

FLORIDA INSTITUTE OF TECHNOLOGY - CIVIL ENGINEERING DEPARTMENT  
FLORIDA DEPARTMENT OF TRANSPORTATION

BDV28 977-04

## Development and Testing of the Miniaturized Pressuremeter Test for Use in Unbound Pavement Layers

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[2018-GRIP MEETING]

# BACKGROUND

- ✦ *Nuclear Density Gage Testing yields Density and Moisture*
- ✦ *Strength and Stiffness of Pavement Layers is critical*
- ✦ *In situ strength and stiffness pavement properties only available from Pressuremeters*
- ✦ *Pavement Engineers could benefit from small diameter PMT testing in NDG hole*

# OBJECTIVE

Develop and evaluate digital in-situ stress-strain responses for 6 & 12-inch long SDPMT probes using both incremental & rapid strain-controlled tests in 6 & 12 inch unbound pavement layers.



# FIELD TESTING SITES

- FIT Campus Overflow Parking
  - A-3 / SP LBR: 10
- FIT Campus Southgate Intramural Field
  - A-3 / SP LBR: 7
- Cypress Landing Residential Development
  - A-3 / SP LBR: 6
- Saint Johns Heritage Parkway
  - Cemented Coquina Base
  - A-1-b / SW LBR: 99





# FIELD TEST SITES



# FIELD TESTS

- **PMT Probe Sizes**
  - SDPMT – 6-inch
  - SDPMT – 12-inch
- **PMT Test Profiles**
  - Incremental
  - Continuous / Rapid
- **Nuclear Density**
- **Lightweight Deflectometers**
  - Dynatest
  - Zorn
- **Clegg Impact Test**
- **Dynamic Cone Penetrometer**

# LABORATORY TESTS

- Gain Size  
Distribution
- Atterberg Limits
- Moisture Density
- LBR
- Resilient Modulus



# TESTING OBSERVATIONS

- Fits NDG Hole
  - Standard 7/8"
  - Modified SDPMT 3/4"
- Surface Cracking
  - Surcharge Plates
- Drill and Drive
  - 5/8" Bit
  - 3/4" NDG Drive Pin



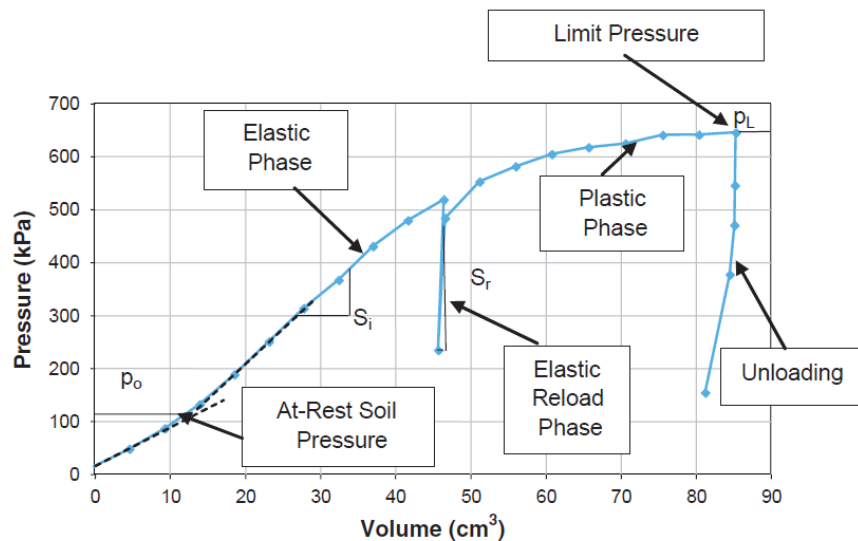


# TESTING SUMMARY

Test	Cypress Landing	FIT Olin Complex	Heritage Parkway	FIT Southgate Field
NDG	24	24	36	24
SDPMT-6 Incremental	0	12	12	12
SDPMT-12 Incremental	11	12	12	12
SDPMT-6 Continuous	0	12	12	12
SDPMT-12 Continuous	10	12	12	11
Zorn LWD	24	12	24	12
Dynatest LWD	12	9	24	12
Clegg Impact	24	24	24	24
DCP	12	12	0	12
Resilient Modulus	6	6	8	6

# TYPICAL PPMT CURVE

## Typical PPMT Curve

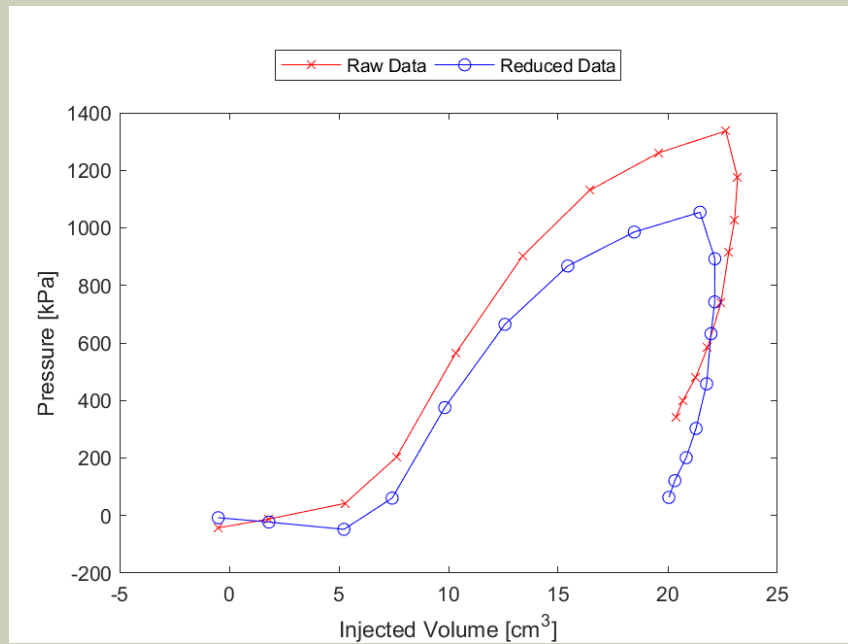


## Key Parameters

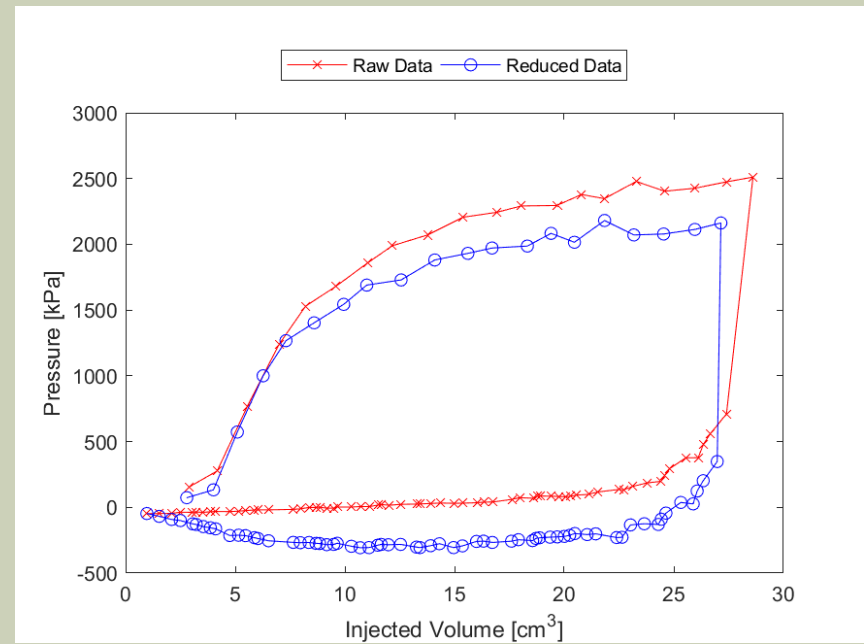
- Observe Elastic Phase
  - Initial Slope ( $S_i$ )
- Observe Plastic Phase
  - Estimate Limit Pressure ( $p_L$ )
- Unloading Phase
  - Strain versus  $1/E$  vs
- At-Rest Soil Pressure
  - Lift-Off Pressure ( $p_0$ )
- Elastic Reload Phase

# TYPICAL SDPMT 6-INCH CURVES

## Incremental (6I)

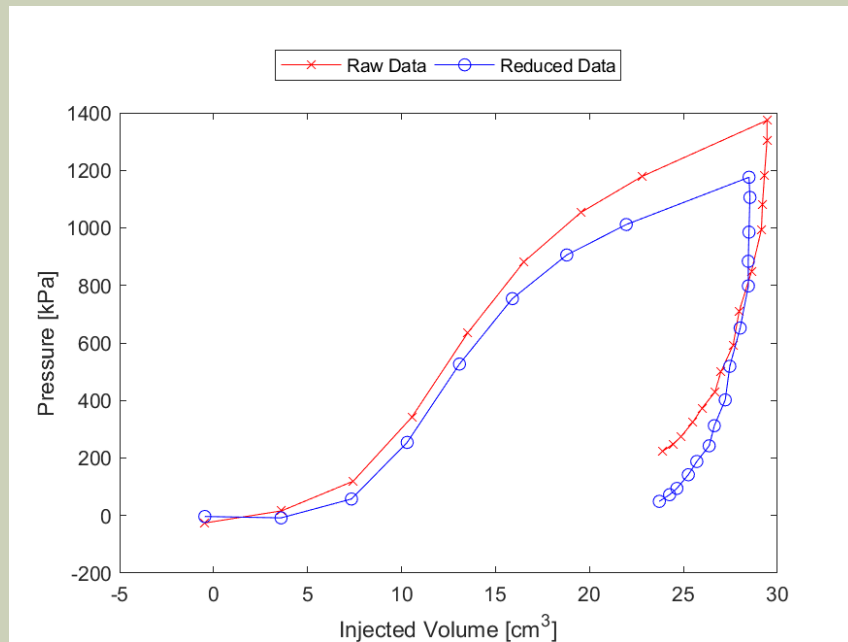


## Continuous / Rapid (6C)

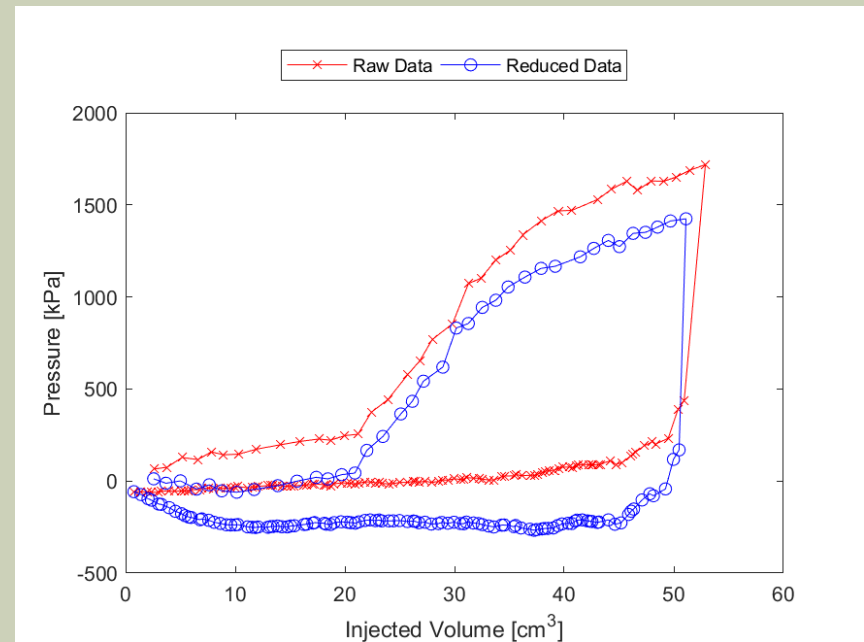


# TYPICAL SDPMT 12-INCH CURVES

## Incremental (12I)



## Continuous / Rapid (12C)





# STRESS – STRAIN RESPONSE CONCLUSIONS

- Observed that the stress – strain response from the incremental and continuous 6 and 12 inch tests resembles those of standard PPMT curve.
- Test quality indicator --  $E_0/P_0$ -- for incremental SDPMT tests average ratio from 7.0 to 16.1 for both 6 and 12 inch probes; similar to Briaud's published ratios of 7 to 12; therefore the test quality is acceptable.
- The test quality indicator --  $E_0/P_0$ -- for rapid or continuous SDPMT tests ranged from 10.9 to 33.2 for 6 and 12 inch probes; although higher than upper range of 12; the tests are still of good quality.
  - Higher values due to the increased strain-rate compared to incremental test.

# STRESS – STRAIN RESPONSE CONCLUSIONS

- $pL/E_0$  for incremental tests ranged from 0.62 to 0.142; Briaud, 1992 estimated ratio of 0.125 and the Cosentino et al. (2008) ratio of 0.079 places the data from these tests in the same general area.
  - The lower values expected because of the stiffer material tested.
- Therefore the developed probes measure realistic stress – strain response of the unbound pavement layers.

# CORRELATION OVERVIEW

## Comparisons Between SDPMT Parameters

- $E_0$  verses  $p_0$
- $p_L$  verses  $p_0$
- $E_0$  verses  $p_L$

## Comparison Between SDPMT Parameters and Other Tests

- $\gamma_{dry}$  and  $\gamma_{wet}$  verses  $E_0, p_0, p_L$
- $E_d$  Zorn LWD verses  $E_0, p_0, p_L$
- $E_0$  Dyanatst LWD verses  $E_0, p_0, p_L$
- CIV verses  $E_0, p_0, p_L$
- DCP Index verses  $E_0, p_0, p_L$

# 5 MODEL TYPES

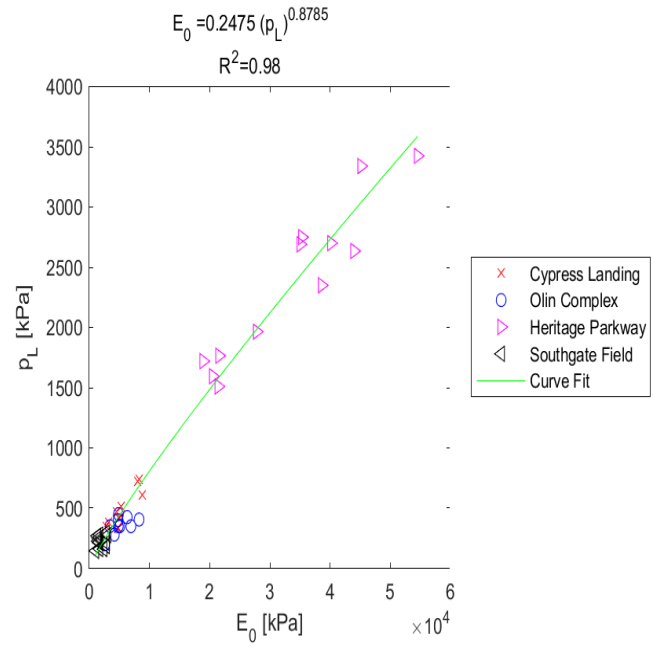
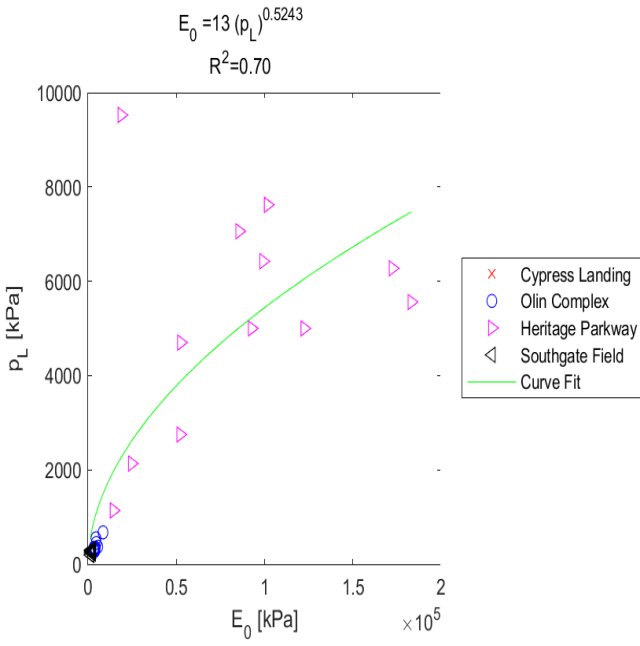
Model Relationship	Generalized Model
Linear	$A = A * X + B$
Log - Linear	$\log_{10}(Y) = A * X + B$
Linear - Log	$Y = A \log_{10}(X) + B$
Log - Log	$\log_{10}(Y) = A \log_{10}(X) + B$
Exponential	$Y = A * (X)^B$



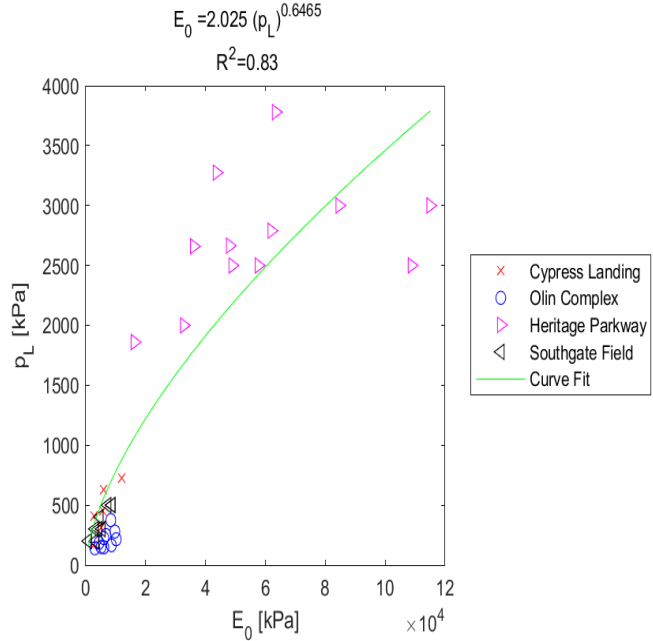
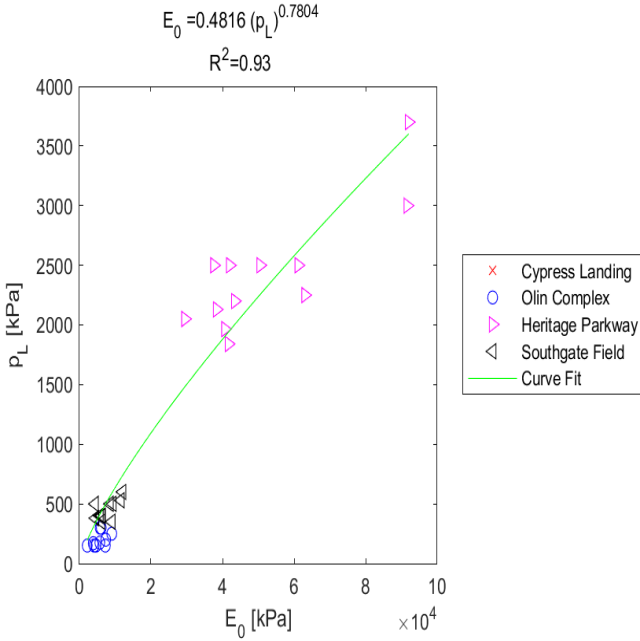
# SDPMT INTERNAL COMPARISONS

		Linear	Log-Linear	Linear-Log	Log-Log	Exponential
E0 vs. p0	6I	0.10	0.12	0.13	0.16	0.10
	6C	0.09	0.24	0.19	0.39	0.16
	12I	0.42	0.47	0.46	0.47	0.48
	12C	0.06	0.09	0.12	0.16	0.11
pL vs. p0	6I	0.09	0.10	0.12	0.13	0.10
	6C	0.20	0.29	0.34	0.43	0.29
	12I	0.43	0.50	0.47	0.53	0.49
	12C	0.12	0.10	0.19	0.18	0.18
E0 vs. pL	6I	0.60	0.74	0.67	0.91	0.63
	6C	0.91	0.91	0.76	0.90	0.92
	12I	0.98	0.84	0.86	0.93	0.98
	12C	0.75	0.83	0.67	0.81	0.75

# 6-in Incremental



# 6-in Continuous

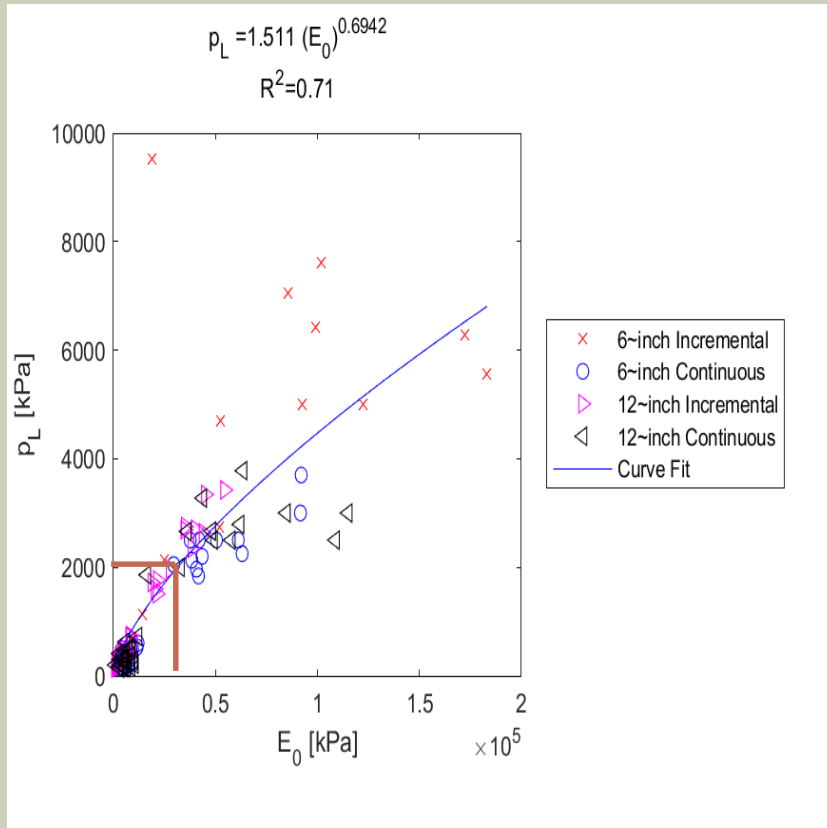


# 12-in Incremental

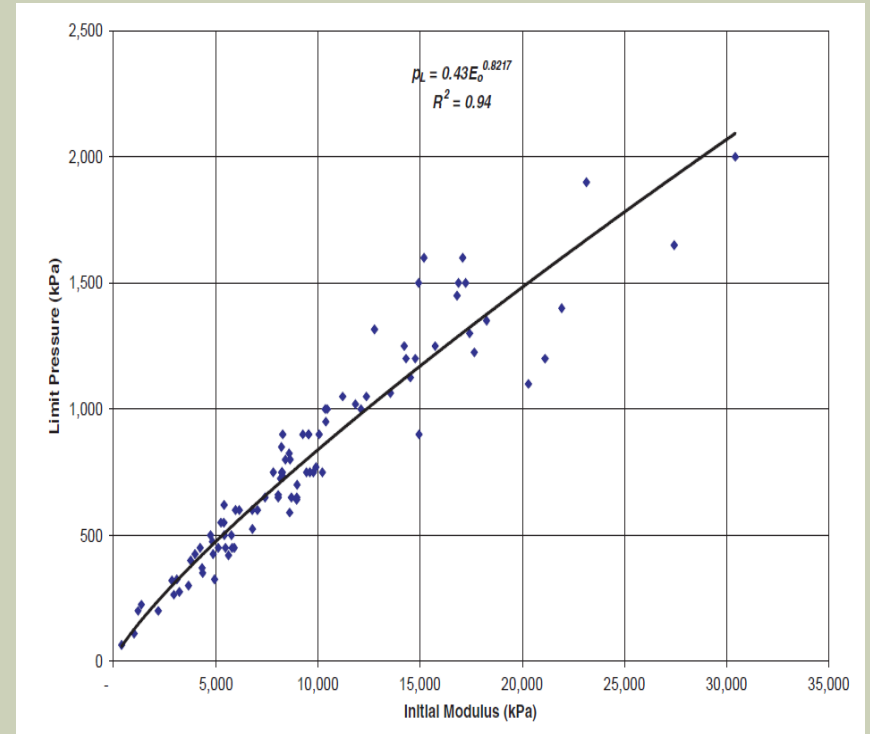
# 12-in Continuous

# COMPARISON TO EXISTING CORRELATION

## Project



## Previous -- Silty Sands



Cosentino, Paul J, Kalajian, Edward, Messaoud, Farid, Sundaram, Sunil, Misilo, Thaddeus J, and Horhota, David J. "Correlations between PENCIL pressuremeter, cone penetrometer, and dilatometer parameters." Transportation Research Record: Journal of the Transportation Research Board 2053 (2008).1: 65-71.

# CONCLUSIONS FOR $p_L$ VERSES $E_0$

- Data collected during this research shows an excellent correlation between  $p_L$  and  $E_0$ .
- An exponential relationship exists between  $p_L$  and  $E_0$ .
- SDPMT test data shows similar results to work by Cosentino et al. for the relationship between  $p_L$  and  $E_0$

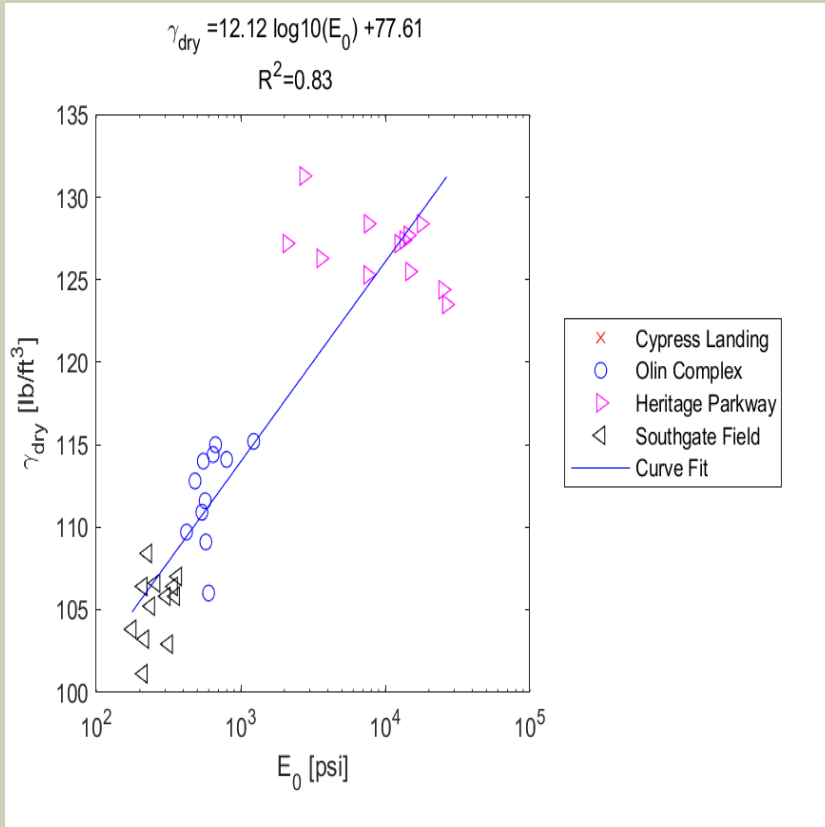


# DRY UNIT WEIGHT COMPARISONS

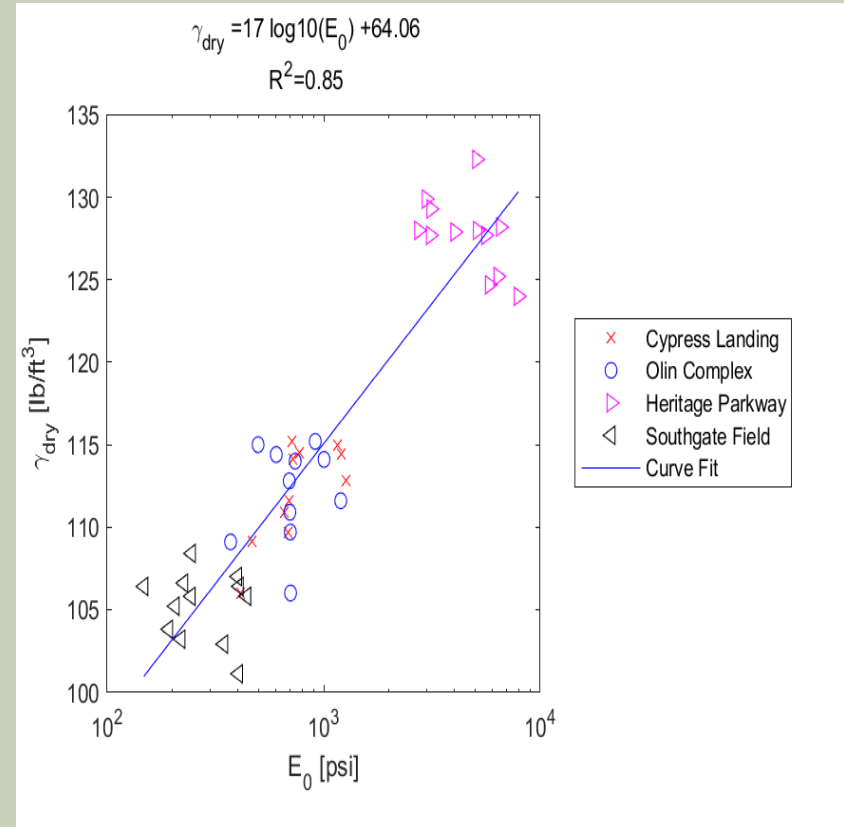
		linear	Linear-Log	log-linear	log-log	Exponential
$\gamma_{dry}$ vs. $E_0$	6I	0.46	0.46	0.83	0.83	0.81
	6C	0.64	0.63	0.72	0.74	0.73
	12I	0.69	0.68	0.85	0.85	0.85
	12C	0.54	0.54	0.74	0.74	0.75
$\gamma_{dry}$ vs. $p_0$	6I	0.11	0.11	0.14	0.14	0.14
	6C	0.38	0.37	0.46	0.45	0.46
	12I	0.47	0.46	0.40	0.40	0.41
	12C	0.22	0.22	0.33	0.33	0.33
$\gamma_{dry}$ vs. $p_L$	6I	0.69	0.67	0.87	0.86	0.86
	6C	0.73	0.71	0.61	0.59	0.63
	12I	0.74	0.73	0.86	0.85	0.86
	12C	0.78	0.76	0.71	0.70	0.73

# LOG-LINEAR MODELS OF $\gamma_{\text{DRY}}$ VERSES $E_0$

## SDPMT-6 Incremental

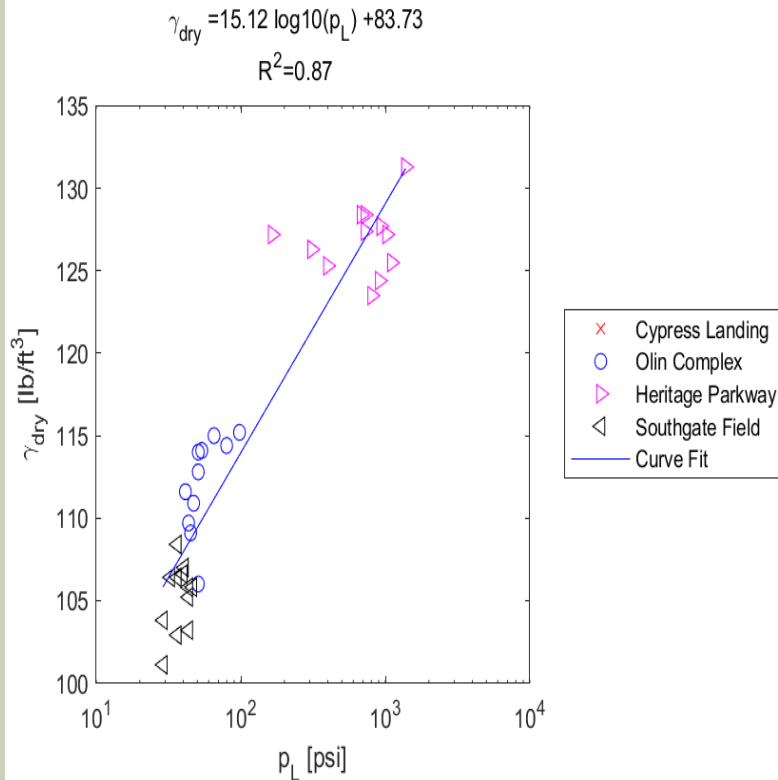


## SDPMT-12 Incremental

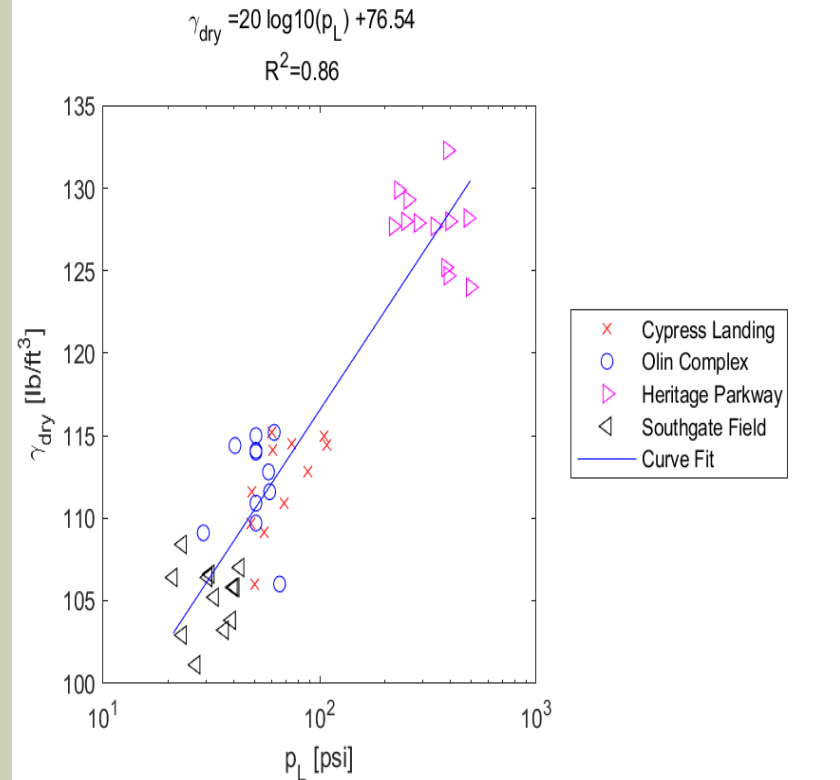


# LOG-LINEAR MODELS OF $\gamma_{\text{DRY}}$ VERSES $p_L$

## SDPMT-6 Incremental



## SDPMT-12 Incremental



# CORRELATIONS WITH $\gamma_{\text{DRY}}$

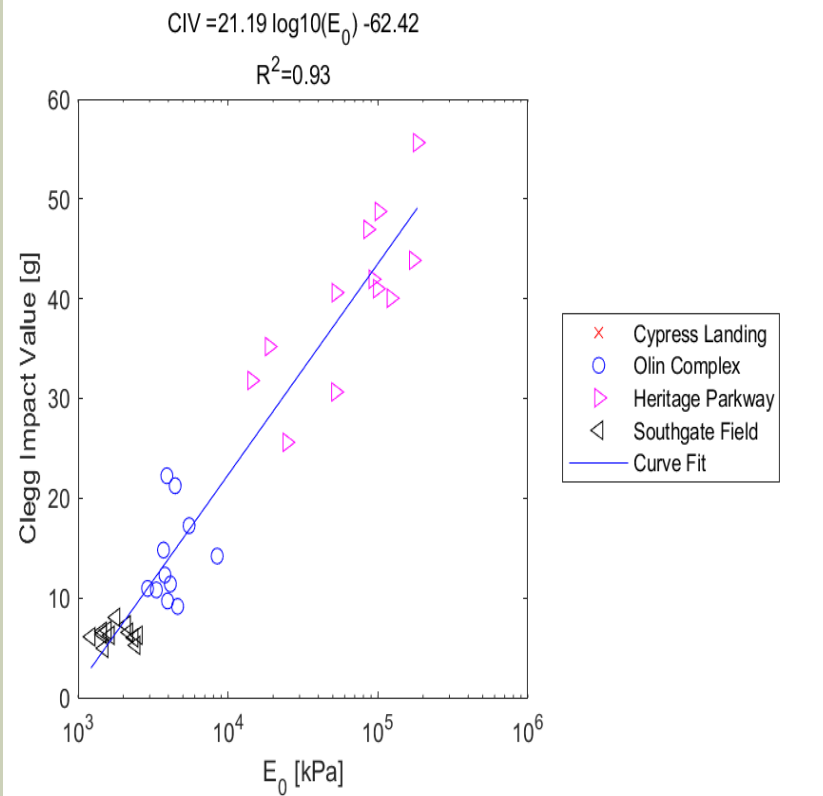
- **Conclusions for  $\gamma_{\text{dry}}$  and  $\gamma_{\text{wet}}$  verses  $E_0$** 
  - Data collected during this research shows an excellent correlation with  $\gamma_{\text{wet}}$ ,  $\gamma_{\text{dry}}$  and  $E_0$  for all test configurations.
  - An logarithmic relationship exists between  $\gamma$  and  $E_0$  for the incremental and continuous SDPMT test with both 6 and 12 inch probes.
  
- **Conclusions for  $\gamma_{\text{dry}}$  and  $\gamma_{\text{wet}}$  verses  $p_L$** 
  - Data collected during this research shows an excellent correlation with  $\gamma_{\text{wet}}$ ,  $\gamma_{\text{dry}}$  and  $p_L$  for all test configurations.
  - An logarithmic relationship exists between  $\gamma$  and  $p_L$  for the incremental and continuous SDPMT test with both 6 and 12 inch probes.

# CLEGG IMPACT TEST COMPARISONS

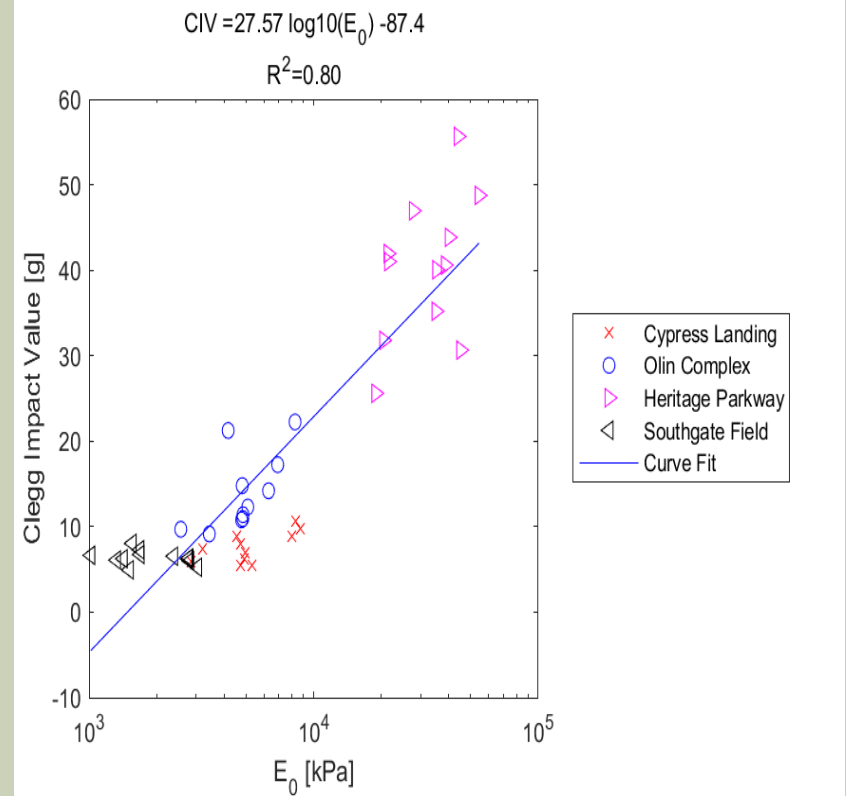
		Log-Linear	Linear-Log	log-linear	log-log	Exponential
CIV vs. $E_0$	6I	0.76	0.59	0.93	0.88	0.90
	6C	0.70	0.63	0.73	0.65	0.75
	12I	0.83	0.75	0.80	0.81	0.86
	12C	0.72	0.64	0.79	0.78	0.80
CIV vs. $p_0$	6I	0.12	0.08	0.15	0.12	0.14
	6C	0.28	0.26	0.39	0.34	0.37
	12I	0.49	0.45	0.44	0.37	0.51
	12C	0.04	0.09	0.17	0.24	0.15
CIV vs. $p_L$	6I	0.78	0.67	0.90	0.83	0.87
	6C	0.79	0.69	0.65	0.52	0.77
	12I	0.79	0.69	0.65	0.52	0.77
	12C	0.79	0.71	0.68	0.58	0.78

# LOG-LINEAR MODELS OF CIV VERSES $E_0$

## SDPMT-6 Incremental

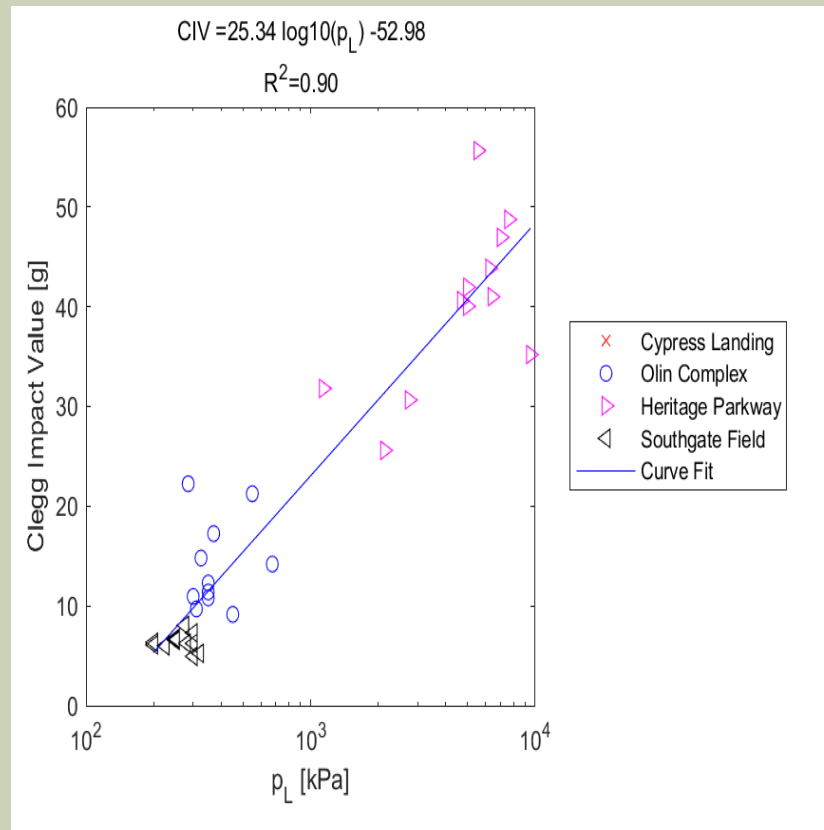


## SDPMT-12 Incremental



# LOG-LINEAR MODELS OF CIV VERSES $p_L$

## SDPMT-6 Incremental



# CIV CONCLUSIONS

- CIV verses SDPMT  $E_0$ 
  - Data shows a good logarithmic correlation ( $0.80 < R^2 < 0.93$ ) with the Clegg impact test value (CIV) and the SDPMT initial moduli ( $E_0$ ) for 6 inch and 12 inch incremental tests.
- CIV verses SDPMT  $p_L$ 
  - Data excellent logarithmic correlation ( $R^2 = 0.90$ ) with the Clegg impact test value (CIV) and the SDPMT initial moduli ( $p_L$ ) for 6 and 12 inch incremental tests.



# LWD – DYNATEST COMPARISONS

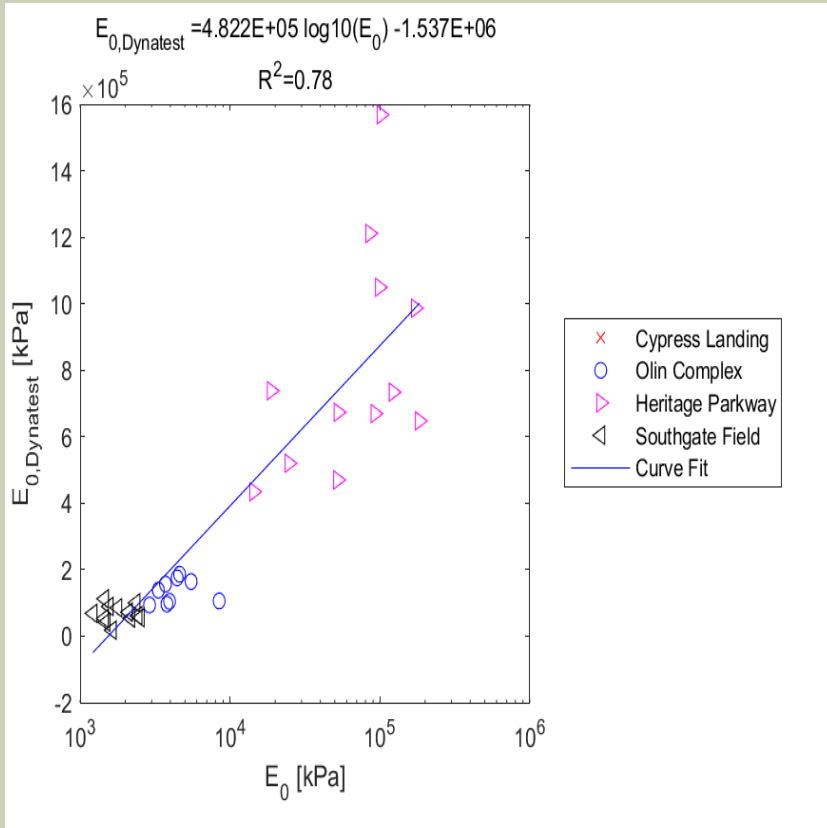
		Log-Linear	Linear-Log	log-linear	log-log	Exponential
$E_{d,zorn}$ vs. $E_0$	6I	0.63	0.55	0.89	0.86	0.82
	6C	0.83	0.69	0.85	0.72	0.87
	12I	0.81	0.70	0.83	0.83	0.86
	12C	0.78	0.63	0.82	0.73	0.86
$E_{d,zorn}$ vs. $p_L$	6I	0.79	0.69	0.93	0.86	0.88
	6C	0.88	0.75	0.76	0.61	0.88
	12I	0.83	0.71	0.86	0.80	0.86
	12C	0.88	0.74	0.79	0.64	0.88

# LWD – ZORN COMPARISONS

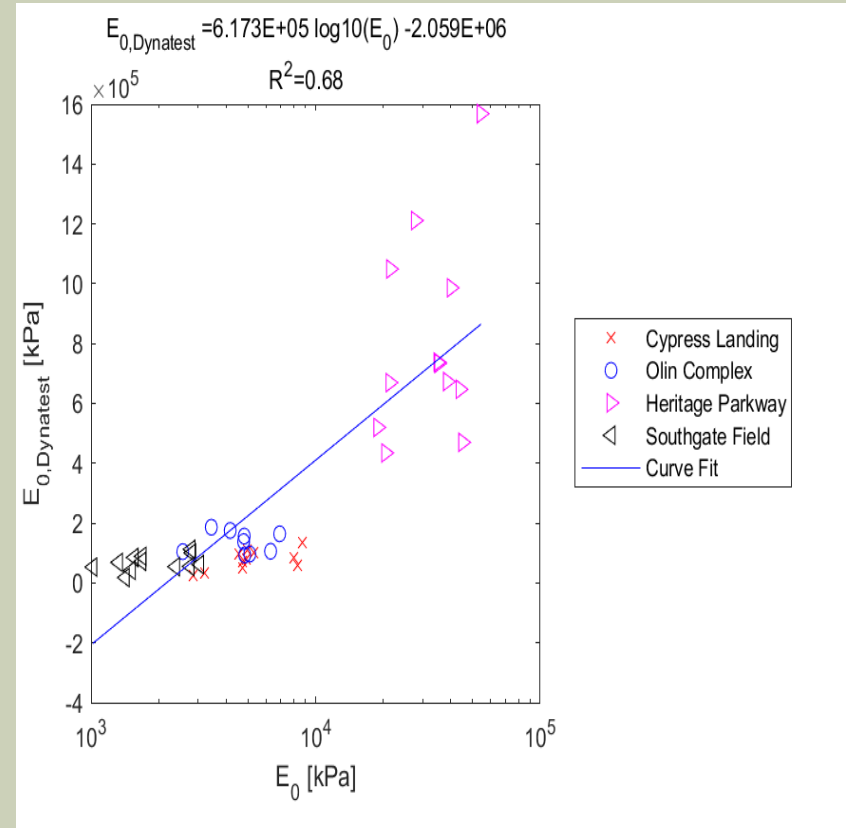
		Log-Linear	Linear-Log	log-linear	log-log	Exponential
$E_{0,dyn}$ vs. $E_0$	6I	0.62	0.58	0.78	0.86	0.75
	6C	0.82	0.72	0.74	0.72	0.82
	12I	0.77	0.74	0.68	0.78	0.77
	12C	0.84	0.70	0.75	0.77	0.85
$E_{0,dyn}$ vs. $p_L$	6I	0.84	0.75	0.84	0.86	0.86
	6C	0.82	0.78	0.68	0.65	0.83
	12I	0.76	0.74	0.70	0.74	0.76
	12C	0.74	0.76	0.67	0.67	0.74

# LOG-LINEAR CORRELATIONS, $E_{0,DYNATEST}$ VERSES $E_0$

## SDPMT-6 Incremental

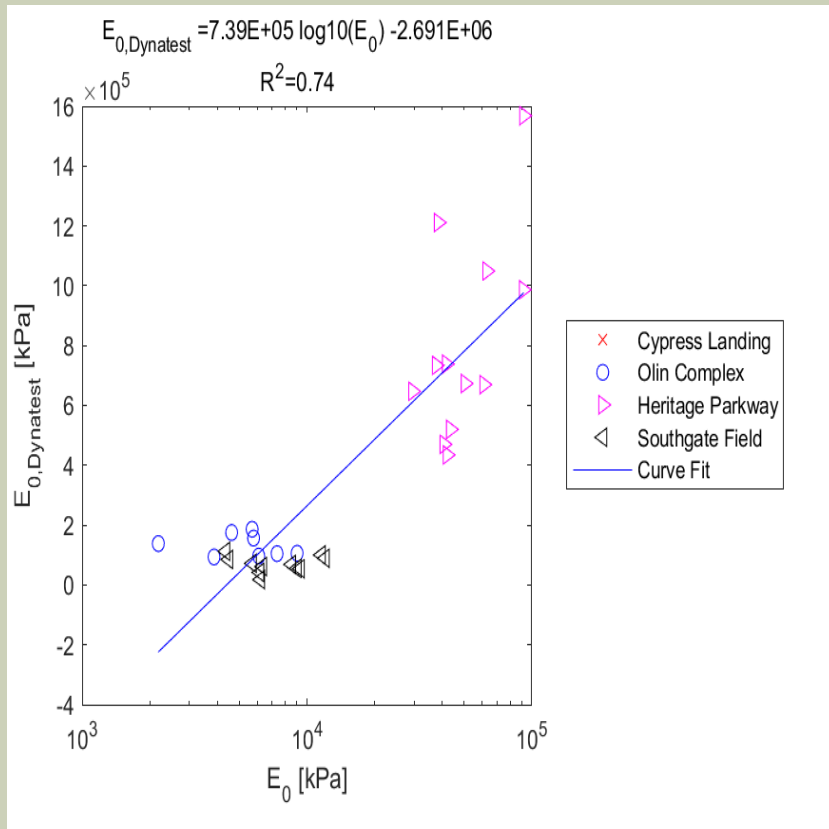


## SDPMT-12 Incremental

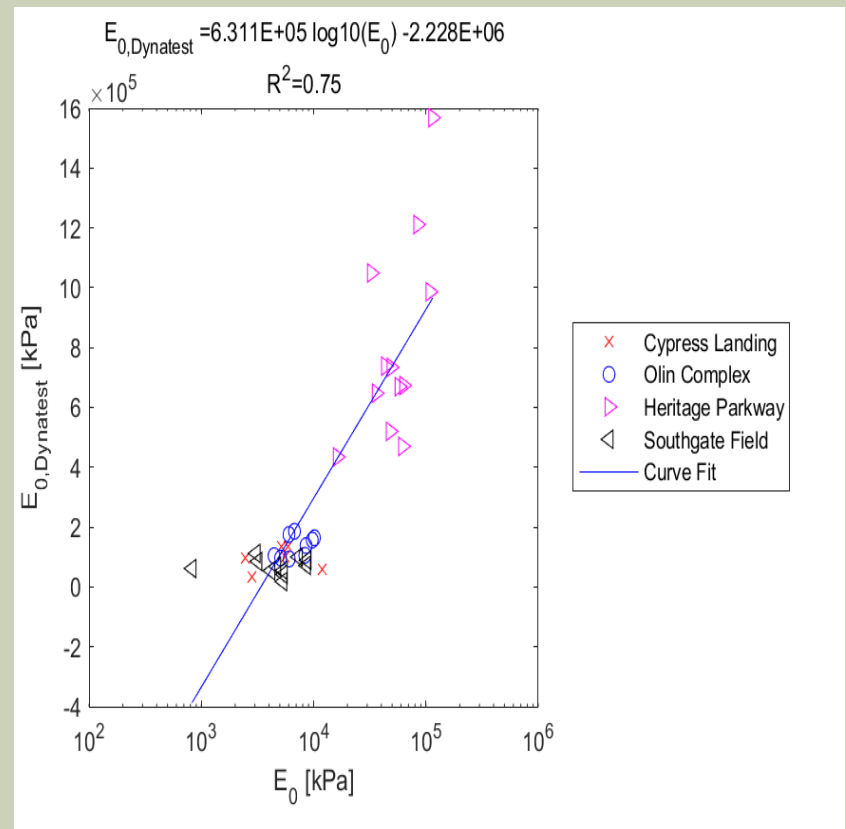


# LOG-LINEAR CORRELATIONS, $E_{0,DYNATEST}$ VERSES $E_0$

## SDPMT-6 Continuous

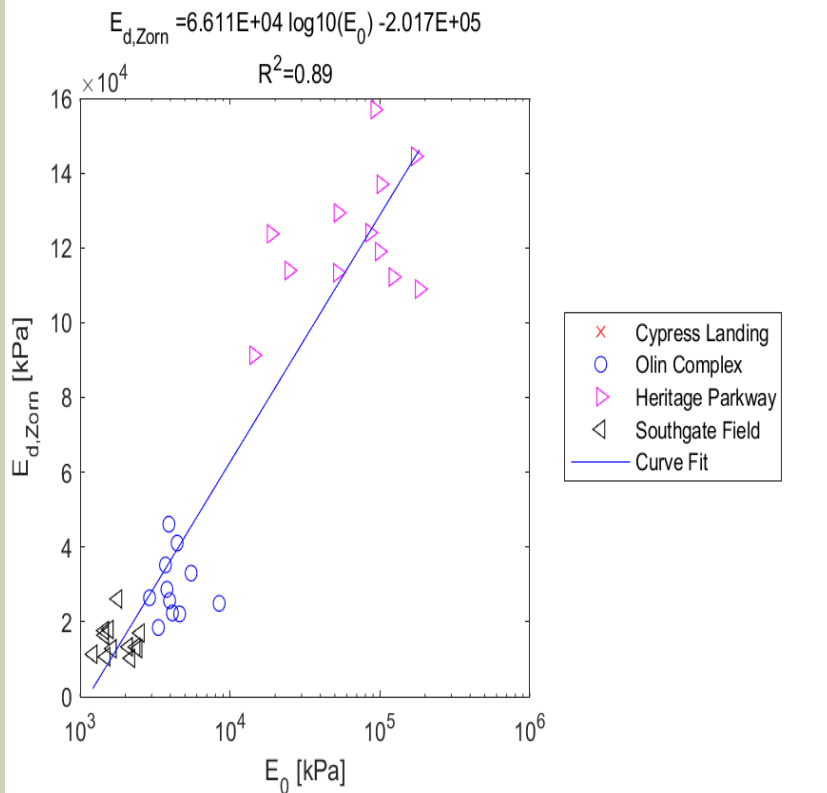


## SDPMT-12 Continuous

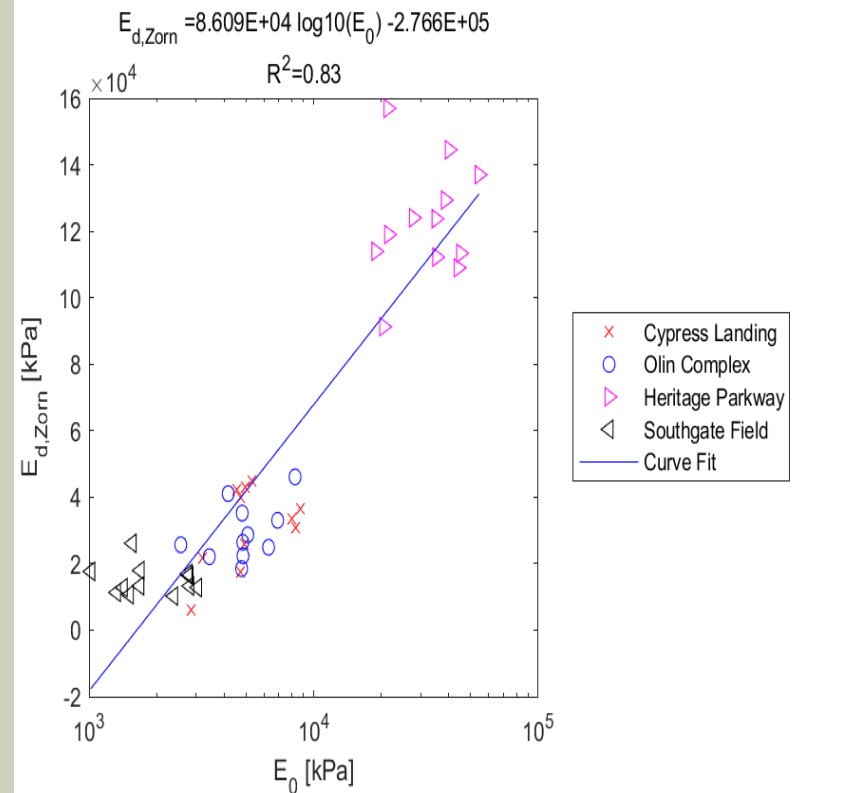


# LOG-LINEAR CORRELATIONS, $E_{D,ZORN}$ VERSES $E_0$

## SDPMT-6 Incremental

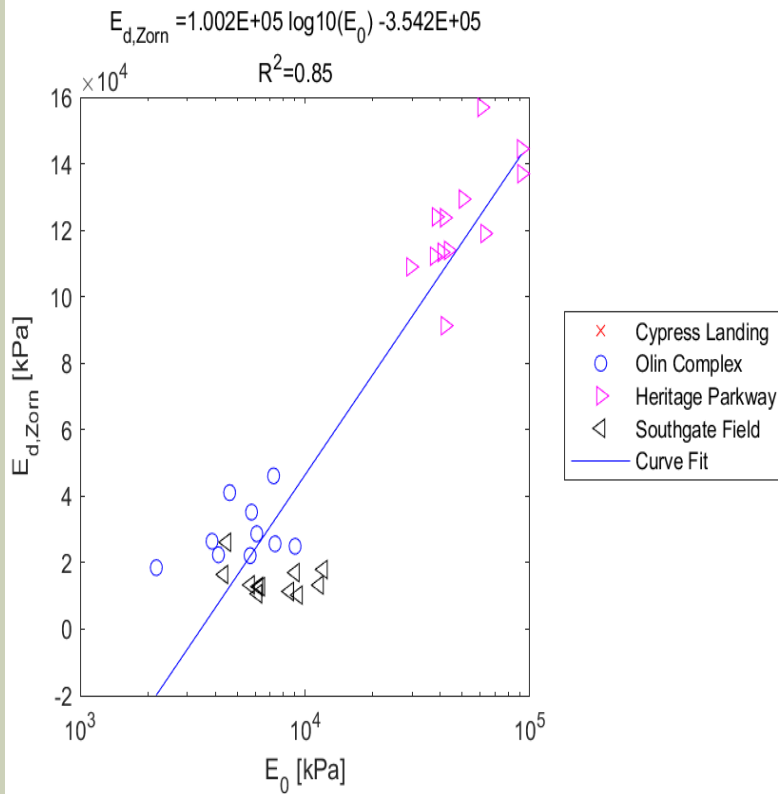


## SDPMT-12 Incremental

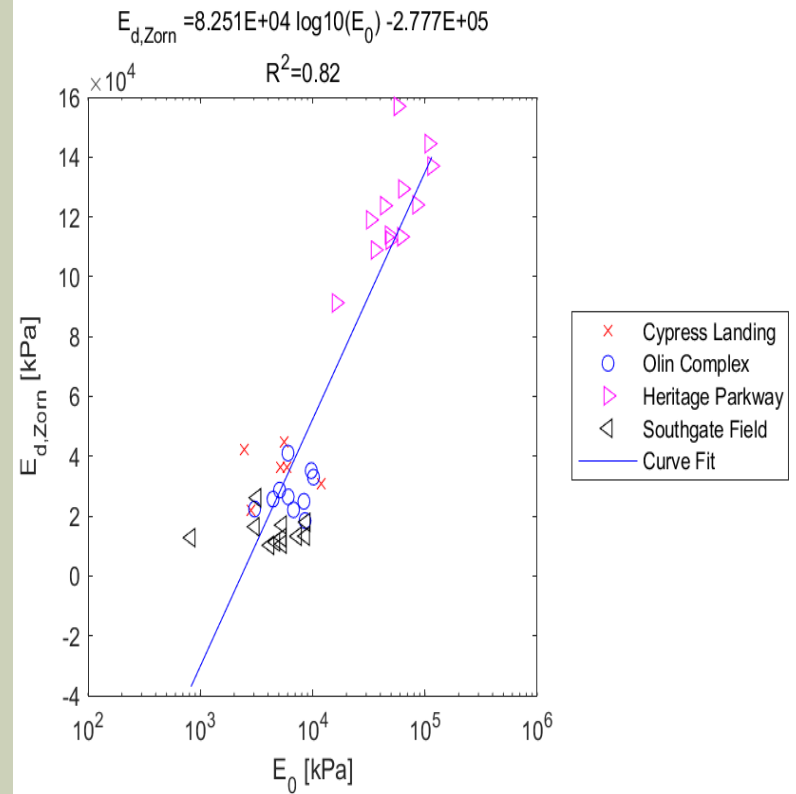


# LOG-LINEAR CORRELATIONS, $E_{D,ZORN}$ VERSES $E_0$

## SDPMT-6 Continuous

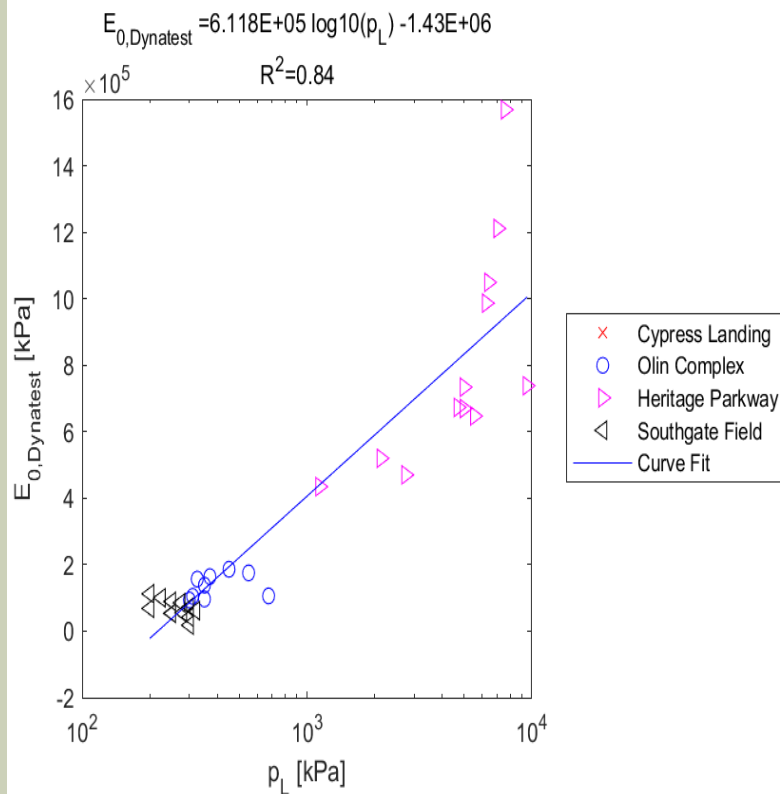


## SDPMT-12 Continuous

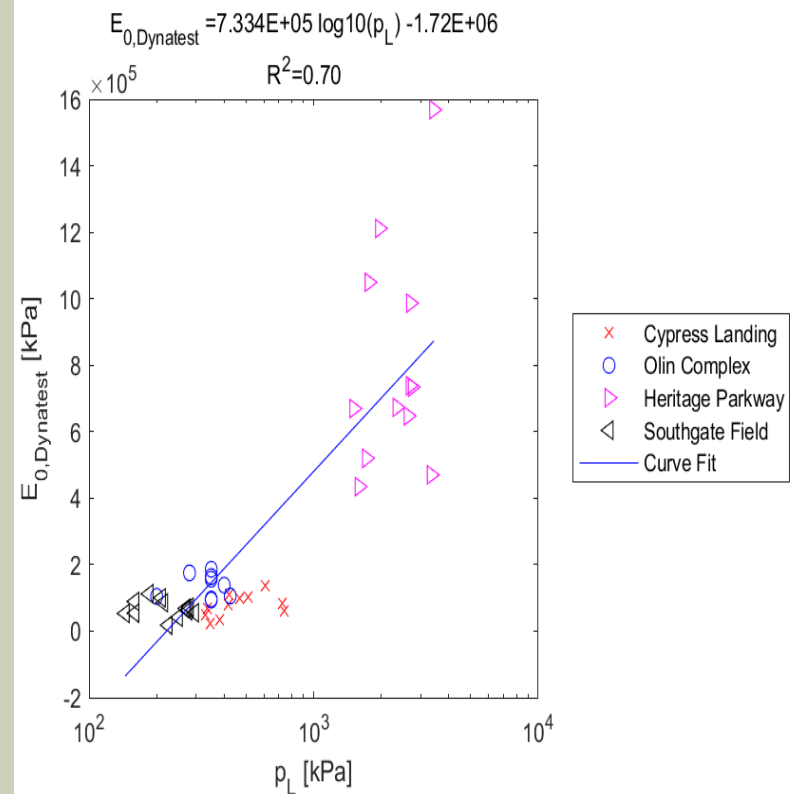


# LOG-LINEAR CORRELATIONS, $E_{0,DYNATEST}$ VERSES $p_L$

## SDPMT-6 Incremental

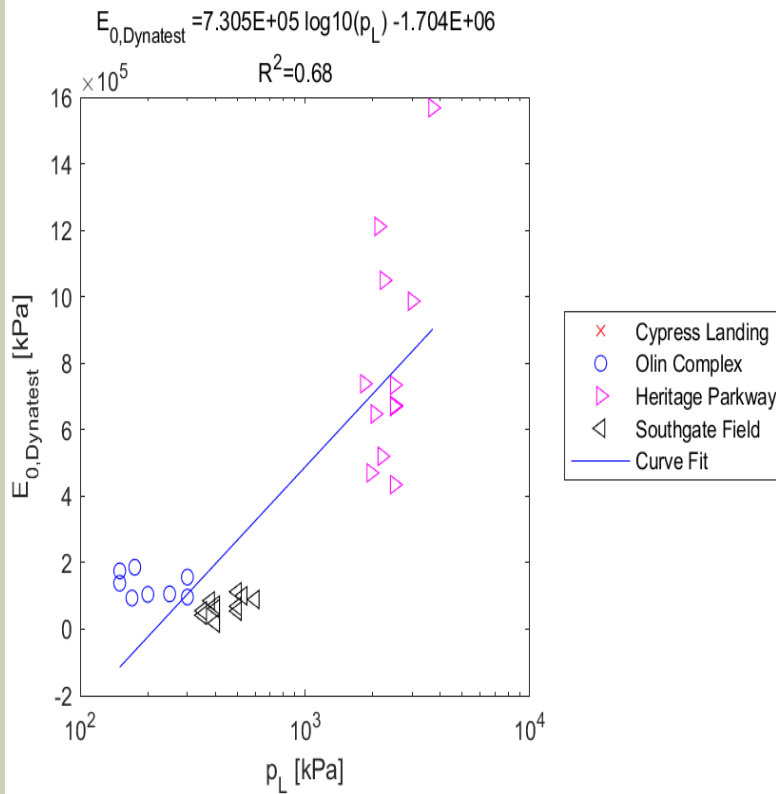


## SDPMT-12 Incremental

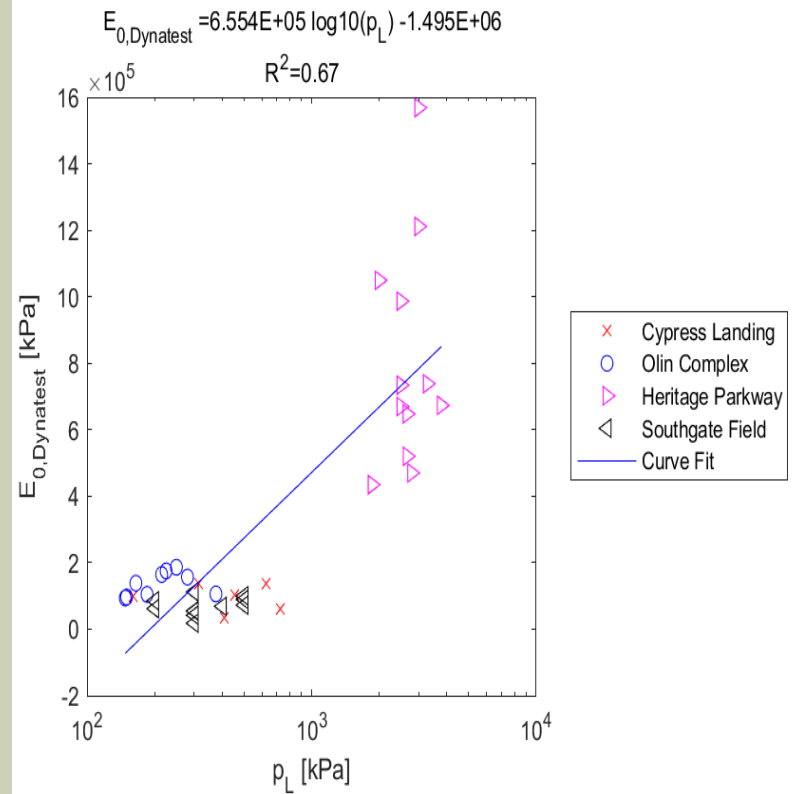


# LOG-LINEAR CORRELATIONS, $E_{0,DYNATEST}$ VERSES $p_L$

## SDPMT-6 Continuous



## SDPMT-12 Continuous





# LWD CONCLUSIONS

- Dynatest LWD  $E_0$  verses SDPMT  $E_0$ 
  - Data shows a good logarithmic correlation ( $0.68 < R^2 > 0.75$ ) with the Dynatest LWD moduli ( $E_0$ ) and initial moduli ( $E_0$ ) for all SDPMT test configurations.
- Zorn LWD  $E_d$  verses  $E_0$ 
  - Data shows an excellent logarithmic correlation with the Zorn LWD deformation moduli ( $E_d$ ) and  $E_0$  for all SDPMT test configurations.

# SDPMT TO DCP COMPARISONS

		Log-Linear	Linear-Log	log-linear	log-log	Exponential
DCP vs. $E_0$	6I	0.57	0.58	0.68	0.69	0.65
	6C	0.16	0.13	0.16	0.13	0.16
	12I	0.38	0.34	0.47	0.38	0.48
	12C	0.14	0.15	0.13	0.13	0.12
DCP vs. $p_0$	6I	0.06	0.03	0.00	0.00	0.01
	6C	0.10	0.12	0.11	0.15	0.11
	12I	0.04	0.08	0.13	0.15	0.11
	12C	0.13	0.05	0.33	0.18	0.33
DCP vs. $p_L$	6I	0.34	0.34	0.39	0.40	0.39
	6C	0.64	0.62	0.67	0.65	0.64
	12I	0.19	0.10	0.29	0.17	0.36
	12C	0.13	0.28	0.20	0.26	0.17

# DCP INDEX CONCLUSIONS

- Based on the data collected no correlation between the DCP Index and the SDPMT  $p_0$ ,  $p_L$  or  $E_0$  exists.

# RECOMMENDATIONS

- Continued Development / Evaluation of Continuous Test Procedure
- Evaluation of the Use of Surcharge Weights to Evaluate Surface Cracking
- Evaluate Drill / Drive Method of Hole Construction

# QUESTIONS ?

