## PAVEMENT EVALUATION CORING AND CONDITION DATA

|             | Cored By:                 | MADRI        | D CPWG     | 3           |           |            |           |         |        |           |      | Coring ( | Completion  | Date:  | 8/23/2023                              |           |         |        |                                     |             |             | Тур      |
|-------------|---------------------------|--------------|------------|-------------|-----------|------------|-----------|---------|--------|-----------|------|----------|-------------|--------|--|-----------|---------|--------|-------------------------------------|-------------|-------------|----------|
|             | W.P.I. No.:               | :            |            |             |           |            |           |         |        |           |      |          | Ν           | Name:  | SR 17                                  |           |         |        |                                     |             | · · · · · · |          |
| F           | in. Proj. ID:             | : 450883-    | 1          |             |           |            |           |         |        |           |      |          |             | From:  | N of Old Sceni                         | c Hwy     |         |        |                                     |             |             | Shou     |
| F.A. F      | Project No.:              | :            |            |             |           | Roa        | adway ID: | 1609000 | 0      |           |      |          |             | To:    | Lake Marion R                          | d / SR 54 | 4       |        |                                     |             |             |          |
|             | County:                   | : Polk       |            |             |           |            | SR No.:   |         |        |           |      |          | Be          | g MP:  | 28.034                                 |           | End MP: | 33.349 | Length:                             | 5.315       |             |          |
|             | Overall                   | Pavemen      | t Conditio | on (from    | DMO field | d review): | Fair      |         |        |           |      | Me       | dian Curbed | (Y/N): | Ν                                      | Paved     |         | Lawn   | Other:                              |             |             |          |
|             |                           |              |            | •           |           |            |           |         |        |           |      |          |             | M      | ainline C                              | ores (    | ML)     |        |                                     |             |             | <u>.</u> |
|             |                           |              |            |             |           |            |           | PA      | VEMENT | LAYER (II | N.)  |          |             |        |  | 0.00 (    |         | SE     |                                     | <b></b>     | CR/         | ACK      |
|             |                           |              |            |             |           |            |           |         |        | ,<br>I    | ,    |          |             |        |  |           |         |        |                                     |             |             | <u> </u> |
| CORE<br>NO. | MILE<br>POST <sup>2</sup> | LANE<br>TYPE | LANE       | WP<br>(Y/N) | FC12.5    | FC3        | SP12.5    | ARMI    | S2     | wc        | T1   | BIND     |             |        | TOTAL<br>ASPHALT<br>THICKNESS<br>(IN.) | LR        | ABC-2   | RAP    | STABILIZED<br>SUBGRADE <sup>3</sup> | DEPTH (IN.) | ТҮРЕ        | 33712    |
| 1           | 28.648                    | ML           | R1         | Y           | 1.5       |            | 2.4       |         |        | 0.6       |      |          |             |        | 4.5                                    | 9.0       |         |        | 0.0                                 | 4.5         | Α           |          |
| 2           | 30.742                    | ML           | R1         | Ν           |           | 1.3        | 3.3       | 0.5     | 3.3    | 0.8       |      |          |             |        | 9.2                                    | 6.0       |         |        | 0.0                                 | 9.2         | С           | I        |
| 4           | 31.022                    | ML           | R1         | Y           |           | 1.4        | 1.8       | 0.6     | 0.8    | 0.5       |      |          |             |        | 5.1                                    | 8.0       |         |        | 6.0                                 | 2.1         | Α           |          |
| 6           | 31.831                    | ML           | L1         | Ν           |           | 1.3        | 2.7       | 0.6     | 0.5    | 0.7       |      |          |             |        | 5.8                                    | 7.0       |         |        | 0.0                                 | 2.0         | В           |          |
| 7           | 28.251                    | ML           | R1         | Y           | 1.1       |            | 2.1       | 0.4     |        | 0.6       |      |          |             |        | 4.2                                    | 9.0       |         |        | 0.0                                 | 3.0         | С           |          |
| 8           | 29.253                    | ML           | R1         | Y           | 1.8       |            |           |         |        |           | 2.3  | 0.9      |             |        | 5.0                                    | 8.0       |         |        | 0.0                                 |             |             |          |
| 9           | 29.792                    | ML           | R1         | Y           |           | 1.5        | 2.7       | 0.5     | 1.1    |           |      |          |             |        | 5.8                                    | 8.0       |         |        | 0.0                                 | 5.8         | Α           |          |
| 10          | 30.256                    | ML           | R1         | Ν           |           | 1.3        | 2.7       | 0.5     | 1.0    | 0.7       |      |          |             |        | 6.2                                    | 7.0       |         |        | 0.0                                 | 2.4         | В           |          |
| 11          | 30.495                    | ML           | R1         | Y           |           | 1.3        | 2.7       | 0.5     | 0.8    | 0.5       |      |          |             |        | 5.8                                    | 7.0       |         |        | 0.0                                 | 2.5         | В           |          |
| 12          | 31.277                    | ML           | R1         | Y           |           | 1.5        | 3.8       | 0.5     | 2.7    | 0.6       |      |          |             |        | 9.1                                    | 8.0       |         |        | 0.0                                 |             |             |          |
| 13          | 31.556                    | ML           | R1         | Y           |           | 1.4        | 2.5       | 0.5     | 1.0    | 0.7       |      |          |             |        | 6.1                                    | 8.0       |         |        | 0.0                                 | 0.4         | Α           | I        |
| 14          | 32.030                    | ML           | R1         | Y           |           | 1.2        | 2.2       | 0.6     | 1.3    | 0.7       |      |          |             |        | 6.0                                    | 6.0       |         |        | 9.0                                 | 2.5         | Α           |          |
| 15          | 32.290                    | ML           | R1         | Ν           |           | 1.5        | 2.3       | 0.4     | 1.2    | 0.4       |      |          |             |        | 5.8                                    | 6.0       |         |        | 8.0                                 |             |             |          |
| 16          | 32.575                    | ML           | R1         | Ν           | 1.5       |            | 3.7       |         |        |           |      |          |             |        | 5.2                                    | 22.0      |         |        | 0.0                                 |             |             |          |
| 17          | 32.799                    | ML           | R1         | Y           | 1.4       |            | 3.5       |         |        |           |      |          |             |        | 4.9                                    | 15.0      |         |        | 0.0                                 |             |             |          |
| 18          | 33.067                    | ML           | R1         | Y           | 1.5       |            | 2.4       |         |        |           |      |          |             |        | 3.9                                    | 8.0       |         |        | 0.0                                 | 3.9         | С           |          |
| 19          | 33.321                    | ML           | L1         | Y           | 1.9       |            | 4.7       |         | 3.5    |           |      |          |             |        | 10.1                                   | 10.0      |         |        | 0.0                                 |             |             |          |
| 20          | 32.941                    | ML           | L1         | Ν           | 1.3       |            | 2.2       |         |        |           |      |          |             |        | 3.5                                    | 8.0       |         |        | 0.0                                 |             |             |          |
| 21          | 32.459                    | ML           | L1         | Y           | 1.5       |            | 4.4       |         |        |           |      |          |             |        | 5.9                                    | 14.0      |         |        | 0.0                                 |             |             |          |
| 22          | 32.140                    | ML           | L1         | Y           |           | 1.5        | 2.6       | 0.5     | 1.2    | 0.7       |      |          |             |        | 6.5                                    | 7.0       |         |        | 0.0                                 | 0.7         | Α           | II       |
| 23          | 31.685                    | ML           | L1         | Ν           |           | 1.5        | 2.3       | 0.5     | 0.9    | 0.7       |      |          |             |        | 5.9                                    | 8.0       |         |        | <br>0.0                             |             |             |          |
| 24          | 31.136                    | ML           | L1         | Y           |           | 1.4        | 3.0       | 0.6     | 1.2    |           |      |          |             |        | 6.2                                    | 8.0       |         |        | 0.0                                 | 6.2         | Α           |          |
| 25          | 30.874                    | ML           | L1         | Ν           |           | 1.5        | 3.2       | 0.7     | 0.5    | 0.6       |      |          |             |        | 6.5                                    | 8.0       |         |        | 0.0                                 |             |             |          |
| 26          | 30.384                    | ML           | L1         | Y           |           | 1.5        | 2.2       | 0.5     | 1.6    | 0.5       |      |          |             |        | 6.3                                    | 8.0       |         |        | <br>0.0                             |             |             |          |
| 27          | 30.031                    | ML           | L1         | Ν           |           | 1.6        | 4.4       | 0.5     | 0.4    | 0.6       |      |          |             |        | 7.5                                    | 8.0       |         |        | 0.0                                 |             |             |          |
| 28          | 29.514                    | ML           | L1         | Ν           |           | 1.5        | 2.9       | 0.5     |        | 0.6       |      |          |             |        | 5.5                                    | 8.0       |         |        | <br>0.0                             |             |             |          |
| 29          | 28.967                    | ML           | L1         | Y           | 1.5       |            |           |         |        |           | 1.8  | 0.7      |             |        | 4.0                                    | 8.0       |         |        | 0.0                                 |             |             |          |
| 30          | 28.436                    | ML           | L1         | Ν           | 1.9       |            | 1.2       | 0.6     | 1.2    | 0.6       |      |          |             |        | 5.5                                    | 8.0       |         |        | <br>0.0                             |             |             |          |
| 67          | 33.067                    | ML           | R1         | Y           | 1.5       |            | 4.5       |         |        |           |      |          |             |        | 6.0                                    | 8.0       |         |        | <br>0.0                             |             |             |          |
| 68          | 33.067                    | ML           | R1         | Y           | 1.5       |            | 6.2       | 0.6     |        | 0.9       |      |          |             |        | 9.2                                    | 8.0       |         |        | 0.0                                 |             |             |          |
| AVERAG      | ĴΕ                        |              |            |             | 1.53      | 1.42       | 3.02      | 0.53    | 1.34   | 0.63      | 2.05 | 0.80     |             |        | 6.04                                   | 8.70      |         |        | 0.77                                | 3.48        |             |          |
| MAX         |                           |              |            |             | 1.90      | 1.60       | 6.20      | 0.70    | 3.50   | 0.90      | 2.30 | 0.90     |             |        | 10.10                                  | 22.00     |         |        | 9.00                                | 9.20        |             |          |
| MIN         |                           |              |            |             | 1.10      | 1.20       | 1.20      | 0.40    | 0.40   | 0.40      | 1.80 | 0.70     |             |        | 3.50                                   | 6.00      |         |        | 0.00                                | 0.40        |             |          |
| LAYER (     | OEF.                      |              |            |             | 0.25      | 0.17       | 0.25      | 0.00    | 0.25   | UNKW      | 0.23 | 0.20     |             |        |  | 0.18      | 0.16    | UNKW   | 0.08                                |             |             | 1        |

| ical Section: 1        |                                     |  |  |  |  |  |  |  |  |  |
|------------------------|-------------------------------------|--|--|--|--|--|--|--|--|--|
| Lanes:                 | Lanes: 2 Lane Urban Major Collector |  |  |  |  |  |  |  |  |  |
| oulder Type and        | ulder Type and Condition:           |  |  |  |  |  |  |  |  |  |
| Inside:                |                                     |  |  |  |  |  |  |  |  |  |
| Outside:               | Outside:                            |  |  |  |  |  |  |  |  |  |
| Curb & Gutter (Y/N): Y |                                     |  |  |  |  |  |  |  |  |  |
|                        |                                     |  |  |  |  |  |  |  |  |  |

| - CO                        |  |
|-----------------------------|--|
|                             |  |
| II M P                      |  |
|                             |  |
| II M P                      |  |
| II M F                      |  |
| II M F                      |  |
| II M F                      |  |
| F                           |  |
| II M F                      |  |
| II M F                      |  |
| II M F                      |  |
| F Bottom up crack           |  |
| IB M F Slippage             |  |
| II M F Bottom up crack      |  |
| F                           |  |
| F                           |  |
| F                           |  |
| II M F Widening crack       |  |
| F                           |  |
| F                           |  |
| F                           |  |
| IB L F Possible slippage    |  |
| F                           |  |
| III S F                     |  |
| F Bottom up crack           |  |
| F Bottom up crack           |  |
| F                           |  |
| F                           |  |
| F                           |  |
|                             |  |
| P RT of Core #18 (Widening) |  |
| P LT of Core #18 (Widening) |  |
|                             |  |
|                             |  |
|                             |  |
|                             |  |

# PAVEMENT EVALUATION CORING AND CONDITION DATA

|             | Cored By:                 | MADRI        | D CPWG     |             |           |            |           |         |        |           |     | Coring | Completic  | on Date:  | 8/23/2023                              |           |         |        |   |                                     |             |      | Тур       |
|-------------|---------------------------|--------------|------------|-------------|-----------|------------|-----------|---------|--------|-----------|-----|--------|------------|-----------|--|-----------|---------|--------|---|-------------------------------------|-------------|------|-----------|
|             | W.P.I. No.:               |              |            |             |           |            |           |         |        |           |     |        |            | Name:     | SR 17                                  |           |         |        |   |                                     |             |      |           |
| F           | in. Proj. ID:             | 450883-      | 1          |             |           |            |           |         |        |           |     |        |            | From:     | N of Old Sceni                         | c Hwy     |         |        |   |                                     |             |      | Sho       |
| F.A. I      | Project No.:              |              |            |             |           | Roa        | adway ID: | 1609000 | 0      |           |     |        |            | To:       | Lake Marion R                          | d / SR 54 | 14      |        |   |                                     |             |      |           |
|             | County:                   | Polk         |            |             |           |            | SR No.:   | 17      |        |           |     |        |            | Beg MP:   | 28.034                                 |           | End MP: | 33.349 |   | Length:                             | 5.315       |      |           |
|             | Overall                   | Pavemen      | t Conditio | n (from     | DMO field | d review): | Fair      | -       |        |           |     | Me     | dian Curbe | ed (Y/N): | N                                      | Paved     |         | Lawn   |   | Other:                              |             |      | $\square$ |
|             |                           |              |            |             |           |            |           |         |        |           |     |        |            | Μ         | ainline C                              | ores      | (ML)    | -      |   |                                     |             |      |           |
|             |                           |              |            |             |           |            |           | PA      | VEMENT | LAYER (II | N.) |        |            |           |  |           | B       | ASE    |   |                                     |             | CRA  | ICK       |
| CORE<br>NO. | MILE<br>POST <sup>2</sup> | LANE<br>TYPE | LANE       | WP<br>(Y/N) | FC12.5    | FC3        | SP12.5    | ARMI    | S2     | WC        | T1  | BIND   |            |           | TOTAL<br>ASPHALT<br>THICKNESS<br>(IN.) | LR        | ABC-2   | RAP    |   | STABILIZED<br>SUBGRADE <sup>3</sup> | DEPTH (IN.) | TYPE | 334 14    |
| Notes:      |                           | -            | •          |             |           |            | -         |         |        | •         |     | •      |            |           |  |           |         | •      | • |                                     |             |      |           |

1. The data presented on this table is specific only at the locations cored at the time of the investigation. Should questions arise regarding the pavement composition, it is incumbent upon those raising the question to perform additional exploration as necessary.

2. Mile posts are approximate based on field recorded measurements using a Distance Measuring Instrument (DMI) or a GPS unit.

3. Stabilization thickness was checked on 10% of the coring locations. For pavement design, assume 12 inches of thickness for stabilization.

4. The cross slope is approximate and measured in the center of the lane.

5. A blank cell indicates measurement was not recorded.

6. A value of "UNK" indicates material was encountered but the total thickness was not determined.

| Lane Designations - Decreasing MP | Lane Designations - Increasing MP |                | Lane Type                      | Crack Type      | Crack Rating   | Extent       | Pavement Condition |
|-----------------------------------|-----------------------------------|----------------|--------------------------------|-----------------|--|--------------|--------------------|
| OL/IL - Outside/Inside Shoulder   | OR/IR - Outside/Inside Shoulder   | ML - Mainline  | S - Shoulder                   | A - Alligator   | Class IB - Hairline cracks that are $\leq$ 1/8 inch wide | L - Light    | G - Good           |
| L1 - 1st Lane Left of Centerline  | R1 - 1st Lane Right of Centerline | TL - Turn Lane | SS - Side Street               | B - Block       | Class II - Cracks > than $1/8$ inch and $\leq 1/4$ inch  | M - Moderate | F - Fair           |
| LL/LR - Left/Right Turn Lane      | RL/RR - Left/Right Turn Lane      | CO - Crossover | BR - Bridge Approach/Departure | C - Combination | Class III - Cracks > 1/4 inch                            | S - Severe   | P - Poor           |

#### bical Section: 1

| Lanes: 2 Lane Urban Major Collector |  |  |  |  |  |  |  |  |  |  |  |
|-------------------------------------|--|--|--|--|--|--|--|--|--|--|--|
| Ider Type and Condition:<br>Inside: |  |  |  |  |  |  |  |  |  |  |  |
|                                     |  |  |  |  |  |  |  |  |  |  |  |
|                                     |  |  |  |  |  |  |  |  |  |  |  |
| r (Y/N): Y                          |  |  |  |  |  |  |  |  |  |  |  |
|                                     |  |  |  |  |  |  |  |  |  |  |  |
|                                     |  |  |  |  |  |  |  |  |  |  |  |
|                                     |  |  |  |  |  |  |  |  |  |  |  |
|                                     |  |  |  |  |  |  |  |  |  |  |  |

| CLASS | EXTENT | PAVEMEN1<br>CONDITION | COMMENTS |
|-------|--------|-----------------------|----------|
|-------|--------|-----------------------|----------|

### PAVEMENT EVALUATION CORING AND CONDITION DATA

| Cored By: MADRID CPWG Coring Co |                          |              |            |             |           | Coring Completion Date: 8/23/2023 Typical Section: 1 |           |         |        |           |      |      |            |           |  |           |         |        |                                     |             |       |          |           |                              |                                      |
|---------------------------------|--------------------------|--------------|------------|-------------|-----------|--|-----------|---------|--------|-----------|------|------|------------|-----------|--|-----------|---------|--------|-------------------------------------|-------------|-------|----------|-----------|------------------------------|--------------------------------------|
|                                 | P.I. No.:                |              |            |             |           |  |           |         |        |           |      |      |            | Name:     | SR 17                                  |           |         |        |                                     |             |       |          | Lanes:    | 2 Lane l                     | Jrban Major Collector                |
|                                 |                          | 450883-1     |            |             |           |  |           |         |        |           |      |      |            |           | N of Old Sceni                         |           |         |        |                                     |             |       | Shoulder | Type and  | d Conditi                    | on:                                  |
| F.A. Proj                       |                          |              |            |             |           | Roa  | adway ID: | 1609000 | 0      |           |      |      |            | To:       | Lake Marion R                          | d / SR 54 | 4       | -      | -                                   | _           |       |          | Inside:   |                              |                                      |
|                                 | County:                  |              |            |             |           |  | SR No.:   | 17      |        |           |      |      | E          | Beg MP:   | 28.034                                 |           | End MP: | 33.349 | Length:                             | 5.315       |       |          | Outside:  |                              |                                      |
| (                               | Overall F                | Pavement     | t Conditio | n (from     | DMO field | review):   | : Fair    |         |        |           |      | Mee  | dian Curbe | ed (Y/N): | Ν                                      | Paved     |         | Lawn   | Other:                              |             |       | Cur      | b & Gutte | er (Y/N):                    | Y                                    |
|                                 |                          |              |            |             |           |  |           |         |        |           |      |      |            | S         | Shoulder (                             | Cores     |         |        |                                     |             |       |          |           |                              |                                      |
|                                 |                          |              |            |             |           |  | 1         | PA      | VEMENT | LAYER (IN | l.)  |      | T          |           |  |           | BA      | SE     |                                     |             | CRA   | ACK      |           |                              |                                      |
|                                 | NILE<br>OST <sup>2</sup> | LANE<br>TYPE | LANE       | WP<br>(Y/N) | FC12.5    | FC3  | SP12.5    | ARMI    | \$2    | wc        | T1   | BIND |            |           | TOTAL<br>ASPHALT<br>THICKNESS<br>(IN.) | LR        | ABC-2   | RAP    | STABILIZED<br>SUBGRADE <sup>3</sup> | DEPTH (IN.) | JAYPE | CLASS    | EXTENT    | <b>PAVEMENT</b><br>CONDITION | COMMENTS                             |
|                                 | 0.743                    | S            | OR         | Ν           |           |  | 2.0       |         |        |           |      |      |            |           | 2.0                                    |           | 1.8     |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 8.099                    | S            | OR         | Ν           | 1.8       |  | 1.0       |         |        |           |      |      |            |           | 2.8                                    |           |         | 6.2    | 0.0                                 |             |       |          |           |                              | Measured in hole (Bottom fell apart) |
|                                 | 8.568                    | S            | OR         | N           | 1.8       |  | 1.7       |         |        |           |      |      |            |           | 3.5                                    |           |         | 4.5    | 0.0                                 |             |       |          |           |                              | Measured in hole (Bottom fell apart) |
|                                 | 9.142                    | S            | OR         | Ν           | 1.3       |  |           |         |        |           | 1.0  | 1.2  |            |           | 3.5                                    | 5.0       |         |        | 0.0                                 | 3.5         | С     |          | М         | F                            |                                      |
|                                 | 9.631                    | S            | OR         | N           |           | 1.2  | 0.8       |         |        |           |      |      |            |           | 2.0                                    | 5.0       |         |        | 0.0                                 | 0.3         | A     | IB       | L         | F                            |                                      |
|                                 | 9.913                    | S            | OR         | Ν           |           | 1.2  | 0.8       |         |        |           |      |      |            |           | 2.0                                    | 6.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 0.149                    | S            | OR         | N           |           | 1.6  |           |         |        |           |      |      |            |           | 1.6                                    | 6.0       |         |        | 0.0                                 | 0.3         | В     | IB       | L         | F                            |                                      |
|                                 | 0.611                    | S            | OR         | Ν           |           | 2.0  |           |         |        |           |      |      |            |           | 2.0                                    | 6.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 1.220                    | S            | OR         | Ν           |           | 1.5  | 1.6       |         |        |           |      |      |            |           | 3.1                                    |           | 9.7     |        | 0.0                                 |             |       |          |           | F                            | Core broke into 2 pieces             |
|                                 | 1.463                    | S            | OR         | Ν           |           | 1.6  | 0.6       |         |        |           |      |      |            |           | 2.2                                    | 3.5       |         |        | 6.0                                 |             |       |          |           | F                            |                                      |
|                                 | 1.943                    | S            | OR         | Ν           |           | 1.5  | 1.6       |         |        |           |      |      |            |           | 3.1                                    | 5.0       |         |        | 6.0                                 |             |       |          |           | F                            |                                      |
|                                 | 2.386                    | S            | OR         | Ν           |           | 1.7  | 1.2       |         |        |           |      |      |            |           | 2.9                                    | 6.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 2.904                    | S            | OR         | Ν           |           |  | 3.0       |         |        |           |      |      |            |           | 3.0                                    | 6.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 3.186                    | S            | OL         | Ν           | 1.1       |  | 2.2       |         |        |           |      |      |            |           | 3.3                                    | 6.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 2.695                    | S            | OL         | N           | 1.6       |  | 3.8       |         |        |           |      |      |            |           | 5.4                                    | 7.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 2.219                    | S            | OL         | Ν           |           | 1.5  | 0.7       |         |        |           |      |      |            |           | 2.2                                    | 4.0       |         |        |                                     |             |       |          |           | F                            |                                      |
|                                 | 1.766                    | S            | OL         | Ν           |           | 1.9  | 0.6       |         |        |           |      |      |            |           | 2.5                                    | 4.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 1.390                    | S            | OL         | N           |           | 1.2  | 4.8       |         |        |           |      |      |            |           | 6.0                                    | 8.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 0.938                    | S            | OL         | N           |           | 1.4  | 1.0       |         |        |           |      |      |            |           | 2.4                                    | 6.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 0.435                    | S            | OL         | N           |           | 2.0  | 0.9       |         |        |           |      |      |            |           | 2.9                                    | 6.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 0.078                    | S            | OL         | Ν           |           | 1.7  | 1.2       |         |        |           |      |      |            |           | 2.9                                    | 6.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 9.441                    | S            | OL         | Ν           |           | 1.6  | 0.8       |         |        |           |      |      |            |           | 2.4                                    | 5.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 8.829                    | S            | OL         | N           | 1.5       |  | 0.7       |         |        |           |      |      |            |           | 2.2                                    | 6.0       |         |        | 0.0                                 |             |       |          |           | F                            |                                      |
|                                 | 8.489                    | S            | OL         | Ν           | 1.4       |  | 0.9       |         |        |           |      |      |            |           | 2.3                                    |           |         | 6.2    | 0.0                                 |             |       |          |           |                              | Measured in hole (Core fell apart)   |
|                                 | 8.307                    | S            | OL         | Ν           | 1.3       |  | 0.7       |         |        |           |      |      |            |           | 2.0                                    |           |         | 6.0    | 0.0                                 |             |       |          |           | F                            | Measured in hole (Core fell apart)   |
| AVERAGE                         |                          |              |            |             | 1.48      | 1.57   | 1.48      |         |        |           | 1.00 | 1.20 |            |           | 2.81                                   | 5.61      | 5.75    | 5.73   | 0.50                                | 1.37        |       |          |           |                              |                                      |
| МАХ                             |                          |              |            |             | 1.80      | 2.00   | 4.80      |         |        |           | 1.00 | 1.20 |            |           | 6.00                                   | 8.00      | 9.70    | 6.20   | 6.00                                | 3.50        |       |          |           |                              |                                      |
| MIN                             |                          |              |            |             | 1.10      | 1.20   | 0.60      |         |        |           | 1.00 | 1.20 |            |           | 1.60                                   | 3.50      | 1.80    | 4.50   | 0.00                                | 0.30        |       |          |           |                              |                                      |
| LAYER COE                       | F                        |              |            |             | 0.25      | 0.17   | 0.25      | 0.00    | 0.25   | UNKW      | 0.23 | 0.20 |            |           |  | 0.18      | 0.16    | UNKW   | 0.08                                |             |       |          |           |                              |                                      |

Notes:

1. The data presented on this table is specific only at the locations cored at the time of the investigation. Should questions arise regarding the pavement composition, it is incumbent upon those raising the question to perform additional exploration as necessary.

2. Mile posts are approximate based on field recorded measurements using a Distance Measuring Instrument (DMI) or a GPS unit.

3. Stabilization thickness was checked on 10% of the coring locations. For pavement design, assume 12 inches of thickness for stabilization.

4. The cross slope is approximate and measured in the center of the lane.

| oical Section: 1 |  |
|------------------|--|
|------------------|--|

| CLASS | EXTENT | PAVEMENT<br>CONDITION | COMMENTS                             |
|-------|--------|-----------------------|--------------------------------------|
|       |        | F                     |                                      |
|       |        | F                     | Measured in hole (Bottom fell apart) |
|       |        | F                     | Measured in hole (Bottom fell apart) |
|       | М      | F                     |                                      |
| IB    | L      | F                     |                                      |
|       |        | F                     |                                      |
| IB    | L      | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     | Core broke into 2 pieces             |
|       |        | F                     | · · · · ·                            |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     |                                      |
|       |        | F                     | Measured in hole (Core fell apart)   |
|       |        | F                     | Measured in hole (Core fell apart)   |
|       |        |                       | · · · · · · ·                        |
|       |        |                       |                                      |
|       |        |                       |                                      |
|       |        |                       |                                      |
|       |        |                       |                                      |

# PAVEMENT EVALUATION CORING AND CONDITION DATA

C - Combination

|   | Cored By:                 | MADRI   | D CPWG   | ì           |            |  |   |          |   |           | Coring Completion Date: 8/23/2023 |      |          |  |                  |          |           |  |                                     |             |      | Туріса |
|---|---------------------------|---|----------|-------------|------------|--|---|----------|---|-----------|-----------------------------------|------|----------|--|------------------|----------|-----------|--|-------------------------------------|-------------|------|--------|
|   | W.P.I. No.:               |   |          |             |            |  |   |          |   |           |                                   |      | Name     | : SR 17                                |                  |          |           |  |                                     |             |      |        |
| Fi  | in. Proj. ID:             | 450883-   | 1        |             |            |  |   |          |   |           |                                   |      | From     | N of Old Scen                          | ic Hwy           |          |           |  |                                     |             |      | Should |
| F.A. F  | Project No.:              |   |          |             |            | Roa  | adway ID:   | 1609000  | 0   |           |                                   |      | То       | Lake Marion F                          | Rd / SR 54       | .4       |           |  |                                     |             |      |        |
|   | County:                   | Polk  |          |             |            |  | SR No.:   | 17       |   |           |                                   |      | Beg MP   | : 28.034                               | 28.034 End MP: 3 |          | 33.349 Le |  | Length: 5.315                       |             |      |        |
|   | Overall I                 | erall Pavement Condition (from DMO field review): Fair Median Curbed (Y/N): N Paved Lawn Other: C |          |             |            |  |   |          |   |           |                                   |      |          |  |                  |          |           |  |                                     |             |      |        |
|   |                           |   |          | •           |            | ,  |   |          |   |           |                                   |      | Ś        | Shoulder                               | Cores            | (S)      | •         |  |                                     |             |      |        |
|   |                           |   |          |             |            |  |   | PA       | VEMENT  | LAYER (II | N.)                               |      |          |  |                  | BA       | SE        |  |                                     |             | CRA  | ACK    |
| CORE<br>NO.   | MILE<br>POST <sup>2</sup> | LANE<br>TYPE  | LANE     | WP<br>(Y/N) | FC12.5     | FC3  | SP12.5  | ARMI     | S2  | wc        | T1                                | BIND |          | TOTAL<br>ASPHALT<br>THICKNESS<br>(IN.) | LR               | ABC-2    | RAP       |  | STABILIZED<br>SUBGRADE <sup>3</sup> | DEPTH (IN.) | TYPE | CLASS  |
| 5. A blan   | k cell indica             | ates meas   | surement | was no      | t recorded | l.   |   |          |   | •         |                                   | •    |          | -                                      | -                |          | •         |  |                                     |             |      | •      |
| 6. A valu   | e of "UNK"                | indicates   | material | was en      | countered  | ntered but the total thickness was not determined. |   |          |   |           |                                   |      |          |  |                  |          |           |  |                                     |             |      |        |
| Lane De   | esignations               | - Decrea  | sing MP  |             | Lane D     | esignatio  | ns - Increa   | asing MP |   |           |                                   | La   | ine Type |  | Crac             | k Type   |           |  | Crack R                             | ating       |      |        |
| OL/IL   | - Outside/I               | Dutside/Inside Shoulder OR/IR - Outside/Inside Shoulder N   |          |             |            |  |   | ML - N   | - Mainline S - Shoulder A - Alligator Class IB - Hairline cracks that are |           |                                   |      |          |  | hat are ≤        | 1/8 inch | wide      |  |                                     |             |      |        |
| L1 - 1st Lane Left of Centerline R1 - 1st Lane Right of Centerline TL - |                           |   |          |             |            | TL - Tu  | TL - Turn Lane SS - Side Street B - Block Class II - Cracks > than 1/8 inch and |          |   |           |                                   |      |          | nd ≤ 1/4                               | inch             |          |           |  |                                     |             |      |        |

BR - Bridge Approach/Departure

CO - Crossover

LL/LR - Left/Right Turn Lane

RL/RR - Left/Right Turn Lane

### pical Section: 1

Class III - Cracks > 1/4 inch

| Lanes:          | 2 Lane Urban          | Major Collector |
|-----------------|-----------------------|-----------------|
| oulder Type an  | d Condition:          |                 |
| Inside:         |                       |                 |
| Outside:        |                       |                 |
| Curb & Gutt     | er (Y/N): Y           |                 |
|                 |                       |                 |
|                 |                       |                 |
| CLASS<br>EXTENT | PAVEMENT<br>CONDITION | COMMENTS        |

|    | Extent       | Pavement Condition |
|----|--------------|--------------------|
| de | L - Light    | G - Good           |
| n  | M - Moderate | F - Fair           |
|    | S - Severe   | P - Poor           |

### PAVEMENT EVALUATION CORING AND CONDITION DATA

|             | Cored By:                 | MADRI        | CPWG       | ì           |           |            |           |         |        |           |      | Coring ( | Completion Date:   | 8/23/2023                              |            |         |        |                                     |             |      | Тур    |
|-------------|---------------------------|--------------|------------|-------------|-----------|------------|-----------|---------|--------|-----------|------|----------|--------------------|--|------------|---------|--------|-------------------------------------|-------------|------|--------|
|             | W.P.I. No.:               |              |            |             |           |            |           |         |        |           |      |          | Name:              | SR 17                                  |            |         |        |                                     |             |      |        |
| F           | in. Proj. ID:             | 450883-      | 1          |             |           |            |           |         |        |           |      |          | From:              | N of Old Scen                          | ic Hwy     |         |        |                                     |             |      | Sho    |
| F.A. I      | Project No.:              |              |            |             |           | Roa        | adway ID: | 1609000 | 0      |           |      |          | To:                | Lake Marion F                          | Rd / SR 54 | 4       |        |                                     |             |      |        |
|             | County:                   | Polk         |            |             |           |            | SR No.:   | 17      |        |           |      |          | Beg MP:            | 28.034                                 |            | End MP: | 33.349 | Length:                             | 5.315       |      |        |
|             | Overall                   | Pavemen      | t Conditio | on (from    | DMO field | d review): | Fair      |         |        |           |      | Me       | dian Curbed (Y/N): | N                                      | Paved      |         | Lawn   | Other:                              |             |      |        |
|             |                           |              |            |             |           |            |           |         |        |           |      |          | Τι                 | urn Lane                               | Cores      | (TL)    |        |                                     |             |      |        |
|             |                           |              |            |             |           |            |           | PA      | VEMENT | LAYER (II | V.)  |          |                    |  |            |         | SE     |                                     |             | CR/  | ACK    |
| CORE<br>NO. | MILE<br>POST <sup>2</sup> | LANE<br>TYPE | LANE       | WP<br>(Y/N) | FC12.5    | FC3        | SP12.5    | ARMI    | \$2    | wc        | T1   | BIND     |                    | TOTAL<br>ASPHALT<br>THICKNESS<br>(IN.) | LR         | ABC-2   | RAP    | STABILIZED<br>SUBGRADE <sup>3</sup> | DEPTH (IN.) | ТҮРЕ | 001 70 |
| 5           | 33.235                    | TL           | LL         | Ν           | 1.5       |            | 5.4       | 0.5     | 1.5    | 0.6       |      |          |                    | 9.5                                    | 12.0       |         |        | 0.0                                 | 3.2         | В    |        |
| 55          | 28.094                    | TL           | LR         | Y           | 1.7       |            | 3.3       |         |        |           |      |          |                    | 5.0                                    | 15.0       |         |        | 0.0                                 |             |      |        |
| 56          | 28.151                    | TL           | LR         | Y           | 1.8       |            | 1.9       |         |        |           |      |          |                    | 3.7                                    | 14.0       |         |        | 0.0                                 |             |      |        |
| 57          | 28.675                    | TL           | LL         | Ν           | 1.8       |            | 1.8       |         |        | 0.5       |      |          |                    | 4.1                                    | 10.0       |         |        | 0.0                                 |             |      |        |
| 58          | 29.050                    | TL           | LR         | Ν           | 1.6       |            |           |         |        |           | 0.4  | 1.1      |                    | 3.1                                    | 5.0        |         |        | 5.0                                 |             |      |        |
| 59          | 30.264                    | TL           | RR         | Ν           |           | 1.4        | 4.4       |         |        |           |      |          |                    | 5.8                                    | 7.0        |         |        | 0.0                                 |             |      |        |
| 60          | 31.297                    | TL           | RL         | Ν           |           | 1.5        | 4.4       | 0.4     | 0.4    | 0.6       |      |          |                    | 7.3                                    | 6.0        |         |        | 8.0                                 |             |      |        |
| 61          | 31.339                    | TL           | LR         | Y           |           | 1.1        | 3.6       |         |        |           |      |          |                    | 4.7                                    |            | 9.9     |        | 0.0                                 |             |      |        |
| 62          | 31.368                    | TL           | LL         | Ν           |           | 1.2        | 4.2       | 0.5     | 0.8    | 0.6       |      |          |                    | 7.3                                    | 8.0        |         |        | 0.0                                 |             |      |        |
| 63          | 32.560                    | TL           | LL         | Ν           | 1.5       |            | 2.4       | 0.3     | 1.5    | 0.6       |      |          |                    | 6.3                                    | 7.0        |         |        | 0.0                                 |             |      |        |
| 64          | 33.093                    | TL           | RR         | Ν           | 1.4       |            | 4.6       |         |        |           |      |          |                    | 6.0                                    | 28.0       |         |        | 0.0                                 |             |      |        |
| 65          | 33.164                    | TL           | LL         | Ν           | 1.9       |            | 5.2       | 0.5     | 0.9    | 0.4       |      |          |                    | 8.9                                    | 7.0        |         |        | 0.0                                 |             |      |        |
| 66          | 33.290                    | TL           | RL         | Ν           | 1.3       |            | 5.4       |         | 1.6    | 0.6       |      |          |                    | 8.9                                    | 8.0        |         |        | 0.0                                 |             |      |        |
| AVERAG      | ĴΕ                        |              |            |             | 1.61      | 1.30       | 3.88      | 0.44    | 1.12   | 0.56      | 0.40 | 1.10     |                    | 6.20                                   | 10.58      | 9.90    |        | 1.00                                | 3.20        |      |        |
| MAX         |                           |              |            |             | 1.90      | 1.50       | 5.40      | 0.50    | 1.60   | 0.60      | 0.40 | 1.10     |                    | 9.50                                   | 28.00      | 9.90    |        | 8.00                                | 3.20        |      |        |
| MIN         |                           |              |            |             | 1.30      | 1.10       | 1.80      | 0.30    | 0.40   | 0.40      | 0.40 | 1.10     |                    | 3.10                                   | 5.00       | 9.90    |        | <br>0.00                            | 3.20        |      |        |
| LAYER (     | COEF.                     |              |            |             | 0.25      | 0.17       | 0.25      | 0.00    | 0.25   | UNKW      | 0.23 | 0.20     |                    |  | 0.18       | 0.16    | UNKW   | 0.08                                |             |      |        |

Notes:

1. The data presented on this table is specific only at the locations cored at the time of the investigation. Should questions arise regarding the pavement composition, it is incumbent upon those raising the question to perform additional exploration as necessary.

2. Mile posts are approximate based on field recorded measurements using a Distance Measuring Instrument (DMI) or a GPS unit.

3. Stabilization thickness was checked on 10% of the coring locations. For pavement design, assume 12 inches of thickness for stabilization.

4. The cross slope is approximate and measured in the center of the lane.

5. A blank cell indicates measurement was not recorded.

6. A value of "UNK" indicates material was encountered but the total thickness was not determined.

| Lane Designations - Decreasing MP | Lane Designations - Increasing MP |                | <u>Lane Type</u>               | Crack Type      | Crack Rating   | Extent       | Pavement Condition |  |  |  |
|-----------------------------------|-----------------------------------|----------------|--------------------------------|-----------------|--|--------------|--------------------|--|--|--|
| OL/IL - Outside/Inside Shoulder   | OR/IR - Outside/Inside Shoulder   | ML - Mainline  | S - Shoulder                   | A - Alligator   | Class IB - Hairline cracks that are $\leq 1/8$ inch wide | L - Light    | G - Good           |  |  |  |
| L1 - 1st Lane Left of Centerline  | R1 - 1st Lane Right of Centerline | TL - Turn Lane | SS - Side Street               | B - Block       | Class II - Cracks > than $1/8$ inch and $\leq 1/4$ inch  | M - Moderate | F - Fair           |  |  |  |
| LL/LR - Left/Right Turn Lane      | RL/RR - Left/Right Turn Lane      | CO - Crossover | BR - Bridge Approach/Departure | C - Combination | Class III - Cracks > 1/4 inch                            | S - Severe   | P - Poor           |  |  |  |

| pical Section: 1           |                              |  |  |  |  |  |  |
|----------------------------|------------------------------|--|--|--|--|--|--|
| Lanes:                     | 2 Lane Urban Major Collector |  |  |  |  |  |  |
| pulder Type and Condition: |                              |  |  |  |  |  |  |
| Inside:                    |                              |  |  |  |  |  |  |
| Outside:                   |                              |  |  |  |  |  |  |
| Curb & Gutter (Y/N): Y     |                              |  |  |  |  |  |  |
|                            |                              |  |  |  |  |  |  |

| CLASS | EXTENT | PAVEMENT<br>CONDITION | COMMENTS |
|-------|--------|-----------------------|----------|
|       | S      | Р                     |          |
|       |        | F                     |          |
|       |        | F                     |          |
|       |        | F                     |          |
|       |        | F                     |          |
|       |        | Р                     |          |
|       |        | F                     |          |
|       |        | F                     |          |
|       |        | F                     |          |
|       |        | F                     |          |
|       |        | F                     |          |
|       |        | F                     |          |
|       |        | F                     |          |
|       |        |                       |          |
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|       |        |                       |          |
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