#### <u>Test Report for NMB Splice System</u> - For Sound Barrier Wall Foundation Connection -

By: Will Potter 6/15/07

### **Overview:**

The testing of the NMB Splice System was brought forth by the Florida Department of Transportation to investigate the sensitivity of the grout material installation. The intent is not to test the NMB Splice System, only the grouting process.

#### **Specimen Construction:**

Six 9U-X NMB Splice Sleeves were constructed, grouted, and then subjected to a tensile test. The specimens were assembled and grouted in accordance to the proposed testing scheme (see attachment). The grout was mixed as per specifications with 1 gallon of water to 1 bag of SS Mortar. The reinforcing bar was a number 9, Grade 60. The assembling and casting setup is shown in figure 1. The specimens are labeled numerically 1 to 6. Specimens 1 to 3 represent the poor grout scenario, in that they were not rodded. Specimens 4 to 6 correspond to the proper grouting technique, with specimen 6 being agitated further by moving the reinforcing bar.



Figure 1: NMB Splice Sleeve setup

### **Tensile Testing:**

A tension test was performed on the six specimens 12 days after casting at the State Materials Office in Gainesville, FL. The test was conducted based on ASTM A615. The setup is shown in figure 2. The objective of testing was to acquire the load at which failure occurs and compare the results between the two installation procedures. The results from the failure test are given in table 1 with further details given in the attachment.



Figure 2: Test Setup

Table 1:	Test Results
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Table I. Test Results			
Specimen	Ultimate Load (kips)	Type of Failure	Location (depth)
1	106.42	Splice Device	1/2
2	111.17	Bar	
3	107.02	Splice Device	1/2
4	107.54	Splice Device	1/4 from top
5	107.72	Splice Device	1/2
6	106.99	Splice Device	1/2

### Analysis of Results:

The results in table 1 depict consistency based on the small variance in ultimate load. With the type of failures that occurred, a comparison of the grout installation cannot be established, due to the fact that the grout was not the controlling factor. It is shown that five of the specimens failed within the splice sleeve with one specimen failing within the reinforcing bar. It is also observed that specimen 4 failed in the upper region of the device (bar insertion end) as opposed to mid-depth as the other four. A plausible explanation for the devices failing rather than the reinforcing bar is that the clear distance between the top of the device and the grips of the testing machine was small, approximately 4 to 5 inches. This short distance prevented the reinforcing bar from failing, except in specimen 2. It is believed that if this clear distance was increased the bar would have a better opportunity to fail. The reason for the failure in specimen 4 is not yet determined. The failed specimens can be seen in figure 3.

The manufacturers of the device specify 160 percent (96 kips for a #9 bar –Grade 60) of bar yield and the results from testing show well above that value with the minimum being 177 percent. The splice system's performance is more than adequate.



Figure 3: Failed Test Specimens

A compression test was completed at the same time of the tension test on grout cubes that were cast concurrently with the splice devices. The results of this test are given in table 2. The grout cubes were cast in accordance to ASTM C 942. The samples remained in the covered grout molds until the day of testing without any additional moisture.

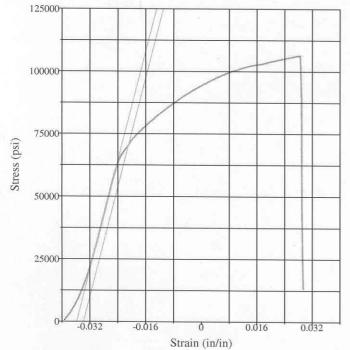
	inpressive rest results
Specimen #	12-day Compressive Strength (psi)
1	16,373
2	16,730
3	16,690

Table 2:	Compressive	Test Results
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### **Conclusion:**

The test results clearly indicate that the grouting procedures for the NMB Splice Sleeves have a low sensitivity. It is apparent that with the grout being fluid it is not that critical for the specimens to be rodded. As long as there is a sufficient amount of grout used and the placement of the reinforcing bars is adequate there will not be an issue with the splice system.

An issue that may need to be investigated is the placement of the reinforcing bar. How will the device perform if the bar is oriented to one side of the system? With the current setup, the bar is located as close to center as possible. The setup in the field may not guarantee this situation.

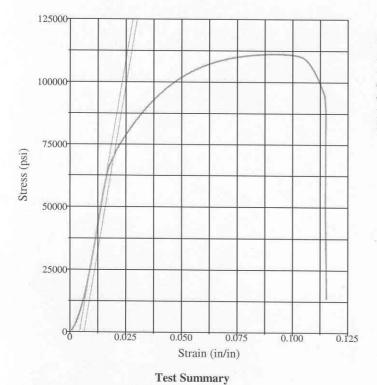


	Test Results
Specimen Gage Length:	24.7500 in
Área:	1.0000 in <sup>2</sup>
Yield Load:	106420 lbf
Yield Strength:	106420 psi
Fotal Load:	106420 lbf
Fensile Strength:	106420 psi
Load at Offset:	70280 İbf
Stress at Offset:	70280 psi
Young's Modulus:	5470000 psi

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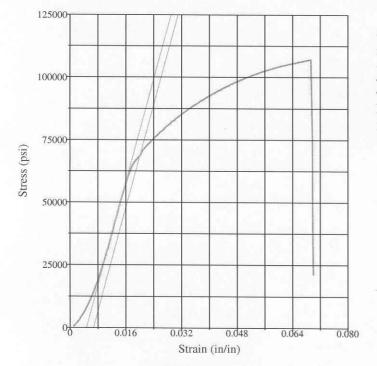
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	Test Summary
Counter:	2765
Elapsed Time:	00:01:48
LIMS Number:	Test Sample
Project Number:	*
Sample Number:	*
Size:	9
Grade:	60
Elongation:	0
Cold Bend:	OK @ 180
Condition of Sampl	e: Satisfactory
Operator:	MC
Comments:	Test Sample #1
Heat Number:	*
Procedure Name:	ASTM A615 - Grade 60 - 3 zones - no extens
Start Date:	6/12/2007
Start Time:	9:32:32 AM
End Date:	6/12/2007
End Time:	9:34:20 AM
Workstation:	FLORIDA-DOT
Tested By:	tech



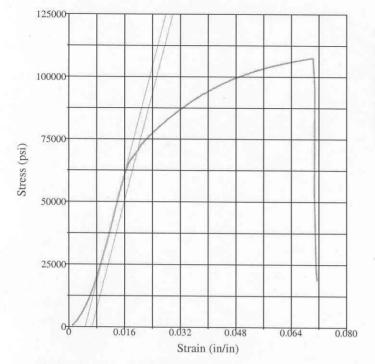
	Test Results
Specimen Gage Length:	24.7500 in
Area:	1.0000 in <sup>2</sup>
Yield Load:	111170 lbf
Yield Strength:	111170 psi
Total Load:	111170 Îbf
Tensile Strength:	111170 psi
Load at Offset:	<b>69910</b> Îbf
Stress at Offset:	69910 psi
Young's Modulus:	5270000 psi

	rest Summary
Counter:	2766
Elapsed Time:	00:02:09
LIMS Number:	Test Sample #2
Project Number:	*
Sample Number:	*
Size:	9
Grade:	60
Elongation:	0
Cold Bend:	*
Condition of Sample	e: Satisfactory
Operator:	MC
Comments:	Test Sample #2
Heat Number:	
Procedure Name:	ASTM A615 - Grade 60 - 3 zones - no extens
Start Date:	6/12/2007
Start Time:	9:41:18 AM
End Date:	6/12/2007
End Time:	9:43:27 AM
Workstation:	FLORIDA-DOT
Tested By:	tech
,	



	Test Results
Specimen Gage Length:	24.7500 in
Area:	1.0000 in <sup>2</sup>
Yield Load:	107020 lbf
Yield Strength:	107020 psi
Total Load:	107020 lbf
Tensile Strength:	107020 psi
Load at Offset:	<b>68790</b> Îbf
Stress at Offset:	68790 psi
Young's Modulus:	5150000 psi

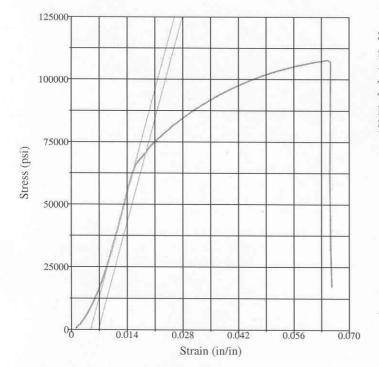
	Test Summary
Counter:	2767
Elapsed Time:	00:01:49
LIMS Number:	Test Sample #3
Project Number:	*
Sample Number:	*
Size:	9
Grade:	60
Elongation:	0
Cold Bend:	*
Condition of Sampl	e: Satisfactory
Operator:	MC
Comments:	Test Sample #3
Heat Number:	
Procedure Name:	ASTM A615 - Grade 60 - 3 zones - no extens
Start Date:	6/12/2007
Start Time:	9:49:07 AM
End Date:	6/12/2007
End Time:	9:50:56 AM
Workstation:	FLORIDA-DOT
Tested By:	tech



	Test Results
Specimen Gage Length:	24.7500 in
Area:	1.0000 in <sup>2</sup>
Yield Load:	107540 lbf
Yield Strength:	107540 psi
Total Load:	107540 lbf
Tensile Strength:	107540 psi
Load at Offset:	<b>70110</b> Îbf
Stress at Offset:	70110 psi
Young's Modulus:	5390000 psi

**Test Summary** 

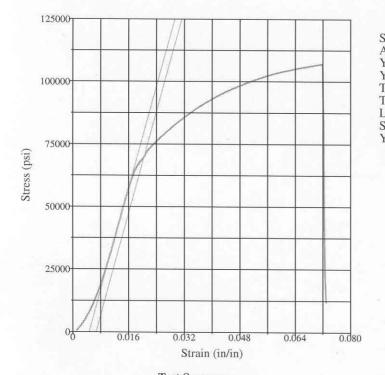
Counter:	2768
Elapsed Time:	00:01:50
LIMS Number:	Test Sample #4
Project Number:	*
Sample Number:	*
Size:	9
Grade:	60
Elongation:	0
Cold Bend:	*
Condition of Sample:	Satisfactory
Operator:	MC
Comments:	Test Sample #4
Heat Number:	<b>A</b>
Procedure Name:	ASTM A615 - Grade 60 - 3 zones - no extens
Start Date:	6/12/2007
Start Time:	9:55:29 AM
End Date:	6/12/2007
End Time:	9:57:19 AM
Workstation:	FLORIDA-DOT
Tested By:	tech



	<b>Test Results</b>
Specimen Gage Length:	24.7500 in
Area:	1.0000 in <sup>2</sup>
Yield Load:	107720 lbf
Yield Strength:	107720 psi
Total Load:	107720 lbf
Tensile Strength:	107720 psi
Load at Offset:	70820 lbf
Stress at Offset:	70820 psi
Young's Modulus:	5920000 psi

**Test Summary** 

Counter:	2769
Elapsed Time:	00:01:43
LIMS Number:	Test Sample #5
Project Number:	*
Sample Number:	*
Size:	9
Grade:	60
Elongation:	0
Cold Bend:	*
Condition of Sample:	Satisfactory
Operator:	MC
Comments:	Test Sample #5
Heat Number:	
Procedure Name:	ASTM A615 - Grade 60 - 3 zones - no extens
Start Date:	6/12/2007
Start Time:	10:10:34 AM
End Date:	6/12/2007
End Time:	10:12:17 AM
Workstation:	FLORIDA-DOT
Tested By:	tech



	<b>Test Results</b>
Specimen Gage Length:	24.7500 in
Area:	1.0000 in <sup>2</sup>
Yield Load:	106990 lbf
Yield Strength:	106990 psi
Fotal Load:	106990 İbf
Fensile Strength:	106990 psi
Load at Offset:	69950 İbf
Stress at Offset:	69950 psi
Young's Modulus:	5090000 psi

	Test Summary
Counter:	2770
Elapsed Time:	00:01:53
LIMS Number:	Test Sample #6
Project Number:	*
Sample Number:	*
Size:	9
Grade:	60
Elongation:	0
Cold Bend:	*
Condition of Sample:	Satisfactory
Operator:	MC
Comments:	Test Sample #6
Heat Number:	
Procedure Name:	ASTM A615 - Grade 60 - 3 zones - no extens
Start Date:	6/12/2007
Start Time:	10:19:51 AM
End Date:	6/12/2007
End Time:	10:21:44 AM
Workstation:	FLORIDA-DOT
Tested By:	tech

Structural Materials Evaluation and Research Laboratory	ASTM C 109	COMPRESSIVE	fective Date: 2005
Raw Data Worksheet		By: T.DILLOW	Page 1 of 1

DATE: 06/12/	ד' כ	Tested by:	BDU
LIMS #	Matl: SS Mortow	LIMS #	Matl:
DAV DDEAK	16373 psi		psi
DAY BREAK	16730 psi	] DAY B	BREAK psi
	16690 psi		psi
AVG.	psi	AVG.	psi

LIMS #	Matl:	LIMS #	Matl:
DAVBBEAU	psi		psi
DAY BREAK	psi	DAY BREAK	psi
	psi	the second second	psi
AVG.	psi	AVG.	psi

LIMS #	Matl:	LIMS #	Matl:
DAV DDEAK	psi	DAY BREAK	psi
DAY BREAK	psi		psi
	psi		psi
AVG.	psi	AVG.	psi

LIMS #	Matl:	LIMS #	Mafl:
DAVERDAY	psi		psi
DAY BREAK	psi	DAY BREAK	psi
	psi		psi
AVG.	psi	AVG.	psi

LIMS #	Matl:	LIMS #	Matl:
DAV DDEAK	psi		psi
DAY BREAK ps	DAY BREAK	psi	
	psi		psi
AVG.	psi	AVG.	psi

IMS #	Matl:	LIMS #	Mat'l:
DAV DDEAK	psi	DAY BREAK	psi
DAY BREAK	psi		psi
	psi	Second and the second second	psi
AVG.	psi	AVG.	psi

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## **Purpose:**

The purpose of this test is to determine the sensitive of the grout placement for the splice system using the PRE-grout installation method. A lack of confidence with the consistent diligent placement and rodding of the grout material warrants the Department to investigate the effects of a poorly installed grout material which may compromise the strength of the completed soundwall post system proposed by Mack Industries. This testing will not discredit the validity of any previous product approval testing, but only to identify the sensitivity to poor installation practice.

## Scope:

A total of six 9U-X NMB splice samples are to be constructed, cured and then subject to tensile testing. Two separate installation procedures will be investigated. Both installation methods will use the PRE-grout installation method but without the splice sleeves cast into concrete. A 18" long #9 bar shall be inserted into the narrow end of the splice, secured with the rubber seal and supported in the vertical position with the wide end opening at the top. The grout shall be mixed to the manufacturers proportions (1 gallon water/1 bag of grout) and simply poured from a bucket into the splice from the top filling the splice completely.

# Installation 1 – No rodding:

The first three samples (1a, 1b, 1c) shall not be rodded or vibrated to consolidate the grout material. The top 18" long #9 bar shall be inserted directly into the splice and supported until initial set of the grout material.

### Installation 2 – Limited Rodding:

The last three samples (2a, 2b, 2c) shall be rodded with a 1/8" diameter wire 10 times for a depth at least 3⁄4 of the splice sleeve, after completely filing the splice with grout. The top #9 bar shall then be inserted directly into the splice and supported until initial set of the grout material.

### Tensile Testing:

After curing for a minimum of 7 days all six samples shall be tested to determine the effective tensile strength of the spliced connection. The test results for each installation method shall be identified and reported separately.

#### GENERAL NOTES FOR PRE-GROUT (PRE) INSTALLATION

<u>PRE-Grout Installations</u>: This procedure is used when the sleeves are oriented below the joint without PVC tubing to pump SS Mortar® inside. It may be useful in situations requiring a "blind" architectural connection with no exposed tubes that require patching.

FIG.-40-1



