## 212 Intersections

### 212.1 General

This chapter provides design criteria and guidance for the geometric layout of at-grade conventional intersections. Conventional intersections include 3-leg (T), 4-leg, and Multileg (5 or more legs).

Multi-leg conventional intersections should be avoided. Alternatives to existing multi-leg intersections include:
(1) Converting to a roundabout.
(2) Converting one or more legs to a one-way operation
(3) Reconfiguring or realigning the intersection to create separate intersections, each with no more than four legs.

See FDM 201 for design vehicle selection and design speed requirements.
See FDM 210 for lane width, median width, island dimensions, and deflection angle requirements.

See FDM 222 for requirements concerning pedestrian facilities and FDM 223 for bicycle facilities.

### 212.1.1 Alternative Intersections

Alternative intersection design is a key component of upgrading our transportation facilities and improving the mobility and safety of all road users. These innovative designs are becoming more common as increasing traffic demand exceed the limitations of traditional intersection solutions.

Alternative intersections offer the potential to improve safety and reduce delay at lower cost and with fewer impacts than traditional solutions such as adding lanes or grade separation. Three of the more common alternative intersection types are:

- Displaced Left Turn (a.k.a. Continuous Flow Intersection)
- Restricted Crossing U-Turn (RCUT)
- Median U-Turn (MUT)

The FHWA has published comprehensive informational guides for alternative intersections which include guidance on how to plan, design, construct, and operate them. The following links provide access to these guides: FHWA Alternative Designs and Alternative Intersections/Interchanges: Informational Report (AIIR).

These types of alternate intersection designs should be coordinated with the Central Office Roadway Design.

### 212.1.2 Intersection Control Evaluation

Intersection Control Evaluation (ICE) is a process to determine the most effective intersection configuration for a specified project. Through ICE, multiple alternative and conventional intersection configurations are compared to one another based on safety, operations, cost, and environmental impacts. The ICE procedure provides a transparent and consistent approach to intersection alternatives selection and provides documentation to support decisions made.

ICE policy and procedure is published on the FDOT Traffic Engineering and Operations Office website at the following Link: Manual on Intersection Control Evaluation.

### 212.2 Intersection Control

Conventional intersections utilize one of four control types; yield, stop, all-way stop and signal.

### 212.2.1 Yield Control

Certain channelized movements at intersections and interchanges, and all approaches to roundabouts are often yield controlled. Refer to the Manual on Uniform Traffic Control Devices (MUTCD) for information on the locations where yield control traffic control devices may be appropriate.

### 212.2.2 Stop Control

Stop-controlled intersections have one or more legs of the intersection controlled by a "STOP" sign (R1-1).

Intersections with stop control are a common, low-cost control, which require the traffic on the minor roadway to stop before entering the major roadway. It is used where
application of the normal R/W rule is not appropriate for certain approaches at the intersection.

To meet the requirements for the assigned access classification, or where U-turn opportunities exist within a corridor, consider limiting stop controlled minor roads or driveways to "right-in, right-out" only.

### 212.2.3 All-Way Stop Control

For an all-way stop intersection, traffic approaching it from all directions is required to stop before proceeding through the intersection. An all-way stop may have multiple approaches and typically marked with a supplemental signing stating the number of approaches.

All-way stop control is most effective at the intersection of low-speed, 2-lane roadways not exceeding 1,400 vehicles during the peak hour. All-way stop control should not be used on multilane highways. Guidance for consideration of the application of all-way stop control is provided in the MUTCD.

All-way stop control may be used as an interim measure when a traffic signal or roundabout is warranted, but the installation is delayed.

### 212.2.4 Signal Control

Signalization provides an orderly and predictable movement of motorized and nonmotorized traffic throughout the highway transportation system. It also provides guidance and warnings to ensure the safe and informed operation of the traffic stream.

Refer to FDM 232 for design criteria for signalization.

### 212.3 Intersection Types

Conventional intersection configurations include flared and channelized intersections (divided and undivided). Flared intersections are illustrated in Figure 212.3.1 and channelized intersections in Figure 212.3.2. See FDM 210.3 for median and island requirements.

## Figure 212.3.1 Flared Intersections



Figure 212.3.2 Channelized Intersections


### 212.4 Intersection Functional Area

The functional area of an intersection extends in both directions including auxiliary lanes and their associated channelization. This is illustrated in Figures 212.4.1 and 212.4.2.

The functional area on the approach to an intersection or driveway consists of three basic elements:
(1) Perception-reaction-decision distance
(2) Maneuver distance
(3) Queue-storage distance (see FDM 212.14.2)

These elements are shown in Figure 212.4.3. The maneuver distance includes the length needed for both braking and lane changing when there is a left or right turning lane. In the absence of turn lanes, the maneuver distance is the distance to brake to a comfortable stop. The storage length includes the most distant extent of any intersectionrelated queue expected to occur during the design period.

Figure 212.4.1
Physical Definition


Ref: Figure 9-2, 2018 AASHTO Green Book

Figure 212.4.2
Functional Definition


Ref: Figure 9-2, 2018 AASHTO Green Book

Figure 212.4.3 Elements of the Functional Area


### 212.5 Intersection Angle

The intersection angle between two roadways has a significant influence on the safety and operation of an intersection. Intersection angles are to be as close to 90 degrees as practical. Intersection angles less than 75 degrees should be avoided for the following reasons:
(1) Heavy skew angles increase the intersection crossing length, exposing vehicles, pedestrians, and cyclists to conflicting traffic streams for longer periods of time. This is of particular concern at stop-controlled approaches on high-speed facilities.
(2) The road user's sight angle to the crossing leg becomes restricted due to the skew, making it difficult to see conflicting vehicles and to perceive safe crossing gaps.
(3) Turning movements are difficult because of the skew. Additional pavement may be necessary to accommodate the turning of large trucks.
(4) Turning movements or positioning may be confusing and require additional channelization.
(5) Increased open pavement areas of highly skewed intersections increase construction and maintenance costs.

Evaluate intersections with severe skew angles and crash histories for geometric improvements as shown in Figure 212.5.1. A high incidence of right-angle crashes is an indicator that improvements may be justified.

Figure 212.5.1 Intersection Reconfigurations


### 212.6 Lane Tapers

Standard taper lengths for auxiliary lanes are given in FDM 212.14. Taper length is based on the following equations:
(1) Merging Taper (L):
(a) For design speeds $\leq 40 \mathrm{mph}: \mathrm{L}=\left(\mathrm{W}^{*} \mathrm{~S}^{2}\right) / 60$
(b) For design speeds $\geq 45 \mathrm{mph}: \mathrm{L}=\mathrm{W} * \mathrm{~S}$

Where:

$$
\begin{aligned}
& \text { L = Taper length (feet) } \\
& \text { W = Width of offset (feet) } \\
& \text { S = Design speed (mph) }
\end{aligned}
$$

(2) Shifting Taper is equal to Merging Taper (L) / 2.

Minimum deceleration lengths are illustrated in Exhibit 212-1. Additional information on lane transitions (add or drop) are provided in Exhibits 212-2 and 212-3.


Brakes Applied After Turning
Vehicle Clears Through Lane
Entry Speed:
Entry Speed:
10 mph Below
For Urban Condition
Average Running Speed For
Rural Condition

| MEDIAN TURN LANES |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design Speed (mph) | $\begin{aligned} & \text { Entry } \\ & \text { Speed } \\ & \text { (mph) } \end{aligned}$ | Clearance Distance $L_{1}(f t$.) | URBAN CONDITIONS |  |  | RURAL CONDITIONS |  |  |
|  |  |  | $\begin{array}{\|c\|} \hline \text { Brake To } \\ \text { Stop } \\ \text { Distance } \\ L_{2} \text { (ft.) } \\ \hline \end{array}$ | Total Decel. Distanc $L$ (ft.) | $\begin{gathered} \text { Clearance } \\ \text { Distance } \\ L_{3}(f t .) \end{gathered}$ | $\begin{array}{\|l\|} \hline \text { Brake To } \\ \text { Stop } \\ \text { Sistance } \\ L_{2} \text { (ft.) } \end{array}$ | $\begin{array}{\|c\|} \hline \text { Total } \\ \text { Decel. } \\ \text { Distance } \\ \text { L (ft.) } \end{array}$ | $\begin{gathered} \text { Clearance } \\ \text { Distance } \\ L_{3} \text { (ft.) } \end{gathered}$ |
| 35 | 25 | 70 | 75 | 145 | 110 | - | - |  |
| 40 | 30 | 80 | 75 | 155 | 120 | - | - | - |
| 45 | 35 | 85 | 100 | 185 | 135 | - | - | - |
| 50 | $40 / 44$ | 105 | 135 | 240 | 160 | 185 | 290 | 160 |
| 55 | 48 | 125 | - | - | - | 225 | 350 | 195 |
| 60 | 52 | 145 | - | - | - | 260 | 405 | 230 |
| 65 | 55 | 170 | - | - | - | 290 | 460 | 270 |


two-way left-turn lanes

| $\begin{aligned} & \text { DESIGN } \\ & \text { SPEED } \\ & \text { (mph) } \end{aligned}$ | $T_{a}$ (ft.) | $T_{d}$ |
| :---: | :---: | :---: |
| <30 | 1:4, 50 ft . min. | 1:25 |
| 30-45 |  | 1:30 |
| >45 |  | 1:40 |
| Note: For locations with unrelocatable control points minimum taper rates for lane drop $\left(T_{d}\right)$ will be 1:20. |  |  |



UNDIVIDED FLARED - SYMMETRICAL

flared \& painted left turns for 2-lane roadways

| DESIGN SPEED (mph) | $L_{a}(F t$. |  | $L_{d}(F t$. |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Standard | MINIMUM UNDER CONSTRAINTS | Standard | MINIMUM UNDER CONSTRAINTS |
| 30 | 180 | 120 | 180 | 120 |
| 40 | 320 | 150 | 240 | 150 |
| 50 | 500 | 180 | 360 | 180 |
| 60 | 720 | 240 | 480 | 240 |

### 212.7 Lane Shifts

Lane shifts through intersections should meet the requirements for non-merging conditions. Pavement markings should be used through the intersection to provide positive guidance to the motorist. The shifting taper length is controlled by the size of the intersection and the deflection angle. Although deflections through intersections are discouraged, there may be conditions where they are necessary.

The maximum deflection angles at intersections to be used in establishing the horizontal alignment are given in Table 212.7.1.

Table 212.7.1 Maximum Deflection Angle Through Intersection

| Maximum Deflection Angle Through Intersection (DM) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Design Speed (mph) |  |  |  |  |  |
| $\leq 20$ | 25 | 30 | 35 | 40 | 45 |
| $16^{\circ} 00^{\prime}$ | $11^{\circ} 00^{\prime}$ | $8^{\circ} 00$ | $6^{\circ} 00^{\prime}$ | $5^{\circ} 00$ | $3^{\circ} 00$ |
| Notes: <br> Deflection angle used is not to cause a lane shift (W) of more than 6 feet from stop bar to stop bar. |  |  |  |  |  |
|  |  |  |  | HROUGH ION <br> ection an |  |

### 212.8 Profile Grades

The profile grade line defines the vertical alignment for construction. The grade line of the mainline road is typically carried through the intersection and the minor crossroad (or cross street) is adjusted to it. This design involves a transition in the crown of the crossroad to an inclined cross section at its junction with the mainline road, as illustrated in Figure 212.8.1.

The break in the crossroad profile at the center of the intersection should be accomplished with a vertical curve.

Vertical alignments at or near intersections should provide traffic lanes that are:
(1) Clearly visible and understandable to drivers for any desired direction of travel,
(2) Free from sudden appearance of potential conflicts, and
(3) Consistent in design with the portions of the highway just traveled.

Steep grades at intersections may increase or decrease stopping or acceleration distance. Avoid grades in excess of $3 \%$ on intersecting roads in the vicinity of the intersection. Where conditions make such designs impractical, grades should not exceed 6\%.

Provide adequate sight distance along both intersecting roads and across their included corners, even where one or both intersecting roads are on vertical curves. The gradients of intersecting roads should be as flat as practical on those sections that are to be used for storage of stopped vehicles.

Figure 212.8.1 Cross Street Intersection Transition



### 212.8.1 Special Profiles

Special profiles for certain roadway elements may be necessary to ensure a safe, efficient, well-drained and smooth roadway system. Elements that may require special profiles include pavement edges or gutter flow lines at street intersections, profile grade lines, intersection plateaus, curb returns, and special superelevation details. Special profiles are developed at close intervals and large scale to clearly identify all construction details of these elements.

### 212.8.2 Plateauing

In some instances, it is desirable for the crossroad to receive the same profile considerations as the mainline road. To provide this "equal treatment", with respect to profile, a technique commonly known as intersection plateauing is applied. Plateauing refers to flattening of the intersection and the transition of both roadway profiles and cross slopes on the intersection approaches.

Provide a profile combination that provides a smooth transition and adequate drainage when applying intersection plateauing. Transition slope rates are to meet the values provided in Table 212.8.1; however, the minimum length of cross slope transition is 50 feet for design speeds less than or equal to 35 mph and 75 feet for design speeds of 40 mph or greater.

An example of a plateaued intersection is illustrated in Figure 212.8.2.

Table 212.8.1 Slope Rates for Intersection Approaches

| Design Speed (mph) | Slope Ratio |
| :---: | :---: |
| $25-35$ | $1: 100$ |
| 40 | $1: 125$ |
| $45-50$ | $1: 150$ |
| $55-60$ | $1: 170$ |
| $65-70$ | $1: 190$ |

Figure 212.8.2 Example of Plateaued Intersection


### 212.9 Median Openings

Locate and design median openings to meet traffic requirements in accordance with the access management plan for the facility. See FDM 201.4 for more information on access management plans and decision making.

See FDM 210.3 for additional requirements for medians at intersections.
The following conditions may require additional median width:

- accommodation for trees (provide space above and below ground for growth)
- offset turn lanes
- directional median openings
- dual and triple left turn lanes

The overall length of a full median opening is typically the same width as the intersecting road (including shoulders) which is sufficient to accommodate the swept path of left turning vehicles. Median functions and minimum widths are provided in Table 212.9.1.

For un-signalized intersections, median openings should not be longer than the required length to avoid multiple vehicles attempting to stop within the opening.

Table 212.9.1 Minimum Median Width

| Median Function | Minimum Width (feet) |
| :--- | :---: |
| Separation of opposing traffic | 4 |
| Provision for pedestrian refuge | 6 |
| Provision for storage of left-turning vehicles | See Table 210.3.1 |
| Provision for protection of vehicles crossing through lanes | 22 |
| Provision for U-turns, left turn lane to outside lanes | 30 |
| Provision for Dual Left Turn Lanes and U Turns | 42 |

The control radius refers to a radius that must be considered in establishing the location of median or traffic separator ends on divided highways and the stop bar on undivided highways. Provide this radius for left-turn movements when appropriate.

Design guidance on minimum edge-of-traveled-way design for various design vehicles is provided in FDM 212.12.1.

For the central part of the turn the use of compound curves is not necessary and the use of simple curves is satisfactory. Table $\mathbf{2 1 2 . 9 . 2}$ provides control radii for minimum-speed turns (10 to 15 mph ) that can be used for establishing the location of the median ends.

Table 212.9.2 Control Radii for Minimum Speed Turns

| Design Vehicles <br> Accommodated | Control Radius (feet) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $50(40 \mathrm{~min})$ | $60(50 \mathrm{~min})$ | 75 | 130 |
| Predominant | P | $\mathrm{SU}-30$ | $\mathrm{SU}-40, \mathrm{WB}-40$ | WB-62FL |
| Occasional | SU-30 | $\mathrm{SU}-40, \mathrm{WB}-40$ | WB-62 | WB-67 |

### 212.9.1 U-Turns

Median width should accommodate passenger vehicle (P) left-turn and U-turn maneuvers. If adequate median width does not exist for accommodating U-turns, then consider adding extra pavement width such as a taper or additional shoulder width. See FDM 210.3 for information on median width criteria.

In cases where U-turn traffic volumes are high, consider the use of jug handles, loop designs, or indirect left turn designs.

### 212.10 Stopping Sight Distance

See FDM 210.11.1 for stopping sight distance requirements.

### 212.11 Clear Sight Triangles

Establish clear sight triangles to assure that drivers are provided a sufficient view of the intersecting highway to identify gaps in traffic and decide when it is safe to proceed. Document the analysis of sight distance for all intersections.

Clear sight triangles are the areas along intersection approach legs and across their common corners that should be clear of visual hindrances. Dimensions of clear sight triangles are based on design speed, design vehicle, and the type of traffic control used at the intersection.

### 212.11.1 Stop Control (AASHTO Case B)

Figure 212.11.1 illustrates clear sight triangles for intersections and driveways.

Figure 212.11.1 Clear Sight Triangles


The minimum driver-eye setback of 14.5 feet from the edge of the traveled way may be adjusted on any intersection leg only when justified by a documented, site-specific field study of vehicle stopping position and driver-eye position.

Exhibits 212-4 through 212-7 provide intersection sight distances for stop-controlled intersections. The tables in the exhibits provide sight distance values for Passenger vehicles, Single Unit (SU) Trucks, and Combination vehicles for design speeds ranging from 30 mph to 65 mph . Intersection sight distance based on Passenger vehicles is suitable for most intersections; however, consider the values for SU Vehicles or Combination vehicles for intersections with high truck volumes.

The following guidance applies to Exhibits 212-4 through 212-7:

## (1) Limitations

(a) The exhibits apply to intersections in all context classifications with stop control or flashing beacon control.
(b) The exhibits apply only to intersections with intersecting angles between $60^{\circ}$ and $120^{\circ}$, and where vertical and horizontal curves are not present.
(2) Dimensions
(a) Sight distance (d) is measured from the center of the entrance lane of the crossroad to the center of the near approach lane (right or left) of the highway.
(b) Distances 'dl' and 'dr' are measured from the centerline of the entrance lane of the crossroad to a point on the edge of the near side outer traffic lane on the highway.
(c) Distance ' $\mathrm{d}_{\mathrm{m}}$ ' is measured from the centerline of the entrance lane of the crossroad to a point on the median clear zone limit or horizontal clearance limit for the far side road of the highway.
(3) Vertical limits
(a) Provide a clear sight window throughout the limits of all intersection sight triangles.
(b) Provide a clear line of sight between vehicles at intersection stop locations and vehicles on the highway throughout the limits of all intersection sight triangles.
(c) The reference datum between roadways is $3^{\prime}-6$ " above respective pavements since observations are made in both directions along the line of sight.

## intersection sight distance: 2-LANE undivided



2-LaNe with left turn lane

| $\begin{array}{\|c} \hline \text { Design } \\ \text { Speed } \\ \text { (mph) } \end{array}$ | (Ft.) | $\begin{gathered} { }_{c}^{d}, \\ (F t .) \end{gathered}$ | $\begin{aligned} & a_{r} \\ & (f t .) \end{aligned}$ | $\begin{gathered} \text { Desigg } \\ \text { Speed } \\ \text { (mph } \end{gathered}$ | $\begin{gathered} d \\ (\mathrm{Ft} .) \end{gathered}$ | $\begin{gathered} d_{1} \\ \left(F L_{1}\right) \end{gathered}$ | $\begin{aligned} & \boldsymbol{c}_{r} \\ & (F t .) \end{aligned}$ | $\begin{array}{\|c} \hline \text { Design } \\ \text { Speed } \\ \text { (mph) } \end{array}$ | $\begin{gathered} d \\ (f t .) \end{gathered}$ | $\begin{gathered} d_{L} \\ (F t .) \end{gathered}$ | [ ${ }_{\text {d }}^{\substack{\text { d } \\ \text { (ft.) }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\leq 25$ | 295 | 165 | 115 | $\leq 25$ | 375 | 205 | 145 | $\leq 25$ | 450 | 250 | 170 |
| 30 | 355 | 195 | 135 | 30 | 450 | 250 | 170 | 30 | 540 | 295 | 205 |
| 35 | 415 | 230 | 160 | 35 | 525 | 290 | 200 | 35 | 630 | 345 | 240 |
| 40 | 475 | 260 | 180 | 40 | 600 | 330 | 230 | 40 | 720 | 395 | 275 |
| 45 | 530 | 290 | 200 | 45 | 675 | 370 | 255 | 45 | 810 | 445 | 305 |
| 50 | 590 | 325 | 225 | 50 | 750 | 410 | 285 | 50 | 900 | 495 | 340 |
| 55 | 650 | 355 | 245 | 55 | 825 | 455 | 315 | 55 | 990 | 545 | 375 |
| 60 | 710 | 390 | 270 | 60 | 900 | 495 | 340 | 60 | 1080 | 590 | 410 |
| 65 | 765 | 420 | 290 | 65 | 975 | 535 | 370 | 65 | 1170 | 640 | 440 |
| 70 | 825 | 455 | 315 | 70 | 1050 | 575 | 395 | 70 | 1260 | 690 | 475 |
| Passenger Vehicle |  |  |  | su venicle |  |  |  | Combination Vehicle |  |  |  |

SIGHT DISTANCE (d) AND RELATED DISTANCES ( $d_{L}, d_{r}$ ) (FEET)
2-LANE WITH LEFT TURN

## INTERSECTION SIGHT DISTANCE: 4-LANE UNDIVIDED



SIGHT DISTANCE (d) AND RELATED DISTANCES ( $d_{L}, d_{r}$ ) (FEET)

| $\begin{array}{\|c\|} \hline \text { Design } \\ \text { Speed } \end{array}$ | ${ }_{d}$ | ${ }_{L}$ | ${ }^{\text {d }}$ | $\begin{array}{\|c\|c\|} \hline \text { Design } \\ \text { Speed } \end{array}$ | ${ }^{\text {d }}$ | ${ }_{L}$ | ${ }^{d}$ | $\begin{array}{\|c\|} \hline \text { Design } \\ \text { Speed } \end{array}$ | ${ }^{\text {d }}$ | ${ }^{\text {d }}$ | ${ }^{\text {d }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (mph) | (Ft.) | (Ft.) | (Ft.) | (mph) | (Ft.) | (rt.) | $\frac{\text { fr.) }}{}$ | (mph) | (Ft.) | (Ft.) | $\frac{\text { frt) }}{}$ |
| $\leq 25$ | 315 | 175 | 90 | $\leq 25$ | 400 | 220 | 115 | $\leq 25$ | 475 | 260 | 140 |
| 30 | 375 | 205 | 110 | 30 | 480 | 265 | 140 | 30 | 570 | 315 | 165 |
| 35 | 440 | 245 | 130 | 35 | 560 | 310 | 165 | 35 | 665 | 365 | 195 |
| 40 | 500 | 275 | 145 | 40 | 640 | 350 | 185 | 40 | 760 | 420 | 220 |
| 45 | 565 | 310 | 165 | 45 | 720 | 395 | 210 | 45 | 855 | 470 | 245 |
| 50 | 625 | 345 | 180 | 50 | 800 | 440 | 230 | 50 | 950 | 520 | 275 |
| 55 | 690 | 380 | 200 | 55 | 880 | 485 | 255 | 55 | 1045 | 575 | 300 |
| 60 | 750 | 410 | 215 | 60 | 960 | 525 | 280 | 60 | 1140 | 625 | 330 |
| 65 | 815 | 450 | 235 | 65 | 1040 | 570 | 300 | 65 | 1235 | 675 | 355 |
| 70 | 875 | 480 | 255 | 70 | 1120 | 615 | 325 | 70 | 1330 | 730 | 385 |

SIGHT DISTANCE (d) AND RELATED DISTANCES ( $d_{L}, d_{r}$ ) (FEET) 4-LANE UNDIVIDED WITH LEFT TURN LANE



4-LaNe undivided with left turn lane and optional lane

1. See Figure 212.11.1 for origin of clear sight line on the minor road.


SIGHT DISTANCE (d) AND RELATED DISTANCES ( $d_{l}, d_{r}$ ) (FEET) 4-LaNe undivided with left turn lane and optional lane

## INTERSECTION SIGHT DISTANCE: 4-LANE DIVIDED



Passenger Vehicle


| 40'-64' Median |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Design } \\ & \text { Speed } \end{aligned}$ (mph) | (Ft.) |  | $\left.\begin{array}{c} c_{b}^{d} \\ (F t .) \end{array}\right)$ | Ft. |
| $\leq 25$ | 375 | 270 | 350 | 260 |
| 30 | 450 | 320 | 420 | 310 |
| 35 | 525 | 375 | 490 | 360 |
| 40 | 600 | 425 | 560 | 410 |
| 45 | 675 | 480 | 630 | 460 |
| 50 | 750 | 530 | 700 | 510 |
| 55 | 825 | 585 | 770 | 560 |
| 60 | 900 | 640 | 840 | 610 |
| 65 | 975 | 690 | 910 | 660 |
| 70 | 1050 | 745 | 980 | 71 |

sU Vehicle


4-LANE DIVIDED


Where The Median Is Sufficiently Wide For The Design Vehicle To Pause In The Median (Vehicle Length Plus 6' Min.) The Clear Line of Sight To The Right ( $d_{v}$ ) Is Measured From The Vehicle
Pause Location, i.e., Not From The Cross Road Stop Position; Distances $d_{r} \& d_{m}$ Do Not Apply

INSET A


NOTES FOR 4-LANE DIVIDED ROADWAY

1. See Figure 212.11.1 for origin of clear
sight line on the minor road.
2. Values shown in the tables are the governing (controlling) sight distances calculated based on 'AASHTO Case B inter section with Stop Control on the


INSET B
Lateral Offset For Restricted Conditions
Clear Zone For Nonrestricted Conditions

Minor Road.'



Combined Vehicles

## INTERSECTION SIGHT DISTANCE: 6-LANE DIVIDED



Passenger Vehicle

| Median 35' or Less |  |  |  |  | $40^{\prime}-64^{\prime}$ Median |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c} \hline \text { Design } \\ \text { Speed } \\ \text { (mph) } \\ \hline \end{array}$ | $\begin{gathered} c \\ (F t) \\ (F) \end{gathered}$ | $\begin{gathered} a_{i}^{d} \\ (F t .) \end{gathered}$ | $\left.\begin{array}{c} d_{r} \\ (F t .) \end{array}\right)$ | $\begin{gathered} d_{m} \\ (\text { (t.) }) \end{gathered}$ | $\begin{array}{\|c} \hline \text { Design } \\ \text { Speed } \\ \text { (mph) } \end{array}$ | $\left.\begin{array}{c} c \\ (F t .) \end{array}\right)$ | $\left.\begin{array}{c} d_{1}, \\ (F t .) \end{array}\right)$ | $\begin{array}{\|c} a_{v} \\ (F t .) \end{array}$ | $\begin{aligned} & d_{V L L} \\ & (F t .) \end{aligned}$ |
| $\leq 25$ | 475 | 340 | 75 | 415 | $\leq 25$ | 400 | 285 | 350 | 250 |
| 30 | 570 | 405 | 90 | 495 | 30 | 480 | 340 | 420 | 300 |
| 35 | 665 | 470 | 105 | 580 | 35 | 560 | 400 | 490 | 350 |
| 40 | 760 | 540 | 120 | 660 | 40 | 640 | 455 | 560 | 400 |
| 45 | 855 | 605 | 135 | 745 | 45 | 720 | 510 | 630 | 450 |
| 50 | 955 | 675 | 155 | 830 | 50 | 805 | 570 | 700 | 500 |
| 55 | 1050 | 745 | 170 | 915 | 55 | 885 | 625 | 770 | 550 |
| 60 | 1145 | 810 | 185 | 995 | 60 | 965 | 685 | 840 | 600 |
| 65 | 1240 | 880 | 200 | 1080 | 65 | 1045 | 740 | 910 | 650 |
| 70 | 1330 | 940 | 210 | 1155 | 70 | 1125 | 795 | 980 | 700 |

su Vehicle

| Median $30^{\prime}$ or Less |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c} \hline \text { Design } \\ \text { Speed } \\ \text { (mph }) \\ \hline \end{array}$ | $\left.\begin{array}{c} d_{x} \\ (F t .) \end{array}\right)$ | $\left.\begin{array}{c} d_{L} \\ (F t .) \end{array}\right)$ | $\begin{array}{\|c\|c} a_{r} \\ (F t .) \end{array}$ | ${ }_{\substack{d_{\text {m }} \\ \text { ft. } \\ \hline \\ \hline}}$ |
| $\leq 25$ | 540 | 385 | 90 | 65 |
| 30 | 650 | 460 | 110 | 560 |
| 35 | 755 | 535 | 130 | 655 |
| 40 | 865 | 615 | 145 | 45 |
| 45 | 970 | 69 | 165 | 835 |
| 50 | 108 | 765 | 185 | 930 |
| 55 | 118 | 840 | 200 | 1025 |
| 60 | 1290 | 915 | 220 | 1115 |
| 65 | 1400 | 990 | 23 | 1210 |
| 70 | 1510 | 1070 | 255 | 130 |



Combined Vehicles


6-LANE DIVIDED

here The Median Is Sufficiently wide For The Design Vehicle To Pause In The Median (Vehicle


INSET A


NOTES FOR 6-LANE DIVIDED ROADWAY
See Figure 212.11.1 for origin of clear sight line on the minor road.
2. Values shown in the tables are the governing (controlling) sight distances
calculated based on 'AASHTO Case B Intersection with Stop Control on the Minor Road.'

### 212.11.2 All-Way Stop Control (AASHTO Case E)

Provide clear sight lines on each of the approach legs for all-way stop controlled intersections.

### 212.11.3 Signal Control (AASHTO Case D)

For signalized intersections incorporate the following:
(1) Develop sight distances based on AASHTO ‘Case D-Intersections with Signal Control'.
(2) The first vehicle stopped on any approach leg is visible to the driver of the first vehicle stopped on each of the other approach legs.
(3) For permissive left turns provide sufficient sight distance for left turning vehicles to select gaps in oncoming traffic and complete left turns.
(4) If a traffic signal is to be placed on two-way flashing operation (i.e., flashing yellow on the major road approaches and flashing red on the minor road approaches) under off peak or nighttime conditions, then provide the appropriate departure sight triangles for AASHTO Case B (Stop Control on the Minor Road).
(5) If right turns on red are permitted from any approach leg, then provide the appropriate departure sight triangle to the left for AASHTO Case B above.

### 212.11.4 Left Turn from Highway (AASHTO Case F)

Provide sufficient sight distance to accommodate a left turn maneuver for locations where left turns across opposing traffic are permitted. Table 212.11.1 provides clear sight distance values for left turn from highway.

For additional information on determining the sight distance refer to Chapter 9 of AASHTO's A Policy on Geometric Design of Highways and Streets.

Table 212.11.1 Sight Distance for Left Turn from Highway


## Notes:

(1) Provide a lateral offset (LO) of 6 ' as shown in the diagram above. $\mathrm{d}_{\mathrm{b}}$ may be determined by the equation $d_{b}=d_{a}(w /(w+12))$. For roadways with non-restricted conditions, $d_{a}$ and $d_{b}$ should be based on the geometry for the left turn storage and on clear zone widths.
(2) For wide medians where the turning vehicle can approach the through lane at or near $90^{\circ}$, use d values from tables in Exhibits 212-6 and 212-7. (The clear sight line origin is assumed to be 14.5 feet from the edge of the near travel lane.

### 212.11.5 On-Street Parking

Table 212.11.2 provides parking restrictions for intersections, including mid-block crossings and roundabout approaches. For additional information, see the following:

- FDM 210.2.3 for additional information concerning on-street parking.
- FDM 222.2.6 for information concerning curb extensions (bulb-outs).
- Chapter 316, Florida Statutes (F.S.), for laws governing parking spaces.

Table 212.11.2 Parking Restrictions for Driveways and Intersections


## Notes:

(1) For entrances to one-way streets, the downstream restriction (B) may be reduced to 20 feet.
(2) Do not place parking within 20 feet of a marked crosswalk.

### 212.11.6 Trees and Vegetation

Intersections should be designed to accommodate the placement of trees and other desired vegetation (e.g., ground cover plants, trunked plants) in C2T, C3C, C4, C5, and C6 context classifications while still maintaining clear sight triangles. Ground cover plants are naturally low-growing plants with a maximum mature height of $\leq 18$ inches. Trunked plants are those with a mature trunk diameter of 4 inches or less (measured 6 inches above the ground).

Maintain clear sight triangles for all approaches. Do not place trees within the hatchedout areas as shown in Figure 212.11.2. The hatched-out areas are for ground cover plants only. Coordinate with the Project Landscape Architect for the placement of vegetation and the necessary space above and below ground for tree growth that will maintain clear sight triangles.

Figure 212.11.2 Special Areas Limited to Ground Cover Plants


Where left turns from the major road are permitted, do not locate trees within the distance $d_{b}$ shown in Table 212.11.1 (see FDM 212.11.4) and not less than the distances shown in Figure 212.11.2 and the spacings in Table 212.11.3 as applicable.

### 212.11.6.1 Clear Sight Window Concept

The clear sight window concept may provide opportunities for vegetation within the limits of intersection sight triangles. This concept is illustrated in Figure 212.11.3. This detail provides the required vertical clear sight limits with respect to the sight line datum. Do not place trees within the hatched-out areas as shown in Figure 212.11.2 (even if using the clear sight window concept). The hatched-out areas are for ground cover plants only.

Figure 212.11.3 Window Detail


* Since observations are made in both directions, the line-of-sight datum between roadways is 3.5 feet above both pavements.

The horizontal limits of the window are defined by clear sight triangles. Within the limits of clear sight triangles, the following restrictions apply:

- Canopy of trees and trunked plants must be at least 5 feet above the sight line datum.
- The top of the ground cover plants must be at least 1.5 feet below the sight line datum.

See FDM 228.2(2)(a) for additional information about plant selection and placement. Enforcing these limits provides a clear line of sight for approaches to an intersection.

When trees are located in the median of a divided roadway and fall within the limits of a clear sight triangle, conform to Table 212.11.3 for tree size and spacing. Spacing values for trees with diameter of 11 inches or less were derived assuming a maximum 6-footwide shadow band on a vehicle at the stop bar location when viewed by a mainline driver beginning at sight distance ' $d$ '. This is illustrated in Figure 212.11.4. Spacing values for
trees with diameter greater than 11 inches and less than or equal to 18 inches were derived assuming a 2 second full view of the vehicle at the stop bar when viewed by the mainline driver beginning at sight distance ' $d$ '. (See Figure 212.11.5).

Table 212.11.3 Minimum Tree Spacing

| Design Speed <br> (mph) | Minimum Tree Spacing <br> (Center-to-Center of Trunk) <br> (feet) |  |
| :---: | :---: | :---: |
|  | $4 "<$ Tree Diameter $\leq 11^{\prime \prime}$ | $11^{\prime \prime}<$ Tree Diameter $\leq 18^{\prime \prime}$ |
| 25 | 20 | 75 |
| 30 | 25 | 90 |
| 35 | 30 | 105 |
| 40 | 35 | 120 |
| 50 | 40 | 135 |
| 55 | 50 | 160 |
| 60 | 55 | 180 |

## Notes:

(1) Size and spacing are based on the following conditions:
(a) A single line of trees in the median parallel to but not necessarily collinear with the centerline.
(b) A straight approaching mainline and intersection angle between $60^{\circ}$ and $120^{\circ}$.
(c) Space trees with 4 " $<$ Dia. $\leq 11^{\prime \prime}$ intermixed with trees with $11^{\prime \prime}<$ Dia. $\leq 18^{\prime \prime}$ based on trees with $11^{\prime \prime}<$ Dia. $\leq 18^{\prime \prime}$.
(2) Detail tree size, spacing, and location in the plans for any other conditions.
(3) Trunked Plants may be placed on 20 -foot centers.

Figure 212.11.4 Shadow Diagram


Figure 212.11.5 Perception Diagram


### 212.12 Turning Roadways

Turning roadways are typically designed for use by right-turning traffic at intersections. There are three types of right-turning roadways:

- edge-of-traveled-way design
- design with a corner triangular island
- free-flow design using a simple radius or compound radii

The turning radii and the pavement cross slopes for free-flow right turns are functions of design speed and design vehicle.

### 212.12.1 Edge-of-Traveled-Way Design

When selected design vehicle is to be accommodated within minimum space, corner radii should be based on the required turning path.

Table 212.12.1 provides simple curve radii with and without tapers. Table 212.12.2 provides symmetric and asymmetric three centered compound curve radii for a range of design vehicles. These values provide the minimum turning paths attainable at design speeds of 10 mph and less.

Figure 212.12.1 demonstrates the angle of turn for use in these tables.
The minimum edge-of-traveled-way values provided in these tables are based on the assumption that the vehicle is properly positioned within the traffic lane at the beginning and end of the turn ( 2 feet from the edge-of-traveled-way on the tangents approaching and leaving the intersection curve). Such designs follow closely the inner wheel path of the selected design vehicle, with a clearance of 2 feet or more throughout most of the turn, and with a clearance at no point less than 9 inches. Differences in the inner paths of vehicles turning left and right are not sufficient to be significant in design. For this reason, these edge designs also apply to left-turn maneuvers, such as a left turn by a vehicle leaving a divided highway at a very low speed.

Figure 212.12.1 Turn Angle for Turning Roadway Designs


Table 212.12.1 Edge-of-Traveled-Way, Simple Curve Radii

| Angle of Turn (degrees) | Design Vehicle | Simple Curve <br> Radius (feet) | Simple Curve Radius with Taper |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Radius (feet) | Offset (feet) | Taper H:V |
| 30 | P | 60 | ---- | --- | ---- |
|  | SU-30 | 100 | ---- | ---- | ---- |
|  | SU-40 | 140 | ---- | ---- | ---- |
|  | WB-40 | 150 | ---- | ---- | ---- |
|  | WB-62 | 360 | 220 | 3.0 | 15:1 |
|  | WB-62FL | 380 | 220 | 3.0 | 15:1 |
|  | WB-67 | 380 | 220 | 3.0 | 15:1 |
|  | WB-92D | 365 | 190 | 3.0 | 15:1 |
|  | WB-100T | 260 | 125 | 3.0 | 15:1 |
|  | WB-109D | 475 | 260 | 3.5 | 20:1 |
| 45 | P | 50 | ---- | ---- | ---- |
|  | SU-30 | 75 | -- | ---- | ---- |
|  | SU-40 | 115 | ---- | ---- | -- |
|  | WB-40 | 120 | ---- | -- | ---- |
|  | WB-62 | 230 | 145 | 4.0 | 15:1 |
|  | WB-62FL | 250 | 145 | 4.5 | 15:1 |
|  | WB-67 | 250 | 145 | 4.5 | 15:1 |
|  | WB-92D | 270 | 145 | 4.0 | 15:1 |
|  | WB-100T | 200 | 115 | 2.5 | 15:1 |
|  | WB-109D | ---- | 200 | 4.5 | 20:1 |
| 60 | P | 40 | ---- | ---- | ---- |
|  | SU-30 | 60 | -- | ---- | ---- |
|  | SU-40 | 100 | ---- | ---- | ---- |
|  | WB-40 | 90 | ---- | ---- | ---- |
|  | WB-62 | 170 | 140 | 4.0 | 15:1 |
|  | WB-62FL | 200 | 140 | 4.5 | 15:1 |
|  | WB-67 | 200 | 140 | 4.5 | 15:1 |
|  | WB-92B | 230 | 120 | 5.0 | 15:1 |
|  | WB-100T | 150 | 95 | 2.5 | 15:1 |
|  | WB-109D | ---- | 180 | 4.5 | 20:1 |

Table 212.12.1 Edge-of-Traveled-Way, Simple Curve Radii, cont.

| Angle of Turn (degrees) | Design <br> Vehicle | Simple Curve <br> Radius (feet) | Simple Curve Radius with Taper |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Radius (feet) | Offset (feet) | Taper H:V |
| 75 | P | 35 | 25 | 2.0 | 10:1 |
|  | SU-30 | 55 | 45 | 2.0 | 10:1 |
|  | SU-40 | 90 | 60 | 2.0 | 10:1 |
|  | WB-40 | ---- | 60 | 2.0 | 15:1 |
|  | WB-62 | ---- | 145 | 4.0 | 20:1 |
|  | WB-62FL | ---- | 145 | 4.0 | 20:1 |
|  | WB-67 | ---- | 145 | 4.5 | 20:1 |
|  | WB-92D | ---- | 110 | 5.0 | 15:1 |
|  | WB-100T | ---- | 85 | 3.0 | 15:1 |
|  | WB-109D | ---- | 140 | 5.5 | 20:1 |
| 90 | P | 30 | 20 | 2.5 | 10:1 |
|  | SU-30 | 50 | 40 | 2.0 | 10:1 |
|  | SU-40 | 80 | 45 | 4.0 | 10:1 |
|  | WB-40 | ---- | 45 | 4.0 | 10:1 |
|  | WB-62 | ---- | 120 | 4.5 | 30:1 |
|  | WB-62FL | ---- | 125 | 4.5 | 30:1 |
|  | WB-67 | ---- | 125 | 4.5 | 30:1 |
|  | WB-92D | ---- | 95 | 6.0 | 10:1 |
|  | WB-100T | ---- | 85 | 2.5 | 15:1 |
|  | WB-109D | ---- | 115 | 2.9 | 15:1 |
| 105 | P | ---- | 20 | 2.5 | 8:1 |
|  | SU-30 | ---- | 35 | 3.0 | 10:1 |
|  | SU-40 | ---- | 45 | 4.0 | 10:1 |
|  | WB-40 | ---- | 40 | 4.0 | 10:1 |
|  | WB-62 | -- | 115 | 3.0 | 15:1 |
|  | WB-62FL | ---- | 115 | 3.0 | 15:1 |
|  | WB-67 | ---- | 115 | 3.0 | 15:1 |
|  | WB-92B | ---- | 80 | 8.0 | 10:1 |
|  | WB-100T | ---- | 75 | 3.0 | 15:1 |
|  | WB-109D | ---- | 90 | 9.2 | 20:1 |

Table 212.12.1 Edge-of-Traveled-Way, Simple Curve Radii, cont.

| Angle of Turn (degrees) | Design Vehicle | Simple Curve Radius (feet) | Simple Curve Radius with Taper |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Radius (feet) | Offset (feet) | Taper H:V |
| 120 | P | ---- | 20 | 2.0 | 10:1 |
|  | SU-30 | ---- | 30 | 3.0 | 10:1 |
|  | SU-40 | ---- | 35 | 6.0 | 8:1 |
|  | WB-40 | ---- | 35 | 5.0 | 8:1 |
|  | WB-62 | ---- | 100 | 5.0 | 15:1 |
|  | WB-62FL | ---- | 105 | 5.2 | 15:1 |
|  | WB-67 | ---- | 105 | 5.2 | 15:1 |
|  | WB-92D | ---- | 80 | 7.0 | 10:1 |
|  | WB-100T | ---- | 65 | 3.5 | 15:1 |
|  | WB-109D | ---- | 85 | 9.2 | 20:1 |
| 135 | P | ---- | 20 | 1.5 | 10:1 |
|  | SU-30 | ---- | 30 | 4.0 | 10:1 |
|  | SU-40 | ---- | 40 | 4.0 | 8:1 |
|  | WB-40 | ---- | 30 | 8.0 | 15:1 |
|  | WB-62 | ---- | 80 | 5.0 | 20:1 |
|  | WB-62FL | ---- | 85 | 5.2 | 20:1 |
|  | WB-67 | ---- | 85 | 5.2 | 20:1 |
|  | WB-92D | ---- | 75 | 7.3 | 10:1 |
|  | WB-100T | ---- | 65 | 5.5 | 15:1 |
|  | WB-109D | ---- | 85 | 8.5 | 20:1 |
| 150 | P | - | 18 | 2.0 | 10:1 |
|  | SU-30 | ---- | 30 | 4.0 | 8:1 |
|  | SU-40 | ---- | 35 | 7.0 | 8:1 |
|  | WB-40 | ---- | 30 | 6.0 | 8:1 |
|  | WB-62 | ---- | 60 | 10.0 | 10:1 |
|  | WB-62FL | ---- | 65 | 10.2 | 10:1 |
|  | WB-67 | ---- | 65 | 10.2 | 10:1 |
|  | WB-92B | - | 65 | 11.0 | 10:1 |
|  | WB-100T | ---- | 65 | 7.3 | 10:1 |
|  | WB-109D | ---- | 65 | 15.1 | 10:1 |

Table 212.12.1 Edge-of-Traveled-Way, Simple Curve Radii, cont.

| Angle of Turn (degrees) | Design Vehicle | Simple Curve Radius (feet) | Simple Curve Radius with Taper |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Radius (feet) | Offset (feet) | Taper H:V |
| 180 | P | ---- | 15 | 0.5 | 20:1 |
|  | SU-30 | ---- | 30 | 1.5 | 10:1 |
|  | SU-40 | ---- | 35 | 6.4 | 10:1 |
|  | WB-40 | ---- | 20 | 9.5 | 5:1 |
|  | WB-62 | ---- | 55 | 10.0 | 15:1 |
|  | WB-62FL | ---- | 55 | 13.8 | 10:1 |
|  | WB-67 | ---- | 55 | 13.8 | 10:1 |
|  | WB-92D | ---- | 55 | 16.8 | 10:1 |
|  | WB-100T | ---- | 55 | 10.2 | 10:1 |
|  | WB-109D | ---- | 55 | 20.0 | 10:1 |

Table 212.12.2 Edge-of-Traveled-Way, 3-Centered Compound Curves

| Angle of Turn (degrees) | Design Vehicle | 3-Centered Compound Curve |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Curve Radif (ft) | Symmetric Offset (ft) | Curve Radif (ft) | Asymmetric <br> (ft) |
| 30 | P | ---- | ---- | ---- | ---- |
|  | SU-30 | ---- | ---- | ---- | ---- |
|  | SU-40 | ---- | ---- | ---- | ---- |
|  | WB-40 | ---- | ---- | ---- | ---- |
|  | WB-62 | ---- | ---- | ---- | ---- |
|  | WB-62FL | 460-175-460 | 4.0 | 300-175-550 | 2.0-4.5 |
|  | WB-67 | 460-175-460 | 4.0 | 300-175-550 | 2.0-4.5 |
|  | WB-92D | 550-155-550 | 4.0 | 200-150-500 | 2.0-6.0 |
|  | WB-100T | 220-80-220 | 4.5 | 200-80-300 | 2.5-5.0 |
|  | WB-109D | 550-250-550 | 5.0 | 250-200-650 | 1.5-7.0 |

Table 212.12.2 Edge-of-Traveled-Way, 3-Centered Compound Curves, cont.

| Angle of Turn (degrees) | Design Vehicle | 3-Centered Compound Curve |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Curve <br> Radif (ft) | Symmetric Offset (ft) | Curve Radif (ft) | Asymmetric <br> (ft) |
| 45 | P | ---- | ---- | -- | -- |
|  | SU-30 | ---- | ---- | ---- | -- |
|  | SU-40 | ---- | ---- | ---- | ---- |
|  | WB-40 | ---- | ---- | ---- | ---- |
|  | WB-62 | 460-240-460 | 2.0 | 120-140-500 | 3.0-8.5 |
|  | WB-62FL | 460-175-460 | 4.0 | 250-125-600 | 1.0-6.0 |
|  | WB-67 | 460-175-460 | 4.0 | 250-125-600 | 1.0-6.0 |
|  | WB-92D | 525-155-525 | 5.0 | 200-140-500 | 1.5-6.0 |
|  | WB-100T | 250-80-250 | 4.5 | 200-80-300 | 2.5-5.5 |
|  | WB-109D | 550-200-550 | 5.0 | 200-170-650 | 1.5-7.0 |
| 60 | P | ---- | ---- | ---- | -- |
|  | SU-30 | ---- | ---- | ---- | ---- |
|  | SU-40 | ---- | ---- | ---- | ---- |
|  | WB-40 | ---- | ---- | ---- | ---- |
|  | WB-62 | 400-100-400 | 15.0 | 110-100-220 | 10.0-12.5 |
|  | WB-62FL | 400-100-400 | 8.0 | 250-125-600 | 1.0-6.0 |
|  | WB-67 | 400-100-400 | 8.0 | 250-125-600 | 1.0-6.0 |
|  | WB-92D | 480-110-480 | 6.0 | 150-110-500 | 3.0-9.0 |
|  | WB-100T | 250-80-250 | 4.5 | 200-80-300 | 2.0-5.5 |
|  | WB-109D | 650-150-650 | 5.5 | 200-140-600 | 1.5-8.0 |
| 75 | P | 100-25-100 | 2.0 | ---- | ---- |
|  | SU-30 | 120-45-120 | 2.0 | ---- | ---- |
|  | SU-40 | 200-35-200 | 5.0 | 60-45-200 | 1.0-4.5 |
|  | WB-40 | 120-45-120 | 5.0 | 120-45-195 | 2.0-6.5 |
|  | WB-62 | 440-75-440 | 15.0 | 140-100-540 | 5.0-12.0 |
|  | WB-62FL | 420-75-420 | 10.0 | 200-80-600 | 1.0-10.0 |
|  | WB-67 | 420-75-420 | 10.0 | 200-80-600 | 1.0-10.0 |
|  | WB-92B | 500-95-500 | 7.0 | 150-100-500 | 1.0-8.0 |
|  | WB-100T | 250-80-250 | 4.5 | 100-80-300 | 1.5-5.0 |
|  | WB-109D | 700-125-700 | 6.5 | 150-110-550 | 1.5-11.5 |

Table 212.12.2 Edge-of-Traveled-Way, 3-Centered Compound Curves, cont.

| Angle of Turn (degrees) | Design Vehicle | 3-Centered Compound Curve |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Curve <br> Radif (ft) | Symmetric Offset (ft) | Curve <br> Radif (ft) | Asymmetric (ft) |
| 90 | P | 100-20-100 | 2.5 | -- | ---- |
|  | SU-30 | 120-40-120 | 2.0 | ---- | ---- |
|  | SU-40 | 200-30-200 | 7.0 | 60-45-200 | 1.0-4.5 |
|  | WB-40 | 120-40-120 | 5.0 | 120-40-200 | 2.0-6.5 |
|  | WB-62 | 400-70-400 | 10.0 | 160-70-360 | 6.0-10.0 |
|  | WB-62FL | 440-65-440 | 10.0 | 200-70-600 | 1.0-11.0 |
|  | WB-67 | 440-65-440 | 10.0 | 200-70-600 | 1.0-11.0 |
|  | WB-92D | 470-75-470 | 10.0 | 150-90-500 | 1.5-8.5 |
|  | WB-100T | 250-70-250 | 4.5 | 200-70-300 | 1.0-5.0 |
|  | WB-109D | 700-110-700 | 6.5 | 100-95-550 | 2.0-11.5 |
| 105 | P | 100-20-100 | 2.5 | ---- | ---- |
|  | SU-30 | 100-35-100 | 3.0 | ---- | ---- |
|  | SU-40 | 200-35-200 | 6.0 | 60-40-190 | 1.5-6.0 |
|  | WB-40 | 100-35-100 | 5.0 | 100-55-200 | 2.0-8.0 |
|  | WB-62 | 520-50-520 | 15.0 | 360-75-600 | 4.0-10.5 |
|  | WB-62FL | 500-50-500 | 13.0 | 200-65-600 | 1.0-11.0 |
|  | WB-67 | 500-50-500 | 13.0 | 200-65-600 | 1.0-11.0 |
|  | WB-92D | 500-80-500 | 8.0 | 150-80-500 | 2.0-10.0 |
|  | WB-100T | 250-60-250 | 5.0 | 100-60-300 | 1.5-6.0 |
|  | WB-109D | 700-95-700 | 8.0 | 150-80-500 | 3.0-15.0 |
| 120 | P | 100-20-100 | 2.0 | ---- | ---- |
|  | SU-30 | 100-30-100 | 3.0 | ---- | ---- |
|  | SU-40 | 200-35-200 | 6.0 | 60-40-190 | 1.5-5.0 |
|  | WB-40 | 120-30-120 | 6.0 | 100-30-180 | 2.0-9.0 |
|  | WB-62 | 520-70-520 | 10.0 | 80-55-520 | 24.0-17.0 |
|  | WB-62FL | 550-45-550 | 15.0 | 200-60-600 | 2.0-12.5 |
|  | WB-67 | 550-45-550 | 15.0 | 200-60-600 | 2.0-12.5 |
|  | WB-92D | 500-70-500 | 10.0 | 150-70-450 | 3.0-10.5 |
|  | WB-100T | 250-60-250 | 5.0 | 100-60-300 | 1.5-6.0 |
|  | WB-109D | 700-85-700 | 9.0 | 150-70-500 | 7.0-17.4 |

Table 212.12.2 Edge-of-Traveled-Way, 3-Centered Compound Curves, cont.

| Angle of Turn (degrees) | Design Vehicle | 3-Centered Compound Curve |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Curve <br> Radif (ft) | Symmetric Offset (ft) | Curve <br> Radit (ft) | Asymmetric <br> (ft) |
| 135 | P | 100-20-100 | 1.5 | --- | ---- |
|  | SU-30 | 100-30-100 | 4.0 | --- | ---- |
|  | SU-40 | 200-40-200 | 4.0 | 60-40-180 | 1.5-5.0 |
|  | WB-40 | 120-30-120 | 6.5 | 100-25-180 | 3.0-13.0 |
|  | WB-62 | 600-60-600 | 12.0 | 100-60-640 | 14.0-7.0 |
|  | WB-62FL | 550-45-550 | 16.0 | 200-60-600 | 2.0-12.5 |
|  | WB-67 | 550-45-550 | 16.0 | 200-60-600 | 2.0-12.5 |
|  | WB-92D | 450-70-450 | 9.0 | 150-65-450 | 7.0-13.5 |
|  | WB-100T | 250-60-250 | 5.5 | 100-60-300 | 2.5-7.0 |
|  | WB-109D | 700-70-700 | 12.5 | 150-65-500 | 14.0-18.4 |
| 150 | P | 75-20-75 | 2.0 | ---- | ---- |
|  | SU-30 | 100-30-100 | 4.0 | ---- | ---- |
|  | SU-40 | 200-35-200 | 6.5 | 60-40-200 | 1.0-4.5 |
|  | WB-40 | 100-30-100 | 6.0 | 90-25-160 | 1.0-12.0 |
|  | WB-62 | 480-55-480 | 15.0 | 140-60-560 | 8.0-10.0 |
|  | WB-62FL | 550-45-550 | 19.0 | 200-55-600 | 7.0-16.4 |
|  | WB-67 | 550-45-550 | 19.0 | 200-55-600 | 7.0-16.4 |
|  | WB-92D | 350-60-350 | 15.0 | 120-65-450 | 6.0-13.0 |
|  | WB-100T | 250-60-250 | 7.0 | 100-60-300 | 5.0-8.0 |
|  | WB-109D | 700-65-700 | 15.0 | 200-65-500 | 9.0-18.4 |
| 180 | P | 50-15-50 | 0.5 | ---- | ---- |
|  | SU-30 | 100-30-100 | 1.5 | ---- | ---- |
|  | SU-40 | 150-35-150 | 6.2 | 50-35-130 | 5.5-7.0 |
|  | WB-40 | 100-20-100 | 9.5 | 85-20-150 | 6.0-13.0 |
|  | WB-62 | 800-45-800 | 20.0 | 100-55-900 | 15.0-15.0 |
|  | WB-62FL | 600-45-600 | 20.5 | 100-55-400 | 6.0-15.0 |
|  | WB-67 | 600-45-600 | 20.5 | 100-55-400 | 6.0-15.0 |
|  | WB-92B | 400-55-400 | 16.8 | 120-60-400 | 9.0-14.5 |
|  | WB-100T | 250-55-250 | 9.5 | 100-55-300 | 8.5-10.5 |
|  | WB-109D | 700-55-700 | 20.0 | 200-60-500 | 10.0-21.0 |

For curbed intersections, the effective turning radius must be considered in addition to the actual curb radius. As shown in Figure 212.12.2, where a parking lane (or bike lane) is present, the vehicle turn is offset from the edge of the roadway by the width of the parking lane or bike lane, creating an "effective turning radius" that is larger than the physical curb radius. Where there is no parking lane or bike lane, the corner radius and effective turning radius are the same. To minimize pedestrian crossing distance, designers should provide the shortest curb radius possible or provide bulbouts within the effective turning radius area. The corner radii should follow the guidance in Table 212.12.3, and accommodate the following:

- The control vehicle, design vehicle, and design speed for each street
- Available R/W
- Angle of turn between intersection legs
- Presence of on-street parking or a bike lane
- The width and number of lanes on the intersecting street

Figure 212.12.2 Actual Curb Radius Vs Effective Radius


Table 212.12.3 Recommended Corner Radii

| R1 Actual Curb <br> Radius (ft) | R2 Effective Turning <br> Radius (ft) | Operational Characteristics |
| :---: | :---: | :--- |
| $5-30$ | $\mathbf{2 5 - 3 0}$ | P vehicles and SU vehicles with minor lane encroachment |
| $5-40$ | $\mathbf{5 0}$ | P vehicles, SU vehicles, and WB-40 vehicles with minor <br> encroachment |
| $5-50$ | All vehicles up to WB-40 |  |
| Notes: <br> (1) Table 212.12.3 assumes perpendicular intersections. For skewed intersections, establish <br> radius using AutoTurn or turning templates. <br> (2) Confirm the actual curb radius using AutoTurn or turn templates. |  |  |

Guidelines for corner radii in C4, C5, and C6 context classification without on-street parking or a bike lane are as follows:
(1) Radii of 15 to 25 feet are adequate for passenger vehicles. These radii are suitable for minor cross streets where there is little occasion for trucks to turn and at major intersections where there are parking lanes;
(2) Radii of 25 feet or more should be provided at minor cross streets on new construction or reconstruction projects;
(3) Radii of 30 feet or more should be provided at minor cross streets where practical so that an occasional truck can turn without too much encroachment;
(4) Radii of 40 feet or more or preferably three-centered curves or simple curves with tapers to fit the paths of large truck combinations, should be provided where such combinations or buses turn frequently. Where speed reductions would cause problems, larger radii should be considered; and,
(5) Curb radii should be coordinated with crosswalk distances or special designs should be used to make crosswalks efficient for all pedestrians. Where larger radii are used, an intermediate refuge or median island is desirable or crosswalks may need to be offset so that crosswalk distances are not excessive. See FDM 210.3 for addtional information on islands.

### 212.12.2 Turning Roadways with Corner Islands

Consider providing a corner island at an intersection where paved areas are excessively large or do not establish proper channelization of traffic. Corner islands can provide delineation for through and turning traffic. In addition, corner islands shorten crosswalks and give pedestrians and bicyclists a refuge area. See FDM 210.3.2 for island requirements.

Channelized right turn lanes can be designed with a flat or near perpendicular angle of entry to the cross street (see Figure 212.12.3). The flat angle of entry is most appropriate for higher speed turning movements with no pedestrian accommodations. Large turning radii and angles of entry into the cross street allow higher turning speeds, reduced traffic delays, and the turning movement of large trucks. The higher speeds, angle of entry and large radii adversely impacts pedestrian safety at the crosswalk.

The near perpendicular angle of entry is preferred where pedestrian facilities are provided. Tight turning radii and angles of entry into the cross street accommodate the following:

- Slower turning speeds,
- Reduced cross walk length,
- Improved pedestrian visibility,
- Improved sight distance
- Decreased angle of driver head turning
- Reduced right-of-way impacts.

Figure 212.12.3 Channelized Right Turn Lanes


Ref: Figure 9-19, 2018 AASHTO Green Book

Consider the near perpendicular right turn lane design in Figure 212.12 .4 when the following conditions are met:

- Context Classification C2T, C3, C4, C5 and C6
- Low speed roadway (design speeds 45 mph and less)
- Pedestrian traffic is expected
- No acceleration lane is provided

This design includes the previously mentioned benefits to passenger cars and pedestrians with stripping and a scalene triangle shaped corner island. An approaching deceleration lane is preferred to provide vehicles additional time to stop for crossing pedestrians. The crosswalk is set back 20 feet minimum from the end of the island to allow room for a passenger car to wait for a gap in traffic with out blocking the crosswalk. As shown in Figure 212.12.4, the outside curb radii can be designed to accommodate over tracking of large vehicles such as single-unit trucks, transit, or Florida Interstate Semi-trailers (WB-62FL).

Figure 212.12.4 Near Perpendicular Right Turn Lane


### 212.12.3 Free-Flow Design

Provide superelevation on free flow turning roadways. An important part of the design on some intersections is the design of a free-flow alignment for turns. Ease and smoothness of operation can result when the free flow turning roadway is designed with compound curves preceded by a deceleration lane. Turning radii and pavement cross slope for free flow right turns at speeds greater than 10 mph are a function of the design speed and design vehicle. In general, the design speed of the turning roadway should be equal to, or within 10 to 20 mph less than the through roadway design speed.

It is desirable to provide as much superelevation as practical on intersection curves, particularly where the intersection curve is sharp and on a downgrade. However, the short curvature and short lengths of turning roadways often prevents the development of a desirable rate of superelevation. Table $\mathbf{2 1 2 . 1 2 . 4}$ provides the minimum superelevation rates in relation to design speed. The wide variation in likely speeds on intersection curves precludes the need for precision, so only the minimum superelevation rate is given for each design speed and intersection curve radius.

Table 212.12.4 Superelevation Rates for Turning Roadways

|  | Design Speed (mph) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 |  |
| Minimum Superelevation Rate | NC | NC | 0.02 | 0.04 | 0.06 | 0.08 | 0.09 | 0.10 |  |
| Minimum Radius (feet) | 25 | 50 | 90 | 150 | 230 | 310 | 430 | 540 |  |

See FDM 210.9 for additional superelevation criteria.

### 212.12.4 Dual and Triple Left Turns

Double and triple turn lanes require turning radii that will accommodate the selected design vehicles turning simultaneously. The radius of curvature in combination with the track width of the design vehicles will establish the required width within the turn. Lane lines (i.e., guidelines) and width requirements should be determined by plotting the swept paths of the selected design vehicles. For preliminary layout of intersection geometry, use the swept path of the design vehicle on the inside turning lane to locate the median nose and crosswalk on the crossing street (at the receiving point of the left turn).

Design of dual turns should accommodate a SU-40 vehicle and a $P$ vehicle turning simultaneously, as illustrated in Figure 212.12.5.

Figure 212.12.5 P and SU Design Vehicles Turning Simultaneously


Design of triple left turns should accommodate a WB-62FL (outside lane), a SU-40 (center or inside lane), and a $P$ vehicle (center or inside lane) turning simultaneously.

Establish control radius for the inside turning lane based on the guidance in FDM 212.14.5 and Table 212.9.2. Establish the inside edge of the outer lane by providing a minimum 4-foot separation between swept paths of the selected design vehicles traveling in the same direction. Except for turns with large radii, the inside edge of the outer lane will not be concentric with the selected control radius. Radius for the inside edge of the outer turn lane should be determined by analysis of the plotted swept path of the design vehicles.

Provide minimum 8-foot separation between vehicles traveling in opposing direction. Separation may be less than 8 feet when:
(1) Turning paths are highly visible and speeds are low, or
(2) Signal left turn phases are not concurrent for the opposing directions.

### 212.13 Islands

See FDM 210.3 for island criteria.

### 212.14 Auxiliary Lanes

The primary function of auxiliary lanes at intersections is to accommodate speed changes, storage and maneuvering of turning traffic. The length of the auxiliary lanes is the sum of the deceleration length, queue length and approach end taper. Pavement marking requirements for auxiliary lanes are included in Standard Plans, Index 711-001.

### 212.14.1 Deceleration Length

The required total deceleration length is that needed for a safe and comfortable stop from the design speed of the highway. See Exhibit 212-1 for minimum deceleration lengths (including taper) for left turn lanes.

Right turn lane tapers and lengths are identical to left turn lanes under stop control conditions. Right turn lane tapers and lengths are site-specific for free-flow or yield conditions.

### 212.14.2 Queue Length

The queue length provided should be based on a traffic study.
For low volume intersections where a traffic study is not justified, a minimum 50-foot queue length (2 vehicles) should be provided for C1, C2, and C3R context classifications. A minimum 100-foot queue length (4 vehicles) should be provided in C2T, C3C, C4, C5, and C6 context classifications. Locations with over $10 \%$ truck traffic should accommodate at least one car and one truck.

For queue lengths at signalized intersections, refer to FDM 232.2.

### 212.14.3 Approach End Taper

The length of approach end tapers is 50 feet for a single turn lane and 100 feet for two or more turn lanes, as shown Exhibit 212-1. These taper lengths apply to all design speeds.

### 212.14.4 Offset Left Turn Lanes

The alignment of opposing left-turn lanes and the horizontal and vertical curvature on the approaches are the principal geometric design elements that determine how much sight distance is available to a left-turning driver. Vehicles queuing in opposing left-turn lanes restrict each other's view of oncoming traffic in the through lanes. The level of restricted view depends on the alignment of opposing left-turn lanes with respect to each other and the type of vehicles in the opposing queue.

The offset distance is defined as the distance between the left edge of the turn lane and the right edge of the opposing turn lane. If the offset distance is to the left of the turn lane it is considered a negative offset, and if it is to the right of turn lane it is considered a positive offset, as illustrated in Figure 212.14.1.

Figure 212.14.1 Negative and Positive Offset Left Turns


The conventional method of designing left turn lanes is to place the left turn lanes adjacent to the through lanes. This design creates a negative offset which restricts the sight distance of the left-turning driver's view of oncoming traffic when another vehicle is in the opposing turn lane. Figure 212.14.2 indicates the negative offset when the conventional design is used.

Figure 212.14.2 Opposing Left Turns (22' Median with Negative 10' Offset)


On curbed roadway designs, offset left-turn lanes should be used with median widths greater than 18 feet. A 4 -foot traffic separator should be used when possible to channelize the left turn and provide separation from opposing traffic.

Consider offset left-turn lanes at C1, C2, and C3R context classification intersections with high turning movements. For median widths 30 feet or less, use a parallel offset left-turn lane. Stripe the area between the offset left-turn lane and the traffic lane where vehicles are moving in the same direction. For medians wider than 30 feet, consider a tapered offset left-turn lane. An offset left is illustrated in Figure 212.14.3.

2018 AASHTO Green Book Figure 9-41 illustrates the design of parallel and tapered left turn lanes.

Figure 212.14.3 Typical Opposing Left Turns (22' Median with Negative 1' Offset)


At locations where the full offset distances cannot be obtained, it is recommended that the minimum offset distances shown in Table 212.14.1 be provided to achieve minimum required sight distances according to design speed. It is recommended that the "Opposing Truck" values be used where the opposing left-turn traffic includes a moderate to heavy volume of large trucks.

Table 212.14.1 Minimum Offset Distances for Left-Turn Lanes

| Design Speed <br> (mph) | Minimum Offset (feet) |  |
| :---: | :---: | :---: |
|  | Opposing Car | Opposing Truck |
| $\leq 30$ | 1.0 | 3.0 |
| 35 | 1.5 | 3.5 |
| $40-45$ | 2.0 | 4.0 |
| $50-55$ | 2.5 | 4.5 |
| $60-65$ | 3.0 | 4.5 |
| 70 | 3.0 | 5.0 |

### 212.14.5 Directional Median Openings

Directional (channelized) median openings are designed to accommodate left-turn movements from the through roadway and prevent or discourage left-turn and crossing movements by traffic from a side road or driveway. Directional median openings are to be provided in accordance with the access management plan for the roadway.

The design of a directional median opening must accommodate the swept path of the predominant design vehicle. Channelization may be achieved using a combination of traffic separators, islands, and tubular markers. See FDM 210 for additional information on islands. See Standard Plans, Index 520-020 for standard details for 4 feet, 6 feet and 8.5 feet wide traffic separators. See FDM 230.2.7 for additional information on tubular markers.

Typical layouts for directional median openings for high-speed roadways with 40-feetwide medians are provided in Exhibits 212-8, 212-9 and 212-10. Type E curb and raised islands in conjunction with the minimum offsets shown in these figures may be used on high-speed roadways for directional median openings.

## DIRECTIONAL MEDIAN OPENING: SU \& WB-40 PARALLEL TURN BAY

> RETURNS:

Returns Depicted:
Three Centered Compound Curves For All Returns Depicted:
$120^{\prime}-40^{\prime}-200^{\prime}$ Radii; $2^{\prime}$ And $8^{\prime}$ offsets
Simple Curve With
40' Radius; 1:15 And 1:8 Tapers With
$2^{\prime}$ And $8^{\prime}$ Offsets Tested (Practical Fit)
SWEPT PATH LEGEND:
$\underset{\text { SU }}{\substack{\text { WB-40 }}}$
QUADRANT NOS. $1 \& 2$ VACANT


NOTE:Return configurations for each quadrant must be analyzed independently to assure adequate return pavement for semi-trailer inside tracking. The depicted design only applies where roads and streets intersect at $90^{\circ}$ to the mainline. ractor-semitrailer.


## DIRECTIONAL MEDIAN OPENING: SU \& WB-40 TAPERED TURN BAY



QUADRANT NOS. $1 \& 2$ VACANT


NOTE: Return configurations for each quadrant must be analyzed independently to assure adequate return pavement for semi-trailer inside tracking. The depicted design only applies where roads and streets
intersect at $90^{\circ}$ to the mainline. Swept paths are by AutoTURN 4.0 for the AASHTO 2018 SU and WB-40 tractor-semitrailer.

