| POLE SELECTION TABLE - SINGLE ARM - WITH \& WITHOUT LUMINAIRE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Arm Length | BI | B3 | B5 | B6 | $B 7$ |
| Pole Type | Q1 \& Q21 Lum | Q2 \& Q22 Lum | Q3 \& Q23 Lum | Q4 \& Q24 Lum | Q6 |


| pole selection table - double arm - without luminaire |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Arm Lengths | $B 1-B I$ | B3-BI | B5-B2 | B6-B2 | B4-B4 | B5-B4 | B6-B4 | B5-B5 | B6-B5 | B6-B6 |
| Pole Type | Q/ | Q2 | Q3 | Q4 | Q3 | Q4 | Q4 | Q4 | Q4 | Q5 |

Arm I Is IIsted first

| arm design table - all cases |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ARM TYPE | ARM LENGTH | MAST ARM |  |  |  | ARM EXTENSION |  |  |  | ARM CONNECTION \& WELDS |  |  |  |  |
|  |  | FA(ft) | FB(I) | FC(In) | FD(In) | FE(ft) | FF(İ) | FG(In) | FH(In) | HT(In) | FJ/SJ(In) | FK/SK(In) | FM/SM(In) | FQ/SQ(In) |
| BI | $36^{\prime}-0^{\prime \prime}$ | 36 | 7.96 | 13 | 0.1793 | - | - | - | - | 20 | 25 | 2.25 | 0.125 | 0.313 |
| B2 | $36^{\prime}-0^{\prime \prime}$ | 36 | 7.96 | 13 | 0.1793 | - | - | - | - | 30 | 36 | 3 | 0.125 | 0.313 |
| B3 | $46^{\prime}-0^{\prime \prime}$ | 36.3 | 7.92 | 13 | 0.7793 | 11.7 | 12.36 | 14 | 0.25 | 20 | 25 | 2.25 | 0.188 | 0.438 |
| B4 | $46^{\prime}-0^{\prime \prime}$ | 36.3 | 7.92 | 13 | 0.1793 | 11.7 | 12.36 | 14 | 0.25 | 30 | 36 | 3 | 0.188 | 0.438 |
| B5 | $60^{\prime}-0^{\prime \prime}$ | 36 | 7.96 | 13 | 0.1793 | 26 | 12.36 | 16 | 0.313 | 30 | 36 | 3 | 0.25 | 0.5 |
| B6 | $70^{\prime}-6^{\prime \prime}$ | 39.4 | 9.49 | 15 | 0.793 | 33.1 | 14.36 | 19 | 0.313 | 30 | 36 | 3 | 0.25 | 0.5 |
| B7 | $78^{\prime}-0^{\prime \prime}$ | 40 | 8.44 | 14 | 0.793 | 40 | 13.40 | 19 | 0.313 | 30 | 36 | 3 | 0.25 | 0.563 |

Arm Camber Angle $=2$ degres

| Pole, connection and shaft design table - Single \& double ark |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| POLE TYPE | UA(ft) | UC(In) | UD(In) | UE(In) | UG(ft) | UPRIGHT BASE CONNECTION |  |  |  |  |  |  | CONNECTION PLATE DATA |  |  |  |  |  |  |  |  | DRILLED SHAFT DATA |  |  |  |
|  |  |  |  |  |  | No. Bolts | $\begin{aligned} & B A \\ & (I n) \end{aligned}$ | $\begin{aligned} & B B \\ & (I n) \\ & (n) \end{aligned}$ | $\begin{aligned} & B C \\ & \hline(I n) \end{aligned}$ | $\begin{aligned} & B D \\ & (I n) \end{aligned}$ | $\begin{aligned} & \begin{array}{l} B E \\ (I n) \end{array} \end{aligned}$ | $\begin{aligned} & B F \\ & (I n) \end{aligned}$ | $\begin{aligned} & H T \\ & (I n) \end{aligned}$ | $\begin{gathered} \hline \text { FJ/SJ } \\ (I n) \\ \hline \end{gathered}$ | $\begin{gathered} F L / S L \\ (I n) \\ \hline \end{gathered}$ | $\begin{gathered} F N / S N \\ (I n) \end{gathered}$ | $\begin{gathered} \text { FO/SO } \\ (\mathrm{In}) \end{gathered}$ | $\begin{gathered} F P / S P \\ (I n) \\ \hline \end{gathered}$ | $\begin{gathered} F R / S R \\ (I n) \end{gathered}$ | $\begin{gathered} F S / S S \\ (I n) \end{gathered}$ | $\begin{gathered} F T / S T \\ (I n) \end{gathered}$ | $\begin{aligned} & \text { DA } \\ & (f t) \end{aligned}$ | $\begin{aligned} & \text { DB } \\ & (f f) \end{aligned}$ | RA | $R B$ |
| Q/ | 24 | 12.64 | 16 | 0.313 | - | 6 | 30 | 1.5 | 1.75 | 0.313 | 0.25 | 36 | 20 | 25 | 0.75 | 0.438 | 15.5 | 1 | 2 | 8 | 0.438 | 13 | 3.5 | 9 | 14 |
| Q2 | 24 | 14.64 | 18 | 0.313 | - | 6 | 32 | 1.5 | 1.75 | 0.313 | 0.25 | 36 | 20 | 25 | 0.75 | 0.438 | 15.5 | 1 | 2 | 8 | 0.438 | 13 | 4 | 9 | 19 |
| Q3 | 24 | 18.64 | 22 | 0.313 | - | 6 | 38 | 1.5 | 2 | 0.313 | 0.2 | 42 | 30 | 36 | 0.75 | 0.438 | 21.5 | 1.25 | 2.25 | 12. | 0.43 | 13 | 4.5 | 9 | 23 |
| Q4 | 24 | 21.64 | 25 | 0.313 | - | 6 | 41 | 1.5 | 2 | 0.313 | 0.25 | 42 | 30 | 36 | 0.75 | 0.438 | 21.5 | 1.25 | 2.25 | 12.5 | 0.438 | 18 | 4.5 | 9 | 23 |
| Q5 | 24 | 23.64 | 27 | 0.313 | - | 6 | 43 | 1.5 | 2 | 0.313 | 0.25 | 42 | 30 | 36 | 0.75 | 0.438 | 21.5 | 1.25 | 2.25 | 12.5 | 0.438 | 19 | 4.5 | 9 | 23 |
| Q6 | 24 | 21.64 | 25 | 0.313 | - | 6 | 41 | 1.5 | 2 | 0.313 | 0.25 | 42 | 30 | 36 | 0.75 | 0.438 | 16 | 1.25 | 2.25 | 12.5 | 0.438 | 16 | 4.5 | 9 | 23 |
| Q21 Lum | 39 | 10.54 | 16 | 0.313 | 37.5 | 6 | 30 | 1.75 | 1.75 | 0.313 | 0.25 | 36 | 20 | 25 | 0.75 | 0.438 | 11.5 | 1 | 2 | 8 | 0.438 | 12 | 3.5 | 9 | 14 |
| Q22 Lum | 39 | 12.54 | 18 | 0.313 | 37.5 | 6 | 32 | 1.75 | 1.75 | 0.313 | 0.25 | 36 | 20 | 25 | 0.75 | 0.438 | 12.5 | 1 | 2 | 8 | 0.438 | 12 | 4 | 9 | 19 |
| Q23 Lum | 39 | 16.54 | 22 | 0.313 | 37.5 | 6 | 38 | 1.75 | 2 | 0.313 | 0.25 | 42 | 30 | 36 | 0.75 | 0.438 | 14.5 | 1.25 | 2.25 | 12.5 | 0.438 | 13 | 4.5 | 9 | 23 |
| Q24 Lum | 39 | 19.54 | 25 | 0.313 | 37.5 | 6 | 41 | 1.75 | 2 | 0.313 | 0.25 | 42 | 30 | 36 | 0.75 | 0.438 | 16 | 1.25 | 2.25 | 12.5 | 0.438 | 16 | 4.5 |  | 23 |

1. Work thls Index with Index No. 17745 .

Standard Mast Arm "B" Assembles are designed to Looding Trees as Indlcoted In Index No. 17741 for Design Wind Speed $=110$ mph wlth Slgnal Backplates.

| POLE SELECTION TABLE - SINGLE ARM - WITH \& WITHOUT LUMINAIRE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Arm Length | $C l$ | $C 3$ | $C 5$ | $C 6$ | $C 7$ |
| Pole Type | $R 1 \& R 21$ Lum | $R 2 \& R 22$ Lum | $R 3 \& R 23$ Lum | $R 4 \& R 24$ Lum | $R 6$ |


| pole selection table - double arm - without luminaire |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Arm Lengths | $C l-c l$ | C3-Cl | C5-C2 | C6-C2 | C4-C4 | C5-C4 | C6-C4 | C5-C5 | C6-C5 | C6-C6 |
| Pole Type | R/ | R2 | R3 | R4 | R3 | R4 | R4 | R4 | R4 | R5 |

Arm I Is Isted first

| arm design table - all cases |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ARM TYPE | ARM LENGTH | MAST ARM |  |  |  | ARM EXTENSION |  |  |  | ARM CONNECTION \& WELDS |  |  |  |  |
|  |  | FA(ft) | FB(In) | FC(In) | FD(In) | $F E(f t)$ | FF(II) | FG( 1 ) | FH(In) | HT(İ) | FJ/SJ(In) | FK/SK(In) | FM/SM(In) | FQ/SQ(In) |
| Cl | $36^{\prime}-0^{\prime \prime}$ | 36 | 5.96 | 11 | 0.1793 | - | - | - | - | 20 | 20 | 2 | 0.125 | 0.25 |
| c2 | $36^{\prime}-0^{\prime \prime}$ | 36 | 5.96 | " | 0.793 | - | - | - | - | 29 | 29 | 2.25 | 0.125 | 0.25 |
| C3 | $46^{\prime}-0^{\prime \prime}$ | 36.3 | 5.92 | " | 0.793 | 11.7 | 10.36 | 12 | 0.25 | 20 | 20 | 2 | 0.188 | 0.375 |
| C4 | $46^{\prime}-0^{\prime \prime}$ | 36.3 | 5.92 | " | 0.793 | 11.7 | 10.36 | 12 | 0.25 | 29 | 29 | 2.25 | 0.188 | 0.375 |
| C5 | $60^{\prime}-0^{\prime \prime}$ | 36 | 5.96 | " | 0.793 | 26 | 10.36 | 14 | 0.313 | 29 | 29 | 2.25 | 0.25 | 0.438 |
| c6 | $70^{\prime}-6^{\prime \prime}$ | 39.4 | 5.49 | / | 0.793 | 33.1 | 10.36 | 15 | 0.313 | 29 | 29 | 2.25 | 0.25 | 0.5 |
| C7 | $78^{\prime}-0^{\prime \prime}$ | 40 | 6.44 | 12 | 0.1793 | 40 | 11.40 | 17 | 0.313 | 30 | 30 | 2.25 | 0.25 | 0.5 |

Arm Camber Angle $=2$ degrees

* See Note 3

| POLE, CONNECTION AND Shaft design table - SINGLE \& double ark |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| POLE TYPE | UA(ft) | UC(In) | UD(In) | UE(In) | UG(ft) | UPRIGHT BASE CONNECTION |  |  |  |  |  |  | Connection plate data |  |  |  |  |  |  |  |  | DRILLED SHAFT DATA |  |  |  |  |
|  |  |  |  |  |  | No. Bolts | $\begin{aligned} & B A \\ & (I n) \end{aligned}$ | $\begin{aligned} & B B \\ & (I n) \end{aligned}$ | $\begin{aligned} & B C \\ & (I n) \\ & \hline \end{aligned}$ | $\begin{aligned} & B D \\ & (I n) \end{aligned}$ | $\begin{aligned} & B E \\ & (I n) \end{aligned}$ | $\begin{aligned} & B F \\ & (I n) \end{aligned}$ | $\begin{aligned} & H T \\ & (I n) \end{aligned}$ | $\begin{array}{\|c\|} \hline F J / S J \\ (I n) \end{array}$ | $\begin{array}{c\|} \hline F L / S L \\ (I n) \end{array}$ | $\begin{gathered} F N / S N \\ (I n) \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { FO/SO } \\ (I n) \end{array}$ | $\begin{array}{c\|} \hline F P / S P \\ (I n) \end{array}$ | $\begin{gathered} F R / S R \\ (I n) \end{gathered}$ | $\begin{array}{\|c\|} \hline F S / S S \\ (I n) \end{array}$ | $\begin{array}{\|c\|} \hline F T / S T \\ (I n) \\ \hline \end{array}$ | $\begin{aligned} & \text { DA } \\ & (f f) \end{aligned}$ | $\begin{gathered} \overbrace{}^{*} D A(D 66) \\ (f f) \end{gathered}$ | $\begin{aligned} & \hline 0 B \\ & (f f) \end{aligned}$ | RA | RB |
| R/ | 24 | 9.64 | 13 | 0.313 | - | 6 | 25 | 1.5 | 1.5 | 0.313 | 0.25 | 36 | 20 | 20 | 0.5 | 0.313 | 13 | 0.75 | 1.75 | 8.5 | 0.313 | 12 | 10 | 3.5 | 9 | 14 |
| R2 | 24 | 11.64 | 15 | 0.313 | - | 6 | 27 | 1.5 | 1.5 | 0.313 | 0.25 | 36 | 20 | 20 | 0.5 | 0.313 | 13 | 0.75 | 1.75 | 8.5 | 0.313 | 15 | 12 | 3.5 | 9 | 14 |
| R3 | 24 | 14.64 | 18 | 0.313 | - | 6 | 32 | 1.5 | 1.75 | 0.313 | 0.25 | 36 | 29 | 29 | 0.5 | 0.313 | 17.5 | 1 | 1.75 | 12.5 | 0.313 | 15 | 12 | 4 | 9 | 19 |
| R4 | 24 | 17.64 | 21 | 0.313 | - | 6 | 35 | 1.5 | 1.75 | 0.313 | 0.25 | 36 | 29 | 29 | 0.5 | 0.313 | 17.5 | 1 | 1.75 | 12.5 | 0.313 | 20 | 16 | 4 | 9 | 19 |
| R5 | 24 | 18.64 | 22 | 0.313 | - | 6 | 36 | 1.5 | 1.75 | 0.313 | 0.25 | 36 | 29 | 29 | 0.5 | 0.313 | 17.5 | 1 | 1.75 | 12.5 | 0.313 | 21 | 17 | 4 | 9 | 19 |
| R6 | 24 | 17.64 | 21 | 0.313 | - | 6 | 35 | 1.5 | 1.75 | 0.313 | 0.25 | 36 | 30 | 30 | 0.5 | 0.375 | 14 | 1.25 | 1.75 | 12.5 | 0.375 | 18 | 15 | 4 | 9 | 19 |
| R21 Lum | 39 | 7.54 | 13 | 0.313 | 37.5 | 6 | 25 | 1.75 | 1.5 | 0.313 | 0.25 | 36 | 20 | 20 | 0.5 | 0.313 | 10 | 0.75 | 1.75 | 8.5 | 0.313 | 11 | 11 | 3.5 | 9 | 14 |
| R22 Lum | 39 | 9.54 | 15 | 0.313 | 37.5 | 6 | 27 | 1.75 | 1.5 | 0.313 | 0.25 | 36 | 20 | 20 | 0.5 | 0.313 | 11 | 0.75 | 1.75 | 8.5 | 0.313 | 14 | 12 | 3.5 | 9 | 14 |
| R23 Lum | 39 | 12.54 | 18 | 0.313 | 37.5 | 6 | 32 | 1.75 | 1.75 | 0.313 | 0.25 | 36 | 29 | 29 | 0.5 | 0.313 | 12.5 | 1 | 1.75 | 12.5 | 0.313 | 15 | 12 | 4 | 9 | 19 |
| R24 Lum | 39 | 15.54 | 21 | 0.313 | 37.5 | 6 | 35 | 1.75 | 1.75 | 0.313 | 0.25 | 36 | 29 | 29 | 0.5 | 0.313 | 14 | 1 | 1.75 | 12.5 | 0.313 | 17 | 14 | 4 | 9 | 19 |

## UMINAIRE AND LUMINAIRE CONNECTION

| $L(A(f)$ | $L B(f)$ | $L C(I n)$ | $L D(i n)$ | $L E$ | $L(f f)$ | $L G(I n)$ | $L H(1 n)$ | $L U(I n)$ | $L K(I n)$ | $L(d e g)$ | $U G(f f)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| 40.0 | 10.0 | 3.0 | 0.125 | 0.50 | 8.0 | 0.5 | 0.75 | 0.25 | 0.188 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## MOTES

. Work thls index with Index No. 17745 .
2. Standard Mast Arm "C" Assemblies are designed to Loading Trees as indicated in Index No. 17741 for elther;


Design Wind Speed $=90$ mph with SIgnal Backplates or Design Wind Speed $=110 \mathrm{mph}$ without SIgnal Backplates.

