''$ 5 ~ D11's @ a. See Sheet 1 for placement details & Table of Beam D11's @ 1'-6" spaces $3^{1/2}$ " sp. = Variables in Structures Plans for variables S1, S2, S3, Varies 1'-6" Max. Varies 9' S4 & V1. b. Place Conventional Reinforcement Bars 5A, 3C & 4L as shown on Sheet 1. Place additional Bars 5Y as shown in Section A-A for Welded Wire Reinforcement. Bars 5Z will not be used with the WWR Option. c. Pieces may be fabricated in multiple length sections. d. For beams with skewed end conditions, Pieces D-1, D-2 & D11 (Typ. Pieces → - 1" extension (Typ.) 1'-111/2" LEGEND: M-1 shall not be used; Conventional Reinforcement Bars D1, D-1, D-2 & D-3) EF = Each FaceD2, C1, C2, M1 & M2 shall be used. See Index No. 20010 FF = Front Face Skew Details and Note 9 for placement details. Shift PIECE D-1 PIECE D-2 PIECE D-3 PIECES D Pieces K & Bars 5Y to accommodate skewed end BF = Back Face(4 Required) ~ 2 Pairs) (4 Required) ~ 2 Pairs) (4 Required) ~ 2 Pairs) END VIEW conditions and align with Bars C and D. **REVISIONS** 2008 Interim Design Standard Sheet No. 07/01/09 2 of 2 RMS New Design Standara FLORIDA-I 54 BEAM - STANDARD DETAILS 20054

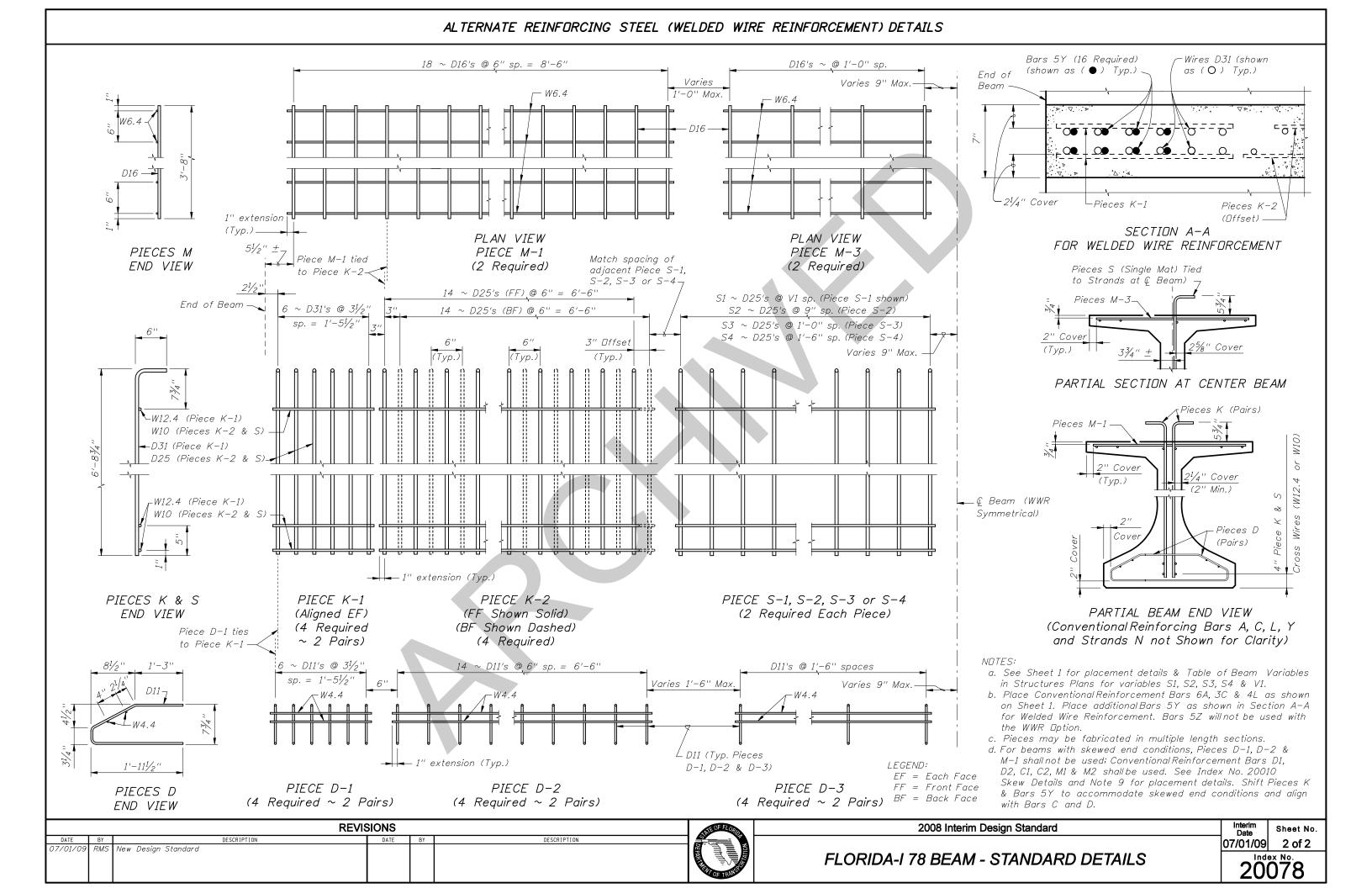


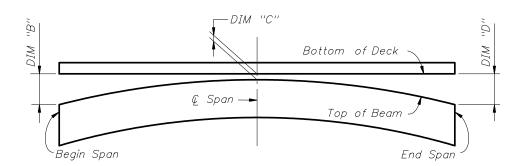
ALTERNATE REINFORCING STEEL (WELDED WIRE REINFORCEMENT) DETAILS Bars 5Y (12 Required) -Wires D31 (shown $14 \sim D16$'s @ 6" sp. = 6'-6" D16's ~ @ 1'-0" sp. (shown as (lacktriangle) Typ.) as (O) Typ.) End of Varies Varies 9" Beam W6.4 1'-0'' Max. - W6.4 D16 -2½" Cover Pieces K-1 Pieces K-2 (Offset) -1" extension (Typ.) — SECTION A-A PLAN VIEW PLAN VIEW FOR WELDED WIRE REINFORCEMENT PIECE M-3 PIECES M PIECE M-1 5" + Piece M-1 ties Match spacing of END VIEW (2 Required) (2 Required) Pieces S (Single Mat) Tied adjacent Piece S-1, to Piece K-2-S-2, S-3 or S-4to Strands at © Beam) 11 ~ D25's (FF) @ 6" = 5'-0" S1 ~ D25's @ V1 sp. (Piece S-1 shown) Pieces M-3 End of Beam — 5 ~ D31's @ 11 ~ D25's (BF) @ 6" = 5'-0" S2 ~ D25's @ 9" sp. (Piece S-2) $S3 \sim D25$'s @ 1'-0" sp. (Piece S-3) $3^{1}/_{2}$ " sp. = S4 ~ D25's @ 1'-6" sp. (Piece S-4) 2" Cover 1'-2" 6" 3" Offset (Typ.)Varies 9" Max. (Typ.) (Typ.) PARTIAL SECTION AT CENTER BEAM Pieces K (Pairs) W12.4 (Piece K−1) W10 (Pieces K-2 & S)-W10) 534' D31 (Piece K-1) 0 —√— D25 (Pieces K-2 & S) (W12.4 - & Beam (WWR *W12.4* (*Piece K−1*) Symmetrical) W10 (Pieces K-2 & S Pieces D (Pairs) - 1" extension (Typ.) PIECES K & S PIECE K-2 PIECE S-1, S-2, S-3 or S-4 PIECE K-1 PARTIAL BEAM END VIEW (FF Shown Solid) END VIEW (Aligned EF) (2 Required Each Piece) (4 Required (BF Shown Dashed) (Conventional Reinforcing Bars A, C, L, Y Piece D-1 ties ~ 2 Pairs) (4 Required) and Strands not Shown for Clarity) to Piece K-1 -NOTES: 5 ~ D11's @ 11 ~ D11's @ 6" sp. = 5'-0" D11's @ 1'-6" spaces a. See Sheet 1 for placement details & Table of Beam Variables $3^{1}/_{2}$ " sp. = Varies 1'-6" Max. in Structures Plans for variables S1, S2, S3, S4 & V1. b. Place Conventional Reinforcement Bars 5A, 3C & 4L as shown on Sheet 1. Place additional Bars 5Y as shown in Section A-A for Welded Wire Reinforcement. Bars 5Z will not be used with the WWR Option. c. Pieces may be fabricated in multiple length sections. d. For beams with skewed end conditions. Pieces D-1. D-2 & ∠ D11 (Typ. Pieces M-1 shall not be used; Conventional Reinforcement Bars D1, — 1" extension (Typ.) 1'-111/2" LEGEND: D-1, D-2 & D-3) D2, C1, C2, M1 & M2 shall be used. See Index No. 20010 EF = Each FaceSkew Details and Note 9 for placement details. Shift Pieces K FF = Front Face PIECE D-1 PIECE D-2 PIECE D-3 PIECES D & Bars 5Y to accommodate skewed end conditions and align BF = Back Face(4 Required ~ 2 Pairs) (4 Required ~ 2 Pairs) (4 Required ~ 2 Pairs) with Bars C and D. END VIEW **REVISIONS** 2008 Interim Design Standard Sheet No. 07/01/09 2 of 2 RMS New Design Standard 20063 FLORIDA-I 63 BEAM - STANDARD DETAILS



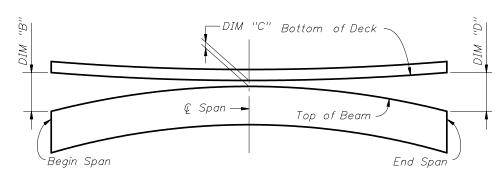




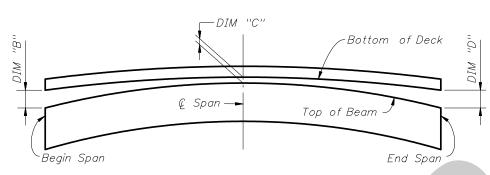




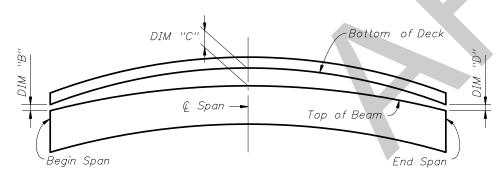
BUILD-UP DIAGRAM FOR TANGENT SPANS (ALONG & BEAM) (CASE 1)



BUILD-UP DIAGRAM FOR SAG VERTICAL CURVE SPANS (ALONG & BEAM) (CASE 2)



BUILD-UP DIAGRAM FOR CREST VERTICAL CURVE SPANS
- CONTROL AT Q SPAN
(ALONG Q BEAM) (CASE 3)



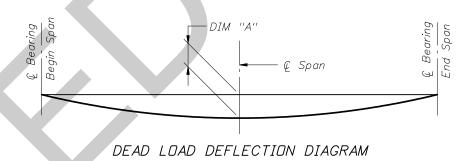
BUILD-UP DIAGRAM FOR CREST VERTICAL CURVE SPANS - CONTROL AT BEGIN OR END SPAN (ALONG & BEAM) (CASE 4)

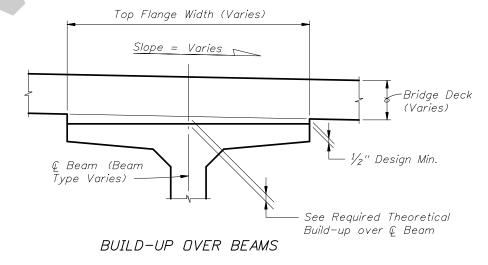
REVISIONS DATE BY DESCRIPTION DATE BY DESCRIPTION O7/01/09 SJN Added FLORIDA-I BEAMS to the Standard Title Block and Note. Changed the beam section to Florida-I Beam in the BUILD UP OVER BEAMS detail. Changed third sentence in BEAM CAMBER AND BUILD-UP NOTES.

BEAM CAMBER AND BUILD-UP NOTES:

The build-up values given in the table are based on theoretical beam cambers. The Contractor shall monitor beam cambers for the purpose of predicting camber values at the time of the deck pour. If the predicted cambers based on field measurements differ more than $+/-\frac{1}{2}$ " from the theoretical "Net Beam Camber @ 120 Days" shown in the Data Table, obtain approval from the Engineer to modify the build-up dimensions as required. When the measured beam cambers create a conflict with the bottom mat of deck steel, notify the Engineer a minimum of 21 days prior to casting.

DIM "A" includes the weight of the Stay-In-Place Formwork.





INSTRUCTIONS TO DESIGNER:

Although not shown here in the Diagrams or Notes, the effect of Horizontal Curvature, when present, needs to be considered for the Build-up Calculations.

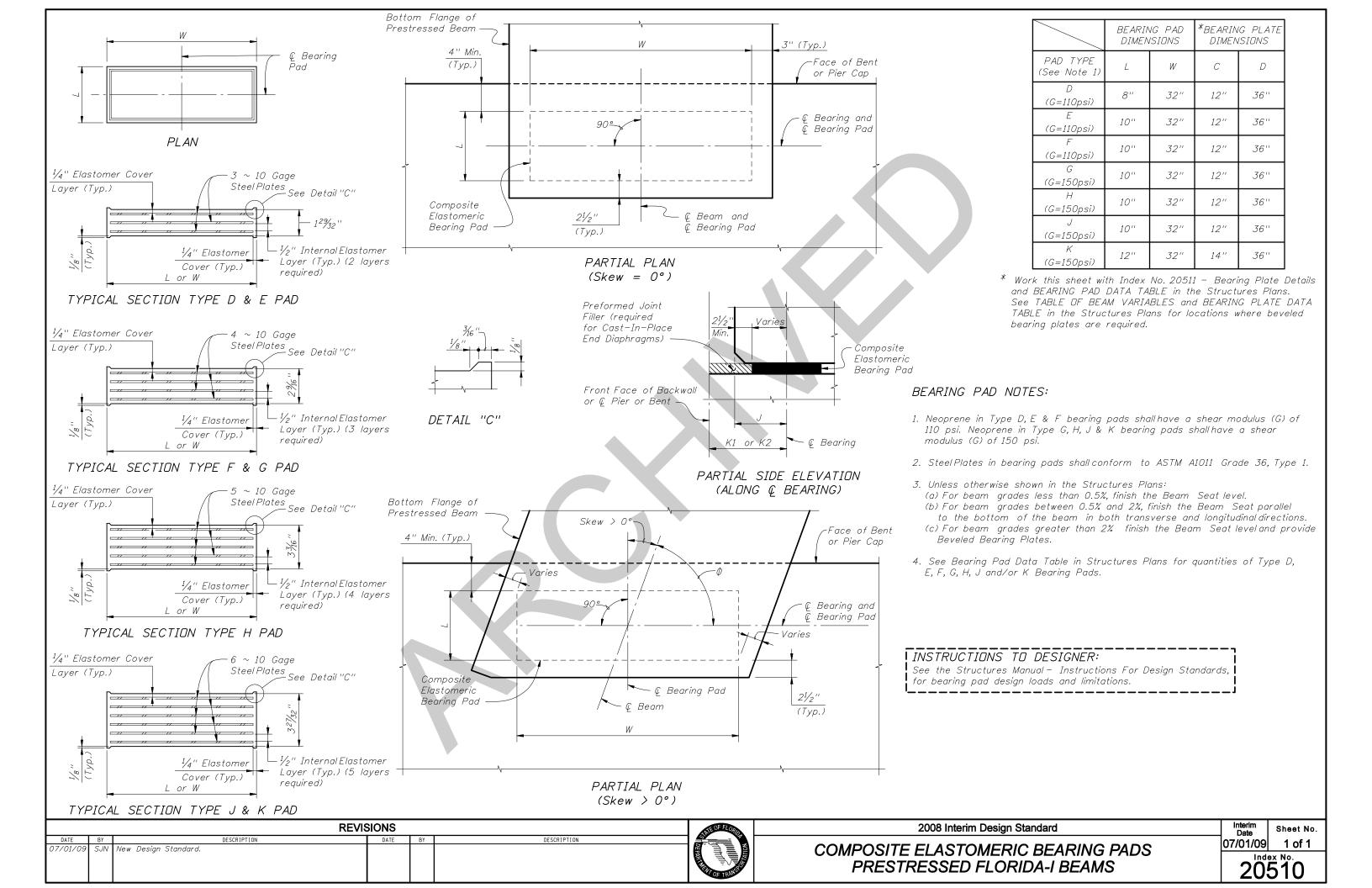
NOTE:

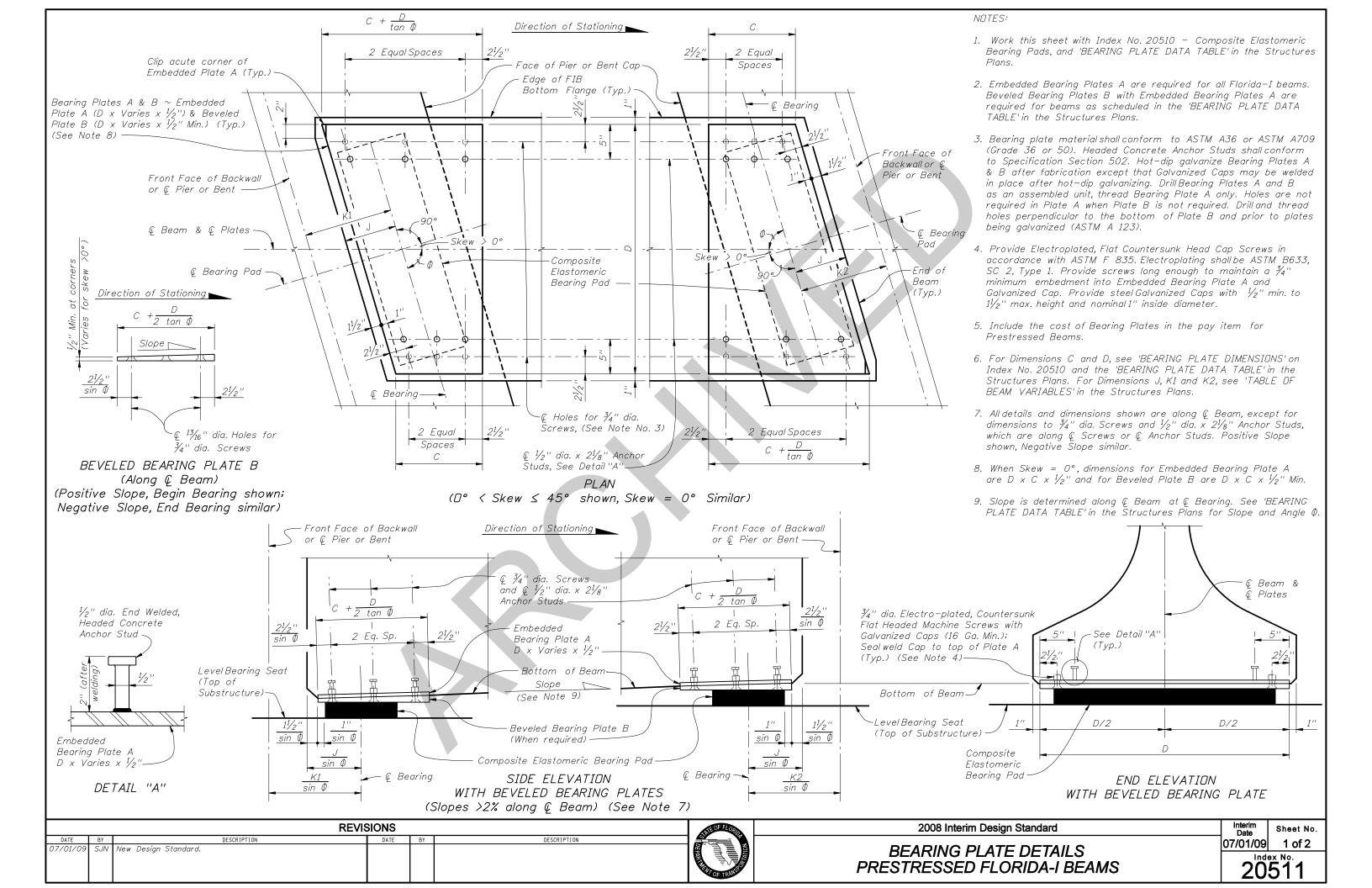
Work this Index with the Build-up and Deflection Data Table for AASHTO, Bulb-T and Florida-I Beams in Structures Plans.

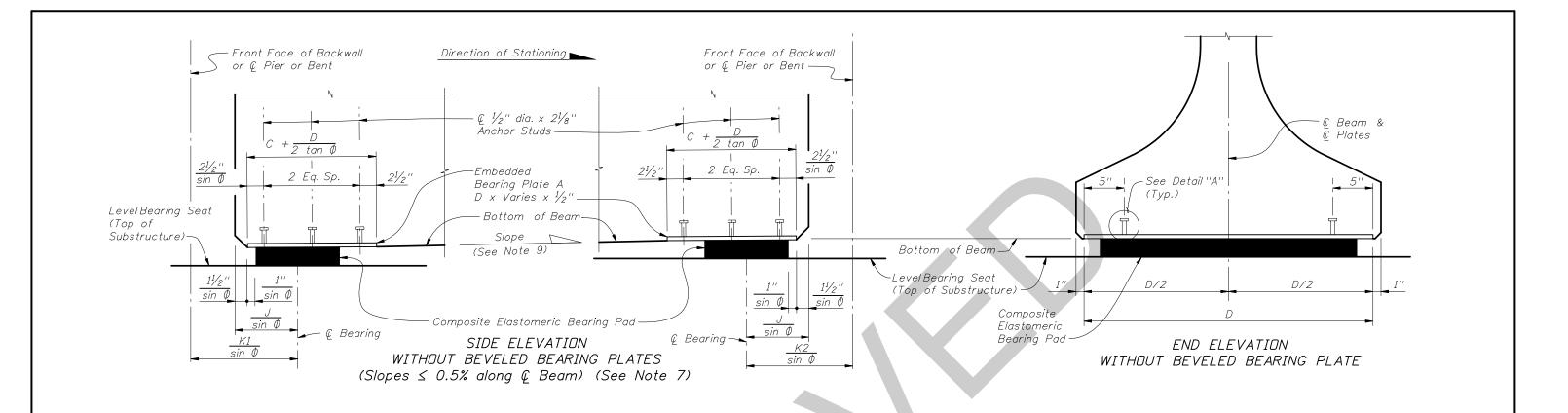
2008 Interim Design Standard

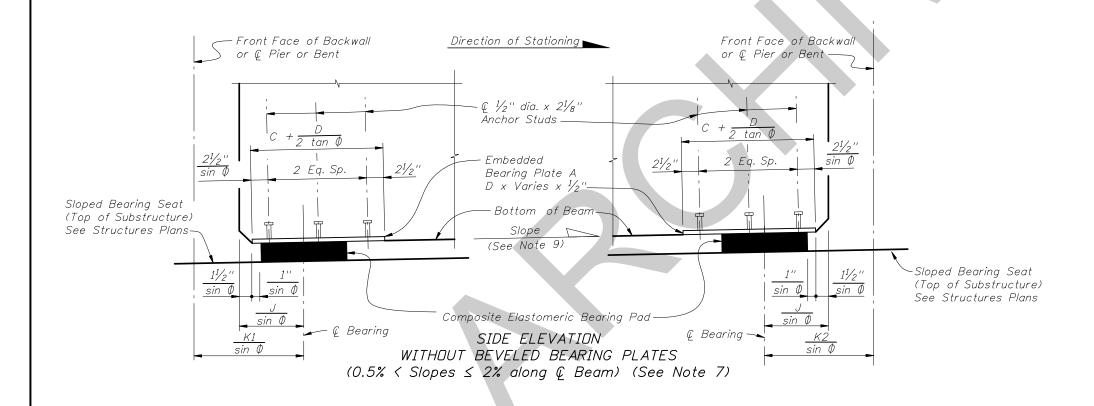
BUILD-UP & DEFLECTION DATA FOR

AASHTO, BULB-T AND FLORIDA-I BEAMS







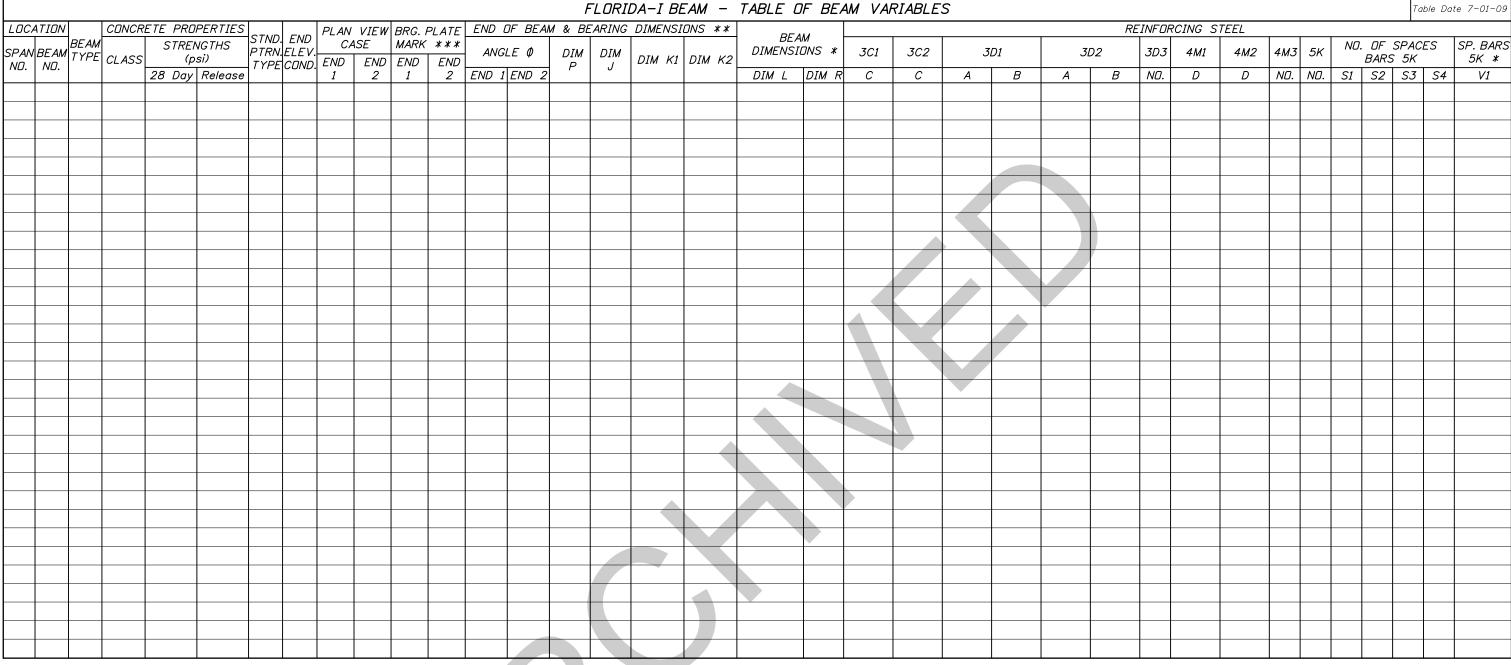


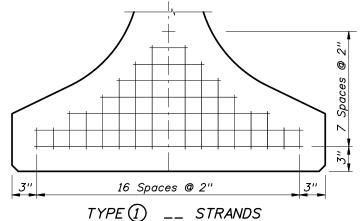
		REVISION	IS		ATE OF FLORID	2008 Interim Design Standard	Interim Date	Sheet No.
07/	 DESCRIPTION ndard.	DA	ATE BY	DESCRIPTION	BEPARENT OF TRAINER	BEARING PLATE DETAILS PRESTRESSED FLORIDA-I BEAMS	07/01/09	ex No.

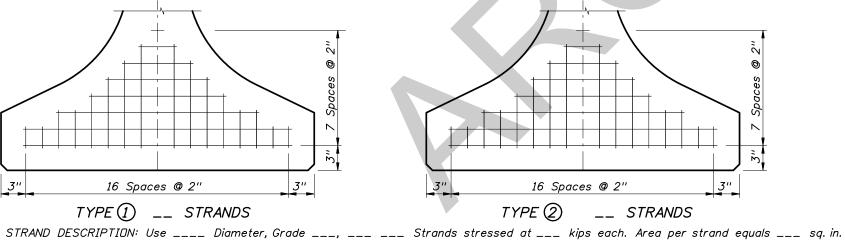
Attachment B

Florida-I Beam Related Data Tables (CADD Cells)

- Cell No. 20010 (1 Sheet): Florida-I Beam Table of Beam Variables
- Cell No. 20199 (1 Sheet): Build-up & Deflection Data Table
- Cell No. 20510 (1 Sheet): Bearing Pad Data Table (Florida-I Beam)
- Cell No. 20511 (1 Sheet): Bearing Plate Data Table (Florida-I Beam)







====== STRAND PATTERNS======

• - strands debonded _'-__" from end of beam.

• - fully bonded strands.

• - strands debonded _'-__" from end of beam.

STRAND DEBONDING LEGEND

▲ – strands debonded _'-__'' from end of beam.

• - strands debonded _'-__" from end of beam.

NOTE: On beams with skewed ends, the debonded length shall be measured along the shielded strand.

NDTE: Work this sheet with Design Standards Index Nos. 20010 and the applicable "Florida-I Beam Standard Details" Index.

DIMENSION NOTES

- * All longitudinal beam dimensions shown on this sheet with a single asterisk (*) are measured along the centerline of beam. Dimension "R" is calculated at mid-height of the beam.
- ** End beam bearing dimensions "J" and "K" are measured perpendicular to @ Bearing along the bottom of the beam.

BEARING PLATES

*** See Index No. 20511 and the Bearing Plate Data Table for details.

F		ASHTO, B	ULB-T A	AND FLOR	ATA TABLE RIDA-I BEAN	NS	ite 7-01-09	F					ATA TABLE RIDA-I BEAN	us	nte 7-01-09	F		ASHTO, B	ULB-T A	AND FLOR	NTA TABLE RIDA-I BEAM	15	nte 7-01-09
	TION		D THEORE P OVER ©	TICAL BEAM	NET BEAM CAMBER	DEAD LOAD DEFLECTION	BUILD-UP	LOCA	ATION	REQUIRI BUILD-U	ED THEORE IP OVER ©	TICAL BEAM	NET BEAM CAMBER (PRESTRESS	DEAD LOAD DEFLECTION DURING	BUILD-UP		ATION		D THEORE IP OVER ©	TICAL BEAM	NET BEAM CAMBER (PRESTRESS	DEAD LOAD DEFLECTION DURING	BUILD-UP
SPAN NO.	BEAM NO.	AT BEGIN SPAN DIM "B"	AT @ SPAN DIM "C"	AT END SPAN DIM "D"	OF REAM)	DURING DECK POUR @ 120 DAYS DIM "A"	CASE NO.	SPAN NO.	BEAM NO.	AT BEGIN SPAN DIM "B"	SPAN	AT END SPAN DIM "D"	- DEAD LOAD	DECK POUR 120 DAYS	CASL	SPAN NO.	BEAM NO.	AT BEGIN SPAN DIM "B"	AT @ SPAN DIM "C"	SPAN	- DEAD LOAD OF BEAM) @ 120 DAYS	DECK POUR @ 120 DAYS	CASE ND.

BEA	RING PAD DA	TA TABL	Ε	Table [Date 7-01-09
SPAN NO(s).	BEAM NO(s).	PAD TYPE	BEAM TYPE		BEAM END *

NOTE:
Work this table with Index No. 20510 for Pad Types D, E, F, G, H, J & K, and/or any project specific bearing pads.

* END 1 = Begin Bridge end of beam (Back station).

END 2 = End Bridge end of beam (Ahead station).

INSTRUCTIONS TO DESIGNER:

This table is intended for use with prestressed beam bridges, but may be modified for steel girder or other bridge types.

Supplement the BEARING PAD DATA TABLE with additional columns or notes as required to clearly identify the location and type of bearing pads.

PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING

	D BEARING P ANTITIES	PAD	Table Date 07-01-09
PAD TYPE	NUMBER REQUIRED		ANTITY (CF)

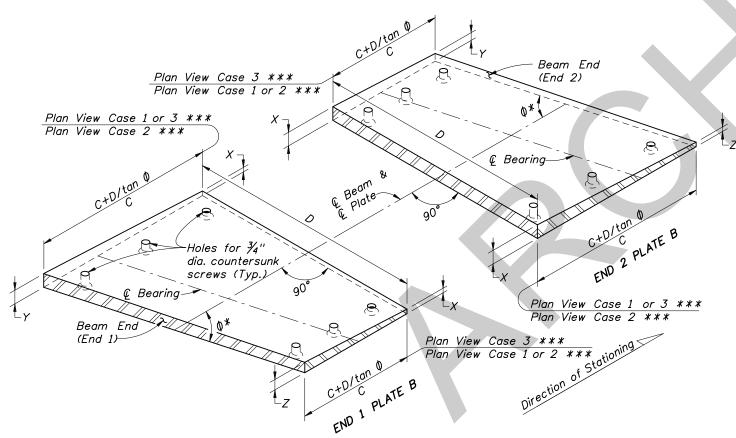


						BEAF	RING P	LATE	DATA	TABLE						Table Date	e 7-01-09			
	GENE	RAL BEAR	RING PL	ATE D	ATA				IBEDDED VSIONS	PLATE (PLATE A)	BEVELED	В	EVELED	PLATE DIME		(PLATE	B)			
BRG. PLATE	SPAN	BEAM	PAD	BEAM	PLAN VIEW	SLUFE		DIME	(inche		PLATE REQUIRED		ı	(inche	s) 					
MARK ***	ND(s).	ND(s).	TYPE	END	CASE	(%) **	<i>Ø *</i>	С	D	C+D/TAN Φ	(Yes/No)	С	D	C+D/TAN Φ	Χ	Υ	Z			

NOTES:

- * \emptyset = Acute angle (\le 90°) measured from left or right side of \emptyset Beam as required.
- ** Slope measured along © of Beam at © of Bearing.
- *** See "TABLE OF BEAM VARIABLES" and Index No. 20010.

See Index No. 20511 for additional notes and details.



ISOMETRIC VIEW OF BEVELED BEARING PLATES (SKEWED PLATES SHOWN, NON-SKEWED PLATES SIMILAR)

INSTRUCTIONS TO DESIGNER:

- 1. Fill in the table to correspond with data on the 'TABLE OF BEAM VARIABLES' using inch units for Beveled Plate dimensions 'X', 'Y' & 'Z' rounded to $\frac{1}{16}$ th of an inch.
- 2. Use the following equations to determine the Beveled Plate thicknesses for 'PLAN VIEW CASES' and 'END ELEVATION CONDITIONS' corresponding to those shown on Design Standards Index No. 20010. The Slope parameter in these equations requires decimal units and correct sign convention:

```
END 1 END 2
```

```
(I) PLAN VIEW CASE 1:
```

(a) END ELEVATION CONDITION 1 or 2 (Positive Slope)

 $X = 0.5'' + (C) \times Slope$ X = 0.500''

Y = Z = 0.500" Y = Z = 0.5" + (C) x Slope

(b) END ELEVATION CONDITION 3 (Negative Slope)

X = 0.500'' $X = 0.5'' - (C) \times Slope$ $Y = Z = 0.5'' - (C) \times Slope$ Y = Z = 0.500''

(II) PLAN VIEW CASE 2:

(a) END ELEVATION CONDITION 1 or 2 (Positive Slope)

 $X = 0.5'' + (C + D / tan \Phi) \times Slope X = 0.500''$

Y = 0.500'' $Y = 0.5'' + (C) \times Slope$

 $Z = 0.5'' + (D / tan \phi) \times Slope$ $Z = 0.5'' + (C + D / tan \phi) \times Slope$

(b) END ELEVATION CONDITION 3 (Negative Slope)

X = 0.500" X = 0.5" - $(C + D / \tan \phi) \times Slope$ Y = 0.5" - $(C + D / \tan \phi) \times Slope$ Y = 0.5" - $(D / \tan \phi) \times Slope$

 $Z = 0.5'' - (C) \times Slope$ Z = 0.500''

(III) PLAN VIEW CASE 3:

(a) END ELEVATION CONDITION 1 or 2 (Positive Slope)

 $X = 0.5'' + (C + D / tan \Phi) \times Slope X = 0.500''$

 $Y = 0.5" + (D / tan \emptyset) \times Slope$ $Y = 0.5" + (C + D / tan \emptyset) \times Slope$

Z = 0.500'' $Z = 0.5'' + (C) \times Slope$

(b) END ELEVATION CONDITION 3 (Negative Slope)

X = 0.500'' $X = 0.5'' - (C + D / tan \Phi) \times Slope$

 $Y = 0.5" - (C) \times Slope$ Y = 0.500" $Z = 0.5" - (C + D / tan <math>\phi$) x Slope $Z = 0.5" - (D / tan <math>\phi$) x Slope

PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING

Attachment C

Instructions for Design Standards

- Index 20000 Series (1 Sheet): Prestressed Florida-I Beam Instructions
- Index 20510 (1 Sheet): Composite Elastomeric Bearing Pad Instructions for Florida-I Beams

The Standard Drawings for prestressed beams depict details and notes that are fully developed. These drawings are included in the contract documents by reference to the Index No. in the plans. Companion MicroStation CADD cells are located on the FDDT Structures Bar Menu, and they contain generic details and notes that require completion including the Table of Beam Variables, the Strand Pattern Details and the Strand Debonding Legend. When completed, the CADD cells shall be included in the plans.

Standard Drawings and completed CADD cells provide sufficient information to permit beam fabrication without the submittal of shop

The prestressed beams in these Standard Drawings are generally assumed to act as simple spans under both Dead Load and Live Load even where the deck is designed continuous across the support.

The elastic and time dependent shortening effects (DIM R) should be reported at mid-height of the beam @ 120 days. The average of the calculated values for the top and bottom of the beam may be used.

The following example shows the data required for completion of a

The example assumes a three span bridge designed for the following conditions:

Live Load: HL-93

20010

NSING

DRAWING

Stay-in-Place Metal Forms:

projected plan area of the forms (this includes the unit weight

When the total initial tensioning force of the fully bonded strands required by design exceeds the values shown on Index No. 20010, shield additional strands at the end of the beam when possible. The end reinforcement may only be redesigned to accommodate an increased vertical splitting force when approved by the State Structures Design Office. If approved, Index No. 20010 and the appropriate Standard Detail Drawings must then be modified for inclusion in the contract documents and signed and sealed by the E.O.R.

Include the following data tables in the Structures Plans for all Florida-I Beams:

DDT Structures CADD Cell:	Description:	Associated Desigi Standards Index N
20010	Table of Beam Variables	20036 through 200
20199	Build-Up & Deflection Data Table	20199
20510	Bearing Pad Data Table	20510
20511	Bearing Plate Data Table	20511

OTHER CONSIDERATIONS:

When the actual number of beams or strand patterns exceed the capacity of a single plan sheet using the standard "TABLE OF BEAM VARIABLES", use additional sheets. If special conditions require dimensions, details or notes not shown in the standard CADD cells, modifications are permitted. However, the "TABLE OF BEAM VARIABLES" should not be modified when utilizing the Standard Drawings.

When required by design, intermediate diaphragms shall be shown on the Framing Plan sheet included with the bridge drawings. Insert locations with respect to the beam ends and beam faces shall be tabulated for each beam. The table shall include length adjustments for beams placed on grade and for elastic and time dependent shortening effects. Type 33 No. 8 reinforcing bars with 3" thread lengths must be shown on the intermediate diaphragm details and included in the rebar list for attachment to the inserts.

Embedded bearing plates are required for all beams. If the beam grade exceeds 2%, provide beveled bearing plates at each end of the beam as shown in Index No. 20511.

Angle ϕ , as defined in Design Standards Index No. 20010, shall be rounded up to the nearest degree. The shear stirrup spacing V1 for Bars 5K should be specified to the nearest inch.

Beam Design: Beam: Florida-I 45 Beam Spacing: 11'-3'', 87' Span (5 Beams) 9'-0", 102' Span (6 Beams) Design Span Length: 84'-6" (Spans 1 & 3) 99'-8" (Span 2)

Florida-I Beam Table of Beam Variables CADD cell. This case shows a Florida-I 45 Beam (Index No. 20045).

No intermediate Diaphragms

Allowance of 20 PSF non-composite dead load over the of metal forms and the concrete required to fill the form flutes). Environment (Superstructure): Moderately Aggressive Bridge Characteristics: Length: 276 ft. Width: 51'-1" (out-to-out) Clear Roadway: 48 ft.

Superstructure: Three simple spans of prestressed concrete beams with 8-inch composite deck slab (plus $\frac{1}{2}$ " sacrificial deck thickness). Span: 87'-0", 102'-0", 87'-0"

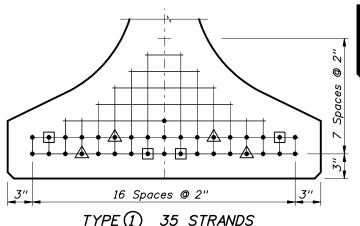
Sidewalk: None

Horizontal Alianment: Straight Vertical Alignment: 0.00% Grade Skew Angle: 15 degrees (Right)

FLORIDA-I BEAM - TABLE OF BEAM VARIABLES

Table Date 7-01-09

, IE	.DCA1	TON		CONCR	ETE PRO	PERTIES	071/0	5,45	PLAN	VIEW	BRG. F	PLATE	END OF BEA	M & BI	EARING	DIMENS1	ONS **	DEA	, [RE	INFORCI	ING ST	TEEL						
; _s	PANIF	FAM	BEAM	CLASS	STREM	VG 1 NO		. END LELEV.	I C4	ISE	MARK		ANGLE Ø	DIM				DIMENSI		3C1	3C2	31	01	31	72	3D3	4M1	4M2	4M3	5K		SPAC	ES	SP. BARS
5 5	vo.	NO.	TYPE			SI)	TYPE	COND.	END	END	END	END		P	J	DIM K1	DIM K2								- <u>-</u>		-					RS 5K		5K *
` _					28 Day	Release			1	2	1	2	END 1 END 2	?				DIM L	DIM R	С	С	Α	В	Α	В	NO.	D	D		<i>NO.</i> .	SI S2	? <i>S3</i>	S4	V1
1 L	1 .	1-5	45	V	6500	5000	2	1	2	2	1-1	1-2	75° 75°	_	71/2"	1'-3½"	1'-11/2"	85'-10 ¹ / ₂ "	1"	1'-6 ¹ /4''	1'-6 ¹ /4''	8¾"	1'-3½"	8¾"	1'-3½"	102 3'-	- <i>9½''</i>	3'-9½"	74 .	148	16 35	5 –	2	6"
<u> </u>	2 .	1-6	45	V	6500	5000	1	1	2	2	2-1	2-2	75° 75°	-	71/2"	1'-11/2"	1'-11/2"	101'-0¾''	11/4"	1'-61/4''	1'-61/4"	8¾''	1'-31/2"	8¾''	1'-31/2"	120 3'-	-9½"	3'-91/2"	<i>89</i> .	136	10 13	10	14	6"
$\langle $	3 .	1-5	45	V	6500	5000	2	1	2	2	3-1	3-2	75° 75°	-	71/2"	1'-11/2"	1'-31/2"	85'-101/2"	1"	1'-61/4''	1'-61/4"	8¾"	1'-31/2"	8¾"	1'-31/2"	102 3'-	-9½"	3'-91/2"	74 .	148	16 35	5 -	2	6"
֓֞֞֞֞֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֞֓֓֓֓֡֡֞֡֓֓֡֡֡֡֡֡																																		



Designer should position two strands at both edges of flange to support Bars D. 16 Spaces @ 2" TYPE (2) 30 STRANDS

STRAND DESCRIPTION: Use 0.6 Diameter, Grade 270, Low Relaxation Strands stressed at 44 kips each. Area per strand equals 0.217 sq. in. = STRAND PATTERNS=

STRAND DEBONDING LEGEND • - fully bonded strands.

• - strands debonded 10'-0" from end of beam.

• - strands debonded 20'-0" from end of beam.

▲ - strands debonded 25'-0" from end of beam.

NOTE: On beams with skewed ends, the debonded length shall be measured along the shielded strand.

NOTE: Work this sheet with Design Standards Index Nos. 20010 and the applicable "Florida-I Beam Standard Details" Index.

DIMENSION NOTES

- * All longitudinal beam dimensions shown on this sheet with a single asterisk (*) are measured along the centerline of beam. Dimension "R" is calculated at mid-height of the beam.
- ** End beam bearing dimensions "J" and "K" are measured perpendicular to © Bearing along the bottom of the beam.

BEARING PLATES

*** See Index No. 20511 and the Bearing Plate Data Table for details.

BRIDGE NO. 123456



Design Instructions & Information For FDOT Design Standards

Last Revision Sheet No. 07/01/09 1 of 1

PRESTRESSED FLORIDA-I BEAM INSTRUCTIONS

Index No.(s) 20000 Series

GENERAL INSTRUCTIONS:

Design Standard No. 20510 depicts details and notes for elastomeric bearing pads for prestressed concrete beams with or without skewed end conditions. Include the 'BEARING PAD DATA TABLE' in the plans. (See FDOT Structures Bar Menu).

Design Standard No. 20511 contains generic details and notes for beveled and embedded bearing plates. Include the 'BEARING PLATE DATA TABLE' in the plans. (See FDDT Structures Bar Menu)

For beam grades greater than 2%, provide beveled bearing plates. For Florida-I beams on grades less than or equal to 2%, only Embedded Bearing Plates A need to be installed in the 'BEARING PLATE DATA TABLE'.

	LIMITING PARAMETERS FOR ELASTOMERIC BEARING PADS USED WITH PRESTRESSED FLORIDA-I BEAMS														
PAD TYPE	LENGTH (in)	WIDTH (in)	MAXIMUM SERVICE LIVE LOAD (kips)	MAXIMUM SERVICE DEAD LOAD (LL = actual Service Live Load)	SKEW ANGLE (degrees)	MAXIMUM SHEAR DEFLECTION (in)	SHEAR MODULUS, G (psi)								
D	8	32	135	DL=147+1.75(135-LL)	0 - 5	0.75	110								
D	8	32	110	DL=120+1.75(110-LL)	0 - 15	0.75	110								
Ε	10	32	150	DL=233+1.75(150-LL)	0 - 5	0.75	110								
Ε	10	32	110	DL=113+1.75(110-LL)	0 - 20	0.75	110								
F	10	32	150	DL=290+1.75(150-LL)	0 - 5	1	110								
F	10	32	120	DL=139+1.75(120-LL)	0 - 30	1	110								
G	10	32	145	DL=230+1.75(145-LL)	0 - 30	1	150								
G	10	32	95	DL=98+1.75(95-LL)	0 - 45	1	150								
Н	10	32	180	DL=268+1.75(180-LL)	0 - 35	1.25	150								
Н	10	32	135	DL=230+1.75(135-LL)	0 - 45	1.25	150								
J	10	32	145	DL=227+1.75(145-LL)	0 - 45	1.5	150								
K	12	32	200	DL=383+1.75(200-LL)	0 - 45	1.5	150								

The Service Live Load (including impact) and Service Dead Load Reactions can be determined from the beam design. The Shear Deflection is the product of the coefficient of thermal expansion, 65% of the thermal gradient and the length of bridge contributing to movement, plus the contributing beam creep and shrinkage at the bottom of beam. Assume beam creep and shrinkage from day 120 to day 240 (this value can be determined from data in the beam design output).

Standard Elastomeric bearing pads have been designed in accordance with AASHTO LRFD Specifications, Method "B" (2009 Interim), for a maximum static rotation (beam grade, camber and dead load rotation) of 0.0125 radians and a cyclic rotation (live load) of 0.004 radians. Live load rotations are assumed to be in the opposite direction to static rotations. Rotation does not need to be checked for standard prestressed beams provided that the top of the beveled bearing plates (when required) or the bearing seats (pedestals) are finished approximately parallel to the slope of the beam. The effects of camber (at day 120) from prestressing and dead load deflection, may be neglected when determining the slope at the ends of the beam, unless the sum of these effects exceeds 0.0125 radians (1.25%). Bearing seats may be finished level for beam grades less than 0.5%, or when the combined effects of beam grade, camber and dead load rotation do not exceed 1.25%. Whenever possible, the bearing seats at each end of the beam should be detailed with the same slope.

For design values exceeding the limiting parameters shown on this sheet, the designer must develop custom designs and details. For skew angles greater than 45°, consider round pads with elastomer and plate thicknesses similar to those shown in Design Standard No. 20510.

EXAMPLES:

The following examples show the information required to determine the correct standard elastomeric bearing pad type to use:

EXAMPLE 1 *

Given Information:

Superstructure Type - One Simple Span

45" Florida I Beams 101'-0" long, spaced at 9'-0" centers (99'-8" center to center bearing)

No longitudinal restraints except friction between the pad and the concrete substructure

Service Live Load Reaction = 106 kips

Service Dead Load Reaction = 109 kips

Coefficient of Thermal Expansion = 0.000006/°F

Thermal Gradient = $70^{\circ}F$

Creep and Shrinkage at the Bottom of Beam (from day 120 to day 240) = 0.28"

Shear Deflection = $(0.000006)^{\circ}F \times 0.65 \times 70^{\circ}F \times 99.67'/2 \times 12''/') + 0.280''/2 = 0.30''$

Beam Grade = 2.0%

Skew Angle = 15°

Service Dead Load Rotation = 0.007 radians (0.7%)

Beam Camber Rotation @ 120 days = 0.012 radians (1.2%)

Net Beam Camber Rotation after Dead Load Deflection = 0.012 - 0.007 = 0.005 radians (0.5%)

Elastomeric Bearing Pad Type Determination:

Compare the design values to the Limiting Parameters Table, Pad Type D for Florida-I Beams.

Limiting Parameters Versus Design Values:

Maximum Service Live Load Reaction of 110 kips versus Design Value of 106 kips; therefore, DK

Maximum Service Dead Load Reaction of 120+1.75(110-106) = 127 kips versus Design Value of 109 kips; therefore, DK

Maximum Shear Deflection of 0.75" versus Design Value of 0.30"; therefore, DK

Skew Angle is between 0° and 15°; therefore, DK

Conclusion:

Use Elastomeric Bearing Pad Type D.

No beveled plate is required. Detail beam seat with a 2% slope along the centerline of beam.

Complete 'BEARING PLATE DATA TABLE' for embedded bearing plate only.

EXAMPLE 2 *

Given Information

Superstructure Type - Four Simple Spans with Continuous Deck

45" Florida I Beams 101'-0" long, spaced at 9'-0" centers (99'-8" center to center bearing)

No longitudinal restraints except friction between the pad and the concrete substructure

Service Live Load Reaction = 106 kips

Service Dead Load Reaction = 109 kips

Coefficient of Thermal Expansion = 0.000006/°F

Thermal Gradient = $70^{\circ}F$

Creep and Shrinkage at the Bottom of each Beam (from day 120 to day 240) = 0.28"

Shear Deflection = $(0.000006)^{\circ}F \times 65\% \times 70^{\circ}F \times 202' \times 12''/') + 0.280''/2 = 0.80''$

Beam Grade = 5%

Skew Angle = 15°

Service Dead Load Rotation = 0.007 radians (0.7%)

Beam Camber Rotation @ 120 days = 0.012 radians (1.2%)

Net Beam Camber Rotation after Dead Load Deflection = 0.012 - 0.007 = 0.005 radians (0.5%)

Elastomeric Bearing Pad Type Determination:

Compare the design values to the Limiting Parameters Table, Pad Type F for Florida-I Beams.

Limiting Parameters Versus Design Values:

Maximum Service Live Load Reaction of 120 kips versus Design Value of 106 kips; therefore, DK

Maximum Service Dead Load Reaction of 139+1.75(120−106) = 163.5 kips versus Design Value of 109 kips; therefore, DK

Maximum Shear Deflection of 1.0" versus Design Value of 0.80"; therefore, DK

Skew angle is between 0° and 30°; therefore, DK

Conclusion:

Use Elastomeric Bearing Pad Type F. Additionally, because beam end slope exceeds 2%, include a beveled bearing plate in the 'BEARING PLATE DATA TABLE' and detail bearing seats level. Neglect the effects of net beam camber in the beveled bearing plate design since rotation is less than 0.0125 radians.

* The above examples do not assume any wind or braking loads are applied to the elastomeric bearing pads.



Design Instructions & Information For FDOT Design Standards

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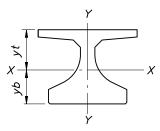
Attachment D

Design Aids

- 'Florida-I Beam Section Properties' (1 Sheet)
- 'Florida-I Beam Estimated Maximum Span Lengths' charts (2 Sheets)

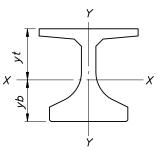
 Note: For preliminary design and cost estimating purposes only, not a substitute for beam design





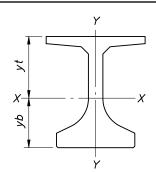
F.I.B.-36 (INDEX NO. 20036)

SECTION PROPERTIES		
Area (in²)	806.58	
Perimeter (in)	206.57	
Ixx (in ⁴)	127,564	
Iyy (in⁴)	81,131	
yt (in.)	19.51	
yb (in.)	16.49	



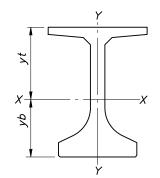
F.I.B.-45 (INDEX NO. 20045)

SECTION PROPERTIES	
Area (in²)	869.58
Perimeter (in)	224.57
Ixx (in ⁴)	226,625
Iyy (in⁴)	81,397
yt (in.)	24.79
yb (in.)	20.21



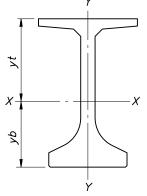
F.I.B.-54 (INDEX NO. 20054)

SECTION PROPERTIES	
Area (in²)	932.58
Perimeter (in)	242.57
Ixx (in ⁴)	360,041
Iyy (in⁴)	81,656
yt (in.)	29.97
yb (in.)	24.03



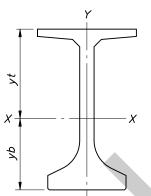
F.I.B.-63 (INDEX NO. 20063)

SECTION PROPERTIES	
Area (in²)	995.58
Perimeter (in)	260.57
Ixx (in ⁴)	530,560
Iyy (in⁴)	81,919
yt (in.)	35.06
yb (in.)	27.94



F.I.B.-72 (INDEX NO. 20072)

SECTION PROPERTIES	
1,058.58	
278.57	
740,895	
82,187	
40.09	
31.91	



F.I.B.-78 (INDEX NO. 20078)

PROPERTIES
1,100.58
290.57
904,567
82,367
43.40
34.60

