DATA TABLES AND SOUND BARRIER GRAPHIC CELLS FOR FDOT DESIGN STANDARDS

Many of the structures related Design Standards require "Data Tables" that must be completed by the designer, which provide critical information for the contractor when these Design Standards are referenced in the contract plans. See the "FDDT Structures Bar Menu" included with the FDDT CADD Software for the Microstation CADD Cell Data Tables. Updates to the Data Tables for Interim Design Standards are available on the Structures Design Dffice website at:

http://www.dot.state.fl.us/structures/CADD/standards/CurrentStandards/MicrostationDrawings.shtm

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lards

BOX CULVERT DATA TABLES

				ВОХ, Н	EADWAL	L AND	CUTOFF	WALL	DATA TA	ABLE (in	ches un	oless sh	own oth	erwise)				Та	ible Date 🕽	7-01-09
LOCATION	STRUCTURE /BRIDGE					BOX								HEADWA	LL AND	CUTOF	F WALL			
LUCATION		Wc(ft)	Hc(ft)	Τt	Tw	Тb	Ti	#cells	Lc(ft)	Cover	Blhw	Hlhw	Brhw	Hrhw	Blcw	HIcw	Brcw	Hrcw	SL(deg)	SR(deg)

				LEF	T SIDE	WINGWA	LLS DA	TA TAB	LE (inch	es unle:	ss show	n other	wise)			Та	ble Date 🕽	7-01-09
STRUCTURE /BRIDGE				LEF	T END W	VINGWAL	LL						LEFT E	BEGIN E	NDWALL			
NUMBER	Rt	Rw	Rh	Rd	SW(deg)	β(deg)	He(ft)	Hs(ft)	Lw(ft)	Rt	Rw	Rh	Rd	SW(deg.	β(deg)	He(ft)	Hs(ft)	Lw(ft)

				RIGH	T SIDE	WINGW	ALLS D	ATA TAE	BLE (inc	hes unle	ess show	vn other	wise)			Ta	ble Date ;	7-01-09
STRUCTURE				RIG	HT END	WINGW	ALL						RIGHT	BEGIN E	NDWALL			
/BRIDGE NUMBER	Rt	Rw	Rh	Rd	SW(deg,	β(deg)	He(ft)	Hs(ft)	Lw(ft)	Rt	Rw	Rh	Rd	SW(deg,	β(deg)	He(ft)	Hs(ft)	Lw(ft)

							Ε	STIMATE	ED CON	CRETE (QUANTIT	TES (C)	0						Ta	ble Date	7-01-09
STRUCTURE	1.54	Diaht			אס	1	Diaht			EFT EN /INGWAL			FT BEG 'INGWAL			GHT EI INGWAL			GHT BE		Culvert
/BRIDGE NUMBER	Left Cutoff Wall	Cutoff Wall	Bottom Slab	Walls	Top Slab	Left Head Wall	Right Head Wall	Sub Total	Footing	Wall	Sub Total	Footing	Wall	Sub Total	Footing	Wall	Sub Total	Footing	Wall	Sub Total	Total

						MAIN	STEEL	REINFO	RCEMEN	IT SPAC	CING (in	ches)					Tc	ble Date .	7-01-09
STRUCTURE				BL	אכ											HEAD	WALLS	CUTOFF	WALLS
/BRIDGE NUMBER	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115, 116	803	806	809	812

										WIN	IGWALL	STEEL	REINFOR	CEMEN	T SPACI	NG (inc	hes)									Tai	ble Date 7	7-01-09
STRUCTURE			LEFT E	END WIN	IGWALL					LEFT BL	EGIN WI	INGWALL	-				RIGHT	END WI	NGWALL				F	RIGHT B	EGIN W	INGWAL	L	
/BRIDGE NUMBER	401 407(8)	402 (403)	404 (405)	406	409	410	411	501 507(8)	502 (503)	504 (505)	506	509	510	511	601 607(8)	602 (603)	604 (605)	606	609	610	611	701 707(8)	702 (703)	704 (705)	706	709	710	711
																												ĺ
																												1

WINGWALL NDTE: Bar designations in "()" are only required for variable height wingwalls.

INSTRUCTIONS TO DESIGNER

- Design Standards Index No. 289.
- the program root directory.

NOTES:

1. Work these data tables with the FDDT Mathcad LRFD Culvert Program and 2. Fill in tables using key-in "include" and line1.prn thru line6.prn files located in 3. Use StructuresSiteMenu>Text>Table Data, which uses "Chart" TextStyle and font 169 Structures proportional. 4. Complete Notes 1 thru 7. Delete Note 7 when not applicable. 5. For box culverts meeting the definition of a bridge structure (See Plans Preparation Manual, Volume 1, Chapter 33) include the Bridge Number in the plans and the Load Rating Sheet per the Structures Design Guidelines 3.15.14. PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING.

> 1. Environmental Class -----Reinforcing Steel, Grade ----f'c = ---- ksi Concrete Class -----Soil Properties: Friction Angle -----Modulus of Subgrade Reaction -----Nominal Bearing Resistance -----Total Estimated Quantity of Reinforcing Steel ----- Ibs

Work this Drawing with Design Standards Index No. 289 and Sheet Nos. -----

7. Settlement criteria for Precast Box Culvert option (Index No. 291): Long Term Differential Settlement $(\Delta Y) = ----- ft$. Effective Length for Settlement (L) = ----- ft.

RETAINING WALLS DATA TABLE

									И	ALL DIM	MENSION	IS													
Wall	Be	gin	E	nd	Be	Hei egin	ight E	nd	W	all ngth	D	W	L	pot	L_t	oe	Slope	D sc	oil	L	D key	V step	Wall Cover		FtgCov (bot.)
No.	Station	Dffset	Station	Dffset	ft.	in.	ft.	in.	ft.	in.	in.	in.	ft.	in.	ft.	in.	Bkwall	ft.	in.	in.	in.	in.	in.	in.	in.
																								ļ'	
																								ļ'	
																								<u> </u> '	
																								<u> </u> '	L
																								 '	L

												BIL	L OF RE	EINFORC	SING ST	EEL													
					Bars J	1										Bars K									Bar	s M			
Size	No.	Spacing	Be	, gin	A E	nd	-	В			Size	No.	Spacing	Be	, gin	А Е	nd	-	В			Size	No.	, A	4		В	TotalL	Length
		in.	ft.	in.	ft.	in.	ft.	in.	ft.	in.			in.	ft.	in.	ft.	in.	ft.	in.	ft.	in.			ft.	in.	ft.	in.	ft.	in.
	Size	Size No.		Size No. <u>' Be</u>	Size No. ' Begin	Size No. Spacing A Begin E	Size No. Begin End	Size No. Spacing A Begin End	Size No. Spacing A B	Size No. Spacing A B Aven Begin End B Total	Size No. Spacing A Average Total Length	Size No. Spacing A B Average Total Length Size	Bars JSizeNo.SpacingAAAverage Total LengthSizeNo.	Bars JSizeNo.SpacingAAverage EndAverage TotalLengthSizeNo.Spacing	Bars J Size No. Spacing A B Average Total Length Size No. Spacing	Bars J Bars J Size No. Spacing A Bars J Average Total Length Size No. Spacing	Size No. Spacing A B Average A Spacing Begin End B Total Length Size No. Spacing Begin End	Bars J Bars K Size No. Spacing A Average Average Begin End B Total Length Size No. Spacing Begin End	Bars J Bars K Size No. Spacing A Average Average Begin End B Total Length Size No. Spacing A	Bars J Bars K Size No. Spacing A B Average Total Length Size No. Spacing A B	Bars J Bars K Size No. Spacing A B Average Total Length Size No. Spacing A B Average Total Length A	Bars J Bars K Size No. Spacing A Average Begin End B Average TotalLength Size No.	Bars J Bars K Size No. Spacing Average Average Begin End B Average No.	Bars J Bars K Size No. Spacing Average Total Length Average Size No. Spacing Average Begin Average Total Length Size No.	Bars J Bars K Size No. Spacing Average Begin Average Fotal Length Average Size Average No. Average Begin Average End Average Size No.	Bars J Bars K Bars K Size No. Spacing Average Begin Average Fotal Length Average Size No.	Bars J Bars K Bars M Size No. Spacing Average Total Length Average Size No. Spacing Average Begin Average End Average Total Length No. Spacing	Bars J Bars K Bars M Size No. Average Average Average Average Size No. End End Size No. Size No. Average No. Average	Bars J Bars K Bars M Size No. Spacing Average Total Length Average Size No. Spacing Average Begin Average Total Length Average Size No. Pacing Begin End Begin Average Total Length No. And Begin Average Total Length No. No

												BIL	L OF RE	INFORC	CING ST	EEL												
			Bars H					Bars G.	1				Bar	s R				Bars Z						Bar	s A			
Wall			Seguina	1.00	nath			Seguine	No. of	Total	Length			1.00	ngth			Seguina	Lor	ngth				Ler	ngth		Aver	rage
No.			igin	Size	No.	Spacing	Lap	Totan	Length	Size	No.	Lei	igin	Size	No.	Spacing	Ler	igin	Size	No.	Be	rgin	Er	nd	Len	ngth		
			in.	ft.	in.			in.	Splices	ft.	in.			ft.	in.			in.	ft.	in.			ft.	in.	ft.	in.	ft.	in.
																												í –
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											BILL D	F REINF	ORCING	STEEL										
					Bars F	-					Bars	s G2			Bar	rs D			Bar	s N			Bars	s G
Wall			Spacing		Lei	ngth		Ave	rage				ngth				ngth			Total	Length			
No.	Size	No.	Spacing	Be	egin	E	nd	Ler	ngṫh	Size	No.	Ler	igin	Size	No.	Lei	igtri	Size	No.	Total	Length	Size	No.	
			in.	ft.	in.	ft.	in.	ft.	in.			ft.	in.			ft.	in.			ft.	in.			f

	EST	TIMATED QUA	WTITIES	
		Concrete		Reinf.
Wall No.	Footing	Wall	TOTAL	Steel
	C. Y.	С. Ү.	C. Y.	LBS.

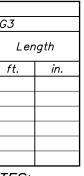
QUANTITIES NOTES:

- $\langle i \rangle$ Includes concrete for optional shear key.
- Includes additional concrete at top of wall for support of optional traffic railing barrier but does not include concrete for barrier itself (see Index No. 5100 - Payment note).
- $\langle \hat{\mathcal{S}} \rangle$ Does not include Bars 5V or any other reinf. steel for optional traffic railing barrier (see Index No. 5100 – Payment note).

- 1. Concrete Class (f'c =
- 2. A value of '0' for Slope Backwall indicates front and back of wall are parallel.

)

- 3. Dsoil is typical depth of soil and is used for design purposes only. See Control Drawings for actual ground line.
- 4. Non-zero values for Lkey and Dkey indicate the existence of a shear key.
- 5. A non-zero value for Vstep indicates the existence of a footing step, see Control Drawings for location.
- 6. Bars J, K, A and F vary uniformly between begin and end wall heights as indicated by begin and end dimensions.
- 7. The number of G1 Bars includes 2 additional bars when a shear key is specified.
- 8. For walls with variable begin/end height, Bars G2 shall be fanned such that they are evenly spaced throughout length of wall.
- 9. Non-zero values for Bars N and Bars G3 indicate the existence of a barrier on the wall.



NOTES:

SOUND BARRIERS DATA TABLES

	PRDJECT AESTHETIC REQUIREMENTS												
WALL NDS:	REQUIRED: (YES/ND)		REQUIRED TE	EXTURES (3):		FLUSH						
	GRAPHICS	COLORED	PRECAST	PANELS:		POSTS:	PANEL / RECESSED						
	(1)	CDATINGS (2)	POST CAP (5)	FRONT FACE	BACK FACE (4)	FRONT FACE	PANEL / EITHER						

(1) See Control Drawings.

(2) Coat all exposed faces of wall with (sacrificial/non-sacrificial) anti-graffiti coating or Class 5 Applied Finish Coating. The color shall be per Federal Color Chart, Federal Standard No. 595B, Table ____, Color ____.

(3) See Index 5201.

(4) Provide broom or Type "A" (smooth) finish when flush face panel option is utilized.

(5) See Index 5207. Coat post caps the same color as posts, with a Class 5 Applied Finish Coating.

	SUMMARY OF FOUNDATIONS	S AND WALL	QUANTITIES	Tab	e Date 07-01-10
WALL ND.	STATION TO STATION	FOUNDATION (6)	TOP OF WALL ELEV. (FT)	BOTTOM OF WALL ELEV. (FT)	AREA (SF)
				TOTAL:	

LIMITS D WALL STATION ND.

NOTES:

1. The Contractor may choose the Standard Precast 20'-0" Panel Dption depicted herein or one of the following QPL approved proprietary sound barrier panels used with FDDT standard posts and foundations:

1)
2)
3)

QPL approved proprietary sound barrier panels not listed above may be approved by the Engineer when all project aesthetic requirements can be met. Refer to the following web site address for the Qualified Products List for Sound Barrier Panels:

www.dot.state.fl.us/specificationsoffice/

2. The Contractor may also choose one of the following QPL approved proprietary sound barrier systems (panels and foundation): 1). _____

2). _____ 3). _____

QPL approved proprietary sound barrier systems not listed above may be approved by the Engineer when all project aesthetic requirements can be met. Refer to the following web site address for the Qualified Products List for Sound Barrier Systems:

www.dot.state.fl.us/specificationsoffice/

3. Sound barriers shall meet the project aesthetic requirements as depicted in the above table and elsewhere in the plans.

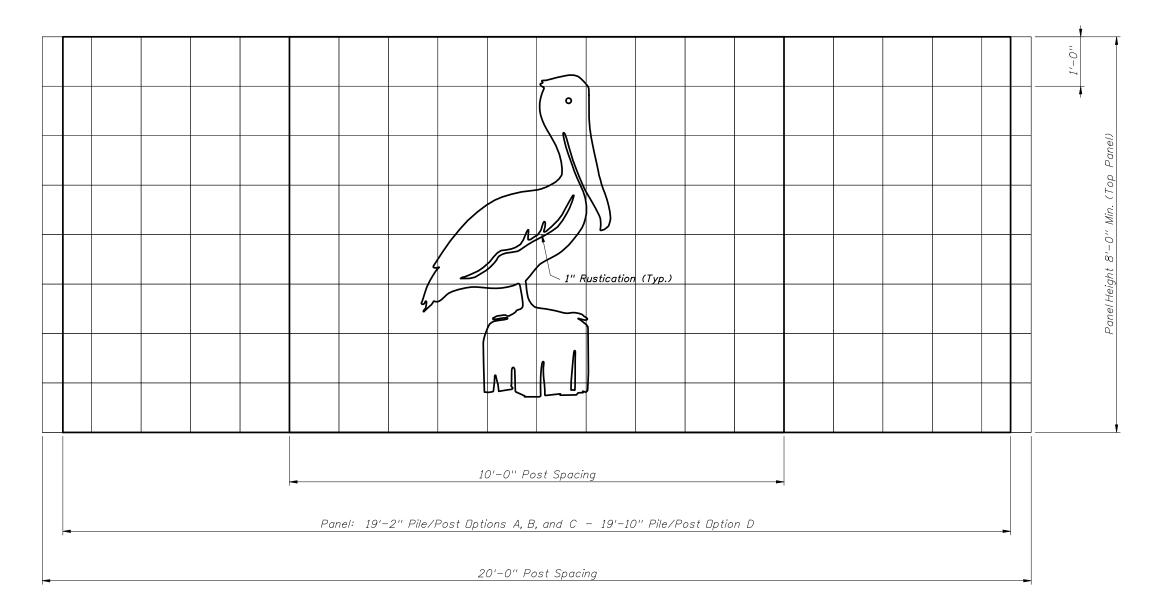
side of wall.

(6) See Index No. 5206 for "1" (Table 1 - Medium Dense Granular Soils) and "2" (Table 2 - Loose Granular Soils). See Plans for "SD" (Special Design) details.

DF ANTI-GRAFFIT.	I CDATING	Tab	ole Date 1-01-06
N TO STATION	FRONT FACE, BACK FACE, BOTH		AREA (SF)
		_	
		_	
		_	
		_	
		_	
		_	
		\rightarrow	
		_	
		_	
		-+	
		_	
		-	
	7074	_	
	TOTAL:		

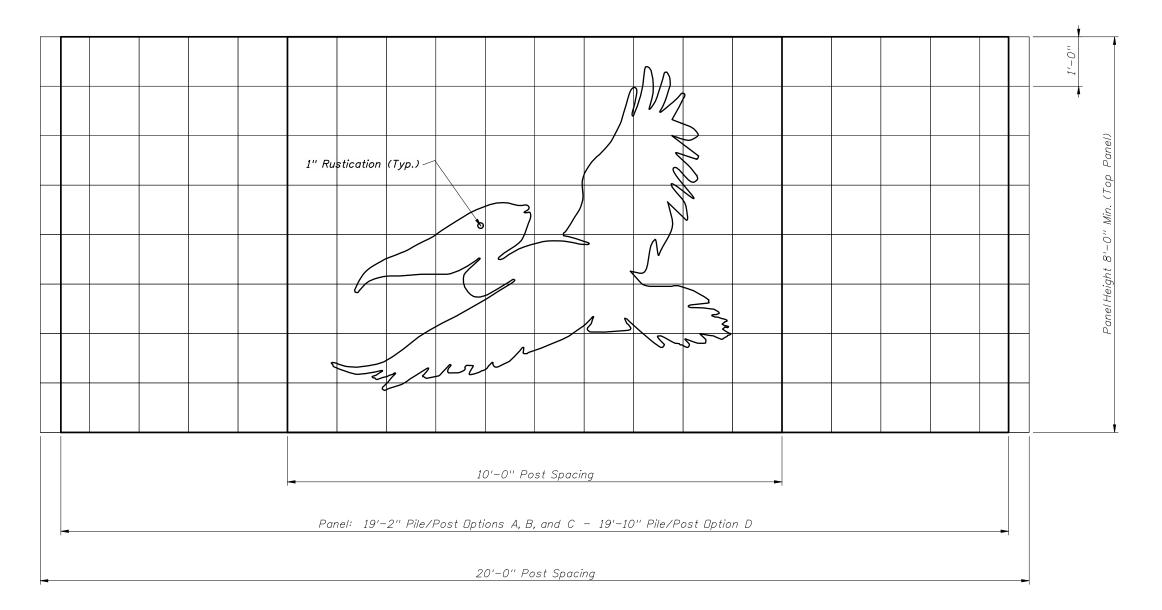
4. Front Face indicates roadway side of wall. Back Face indicates non-roadway

BROWN PELICAN (BP-1)



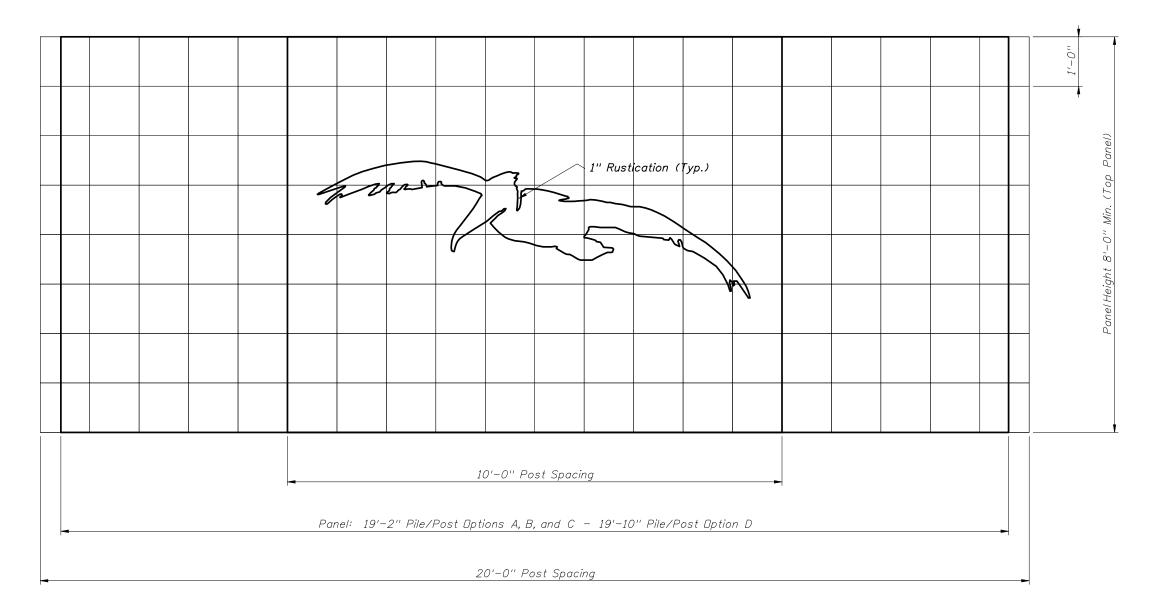


BROWN PELICAN (BP-3)



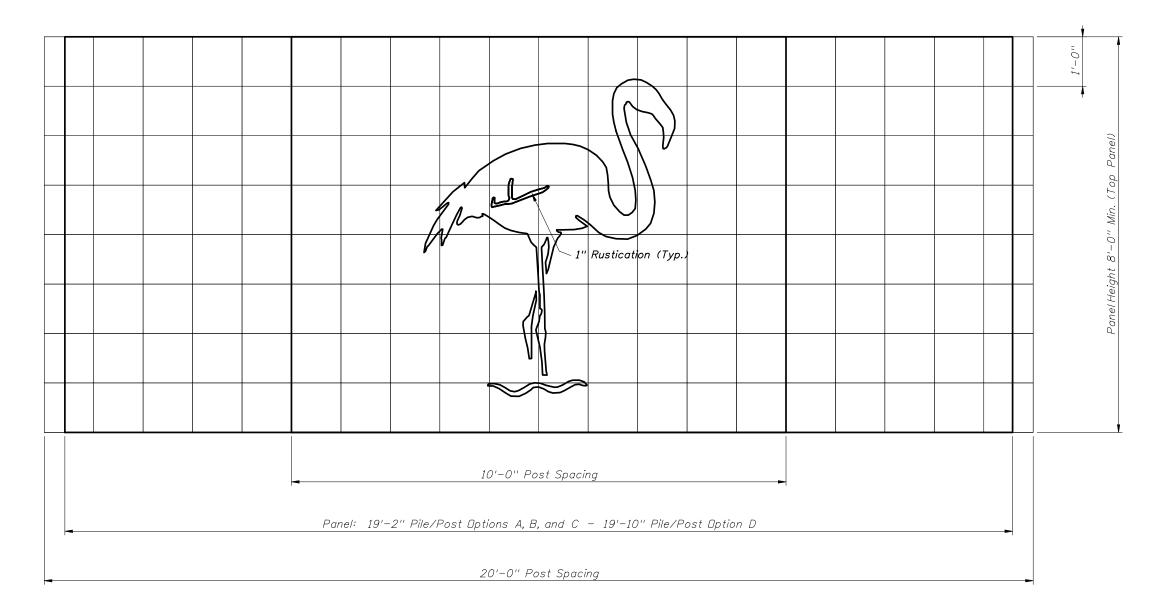


BROWN PELICAN (BP-2)

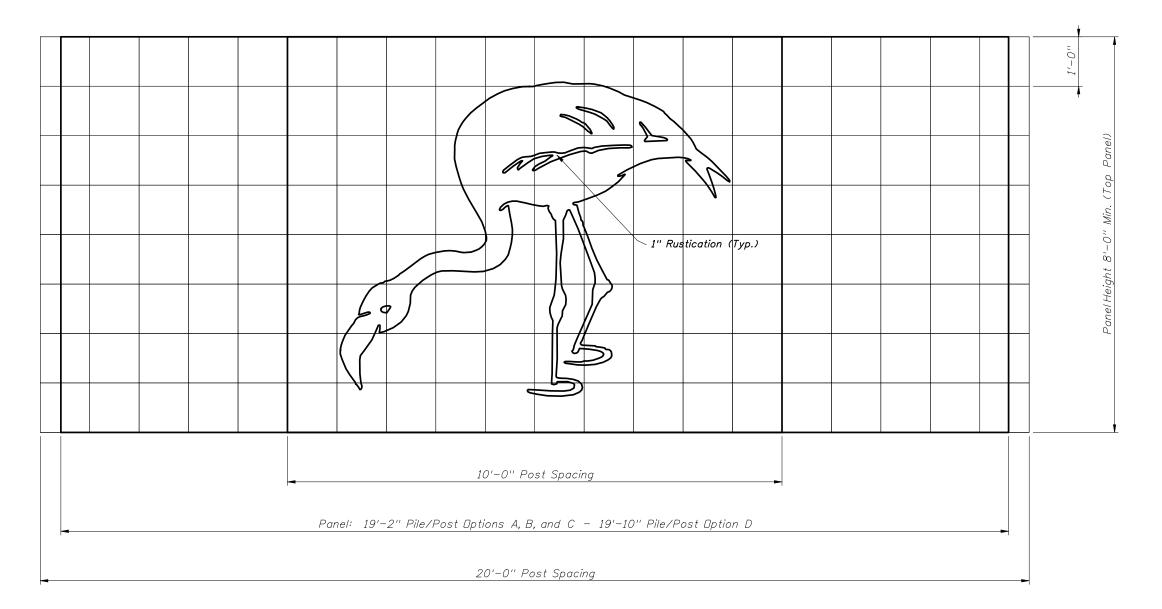




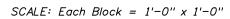
FLAMINGD (F-1)

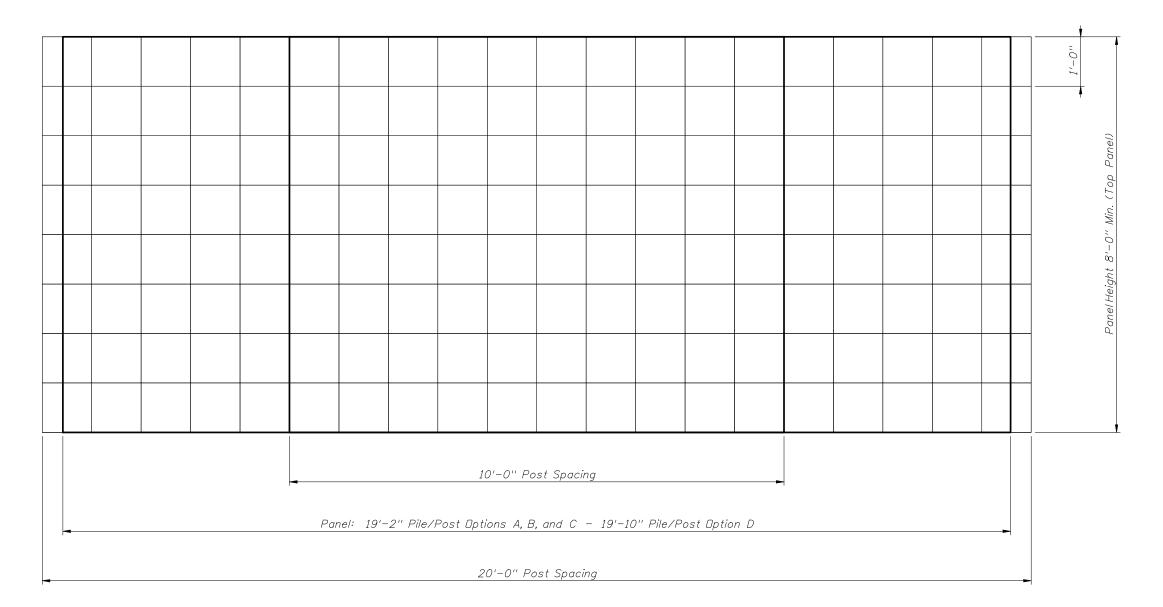






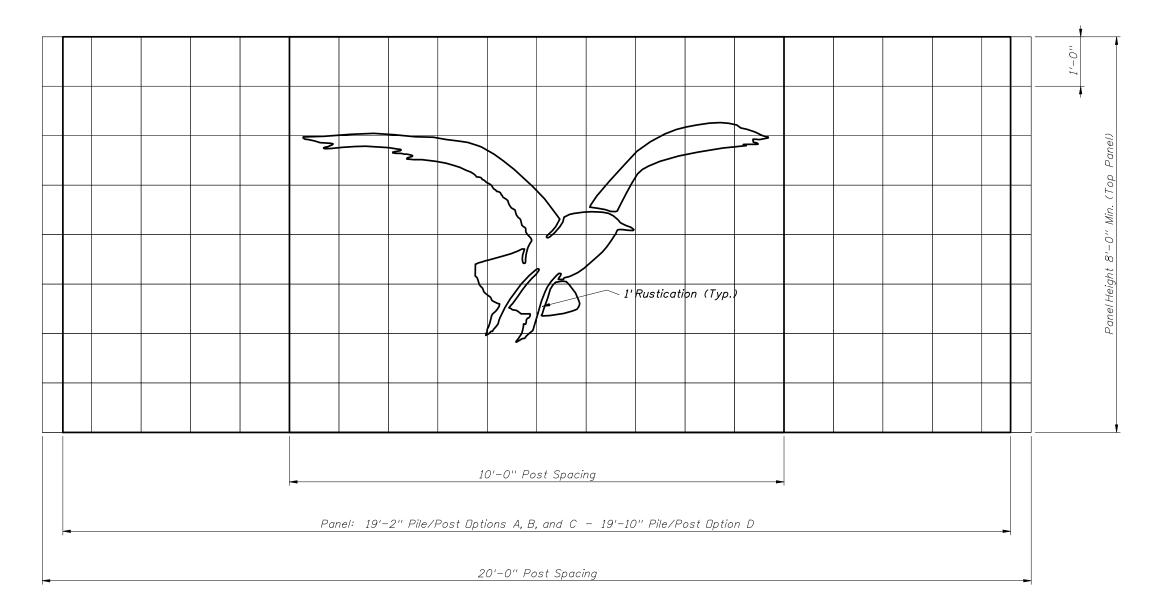
FLAMINGO (F-2)





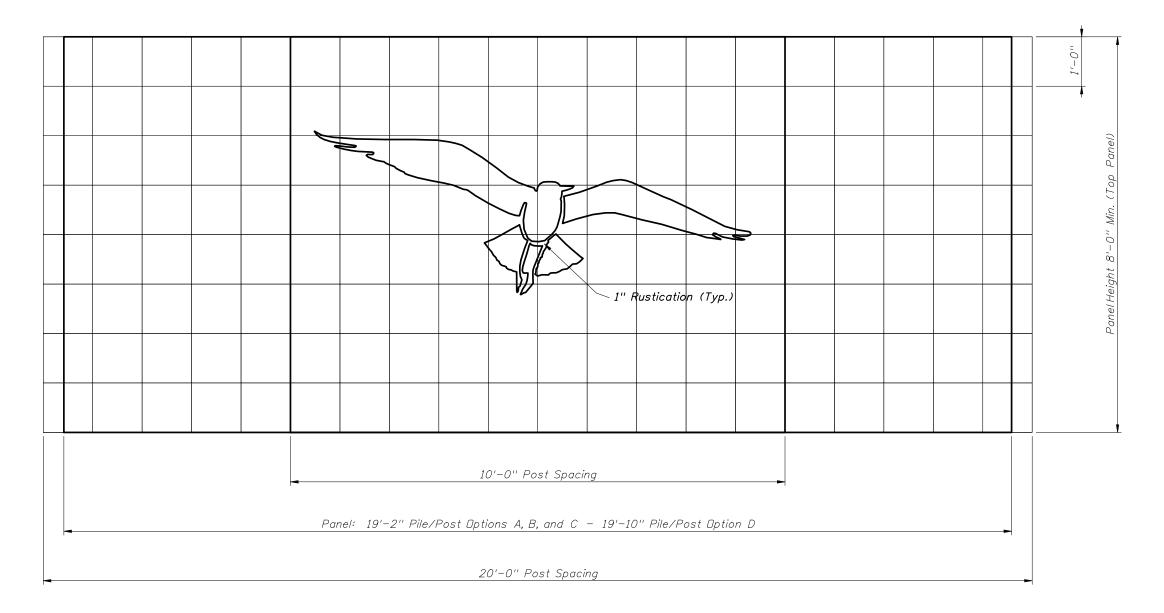


LAUGHING GULL (LG-1)



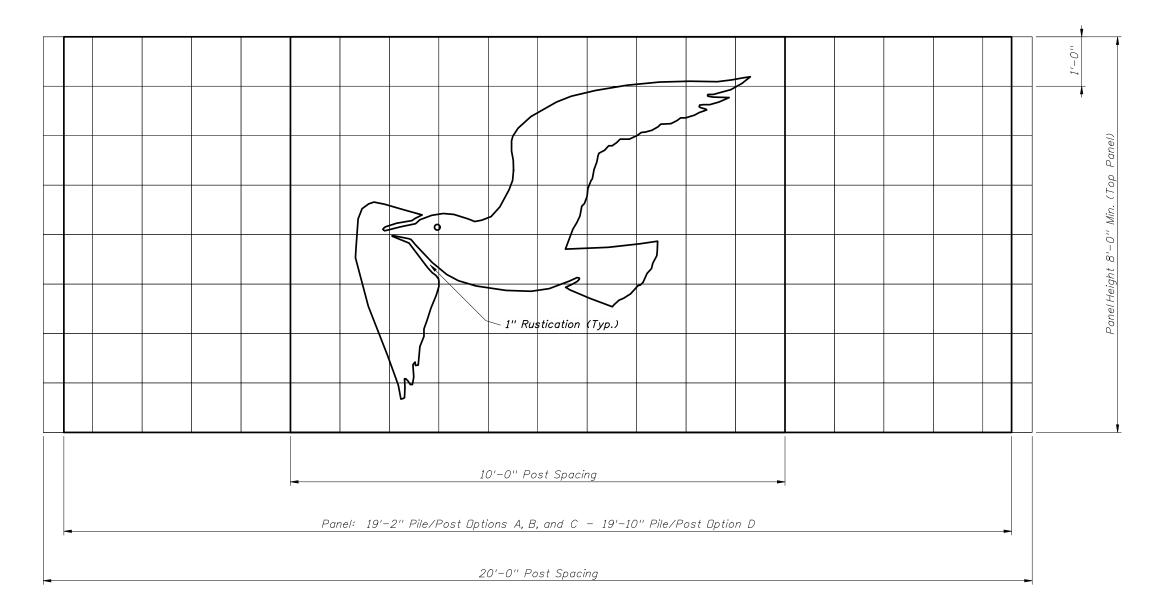


LAUGHING GULL (LG-2)



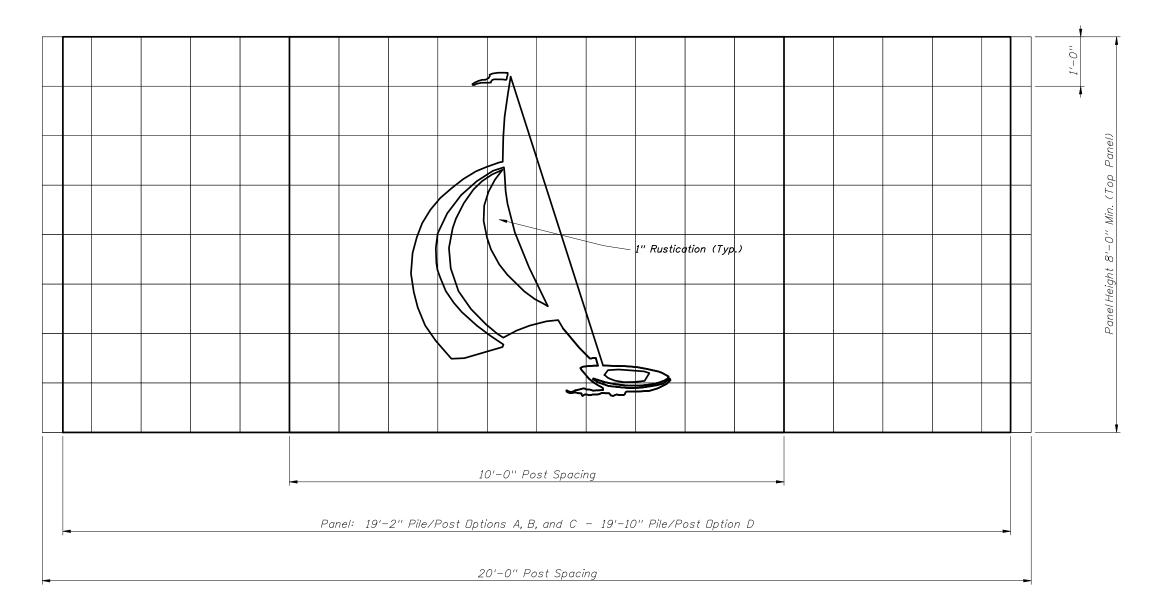


LAUGHING GULL (LG-3)



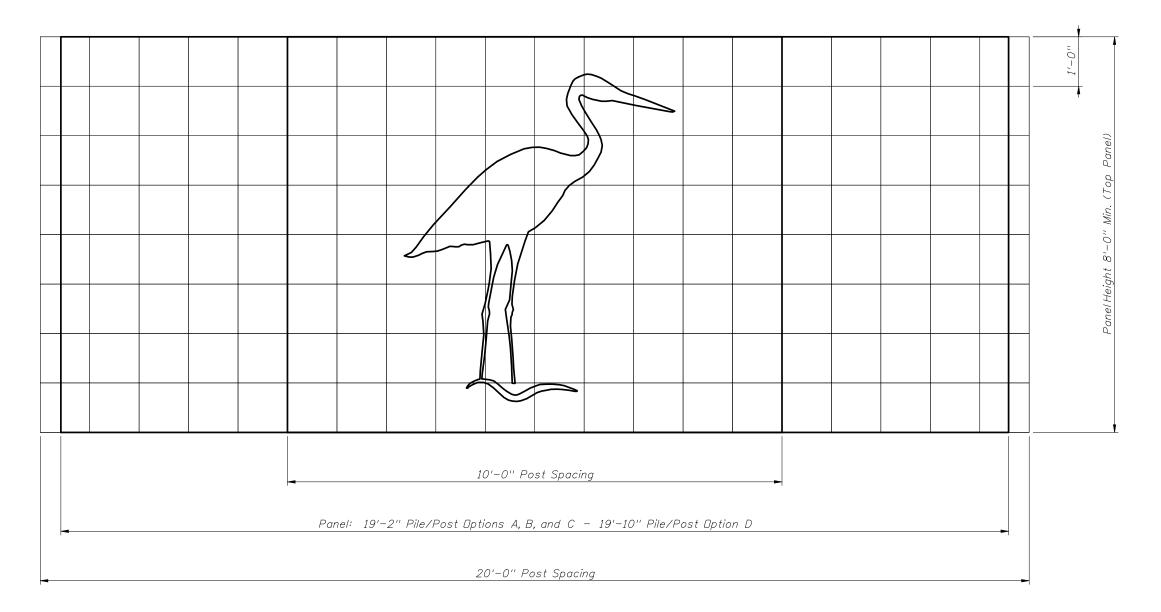


SAIL BOAT (SB-1)



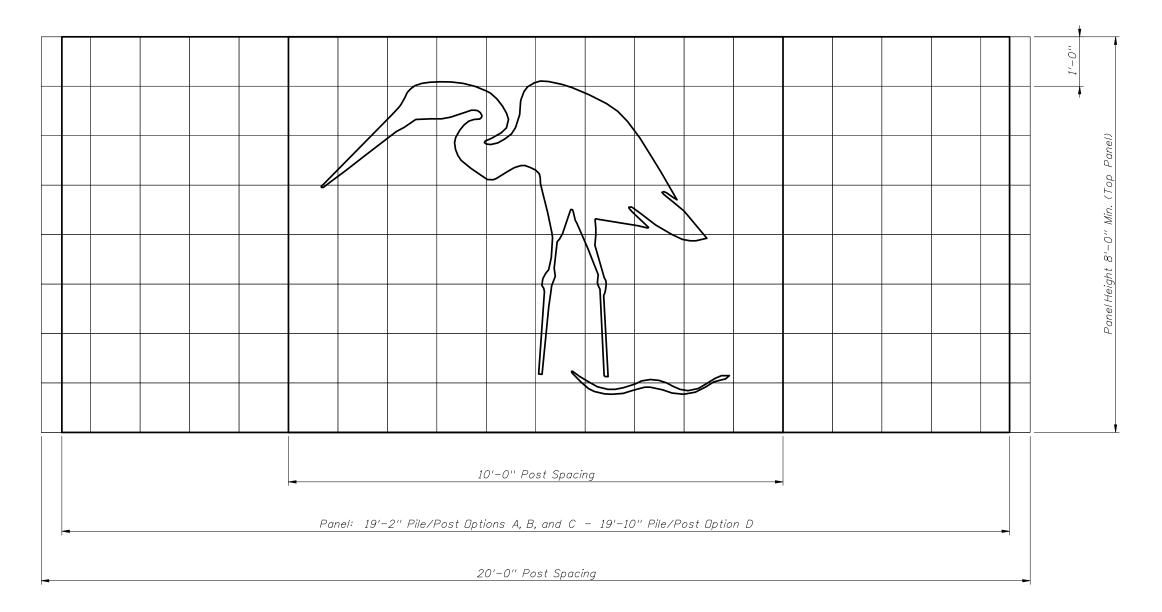


SNOWY EGRET (SE-1)



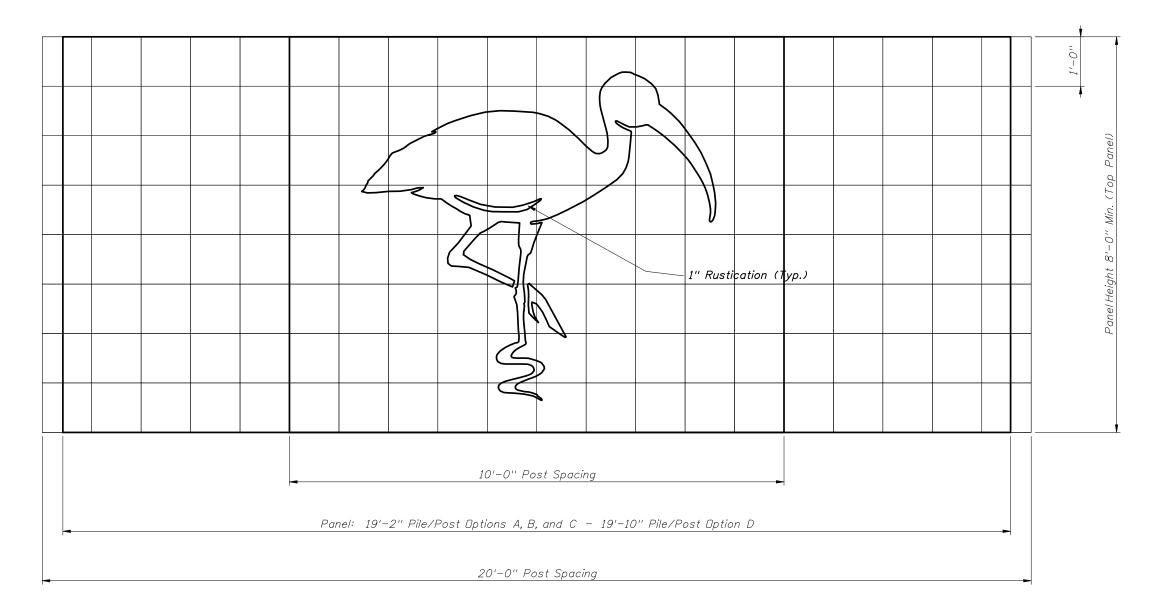


SNDWY EGRET (SE-2)



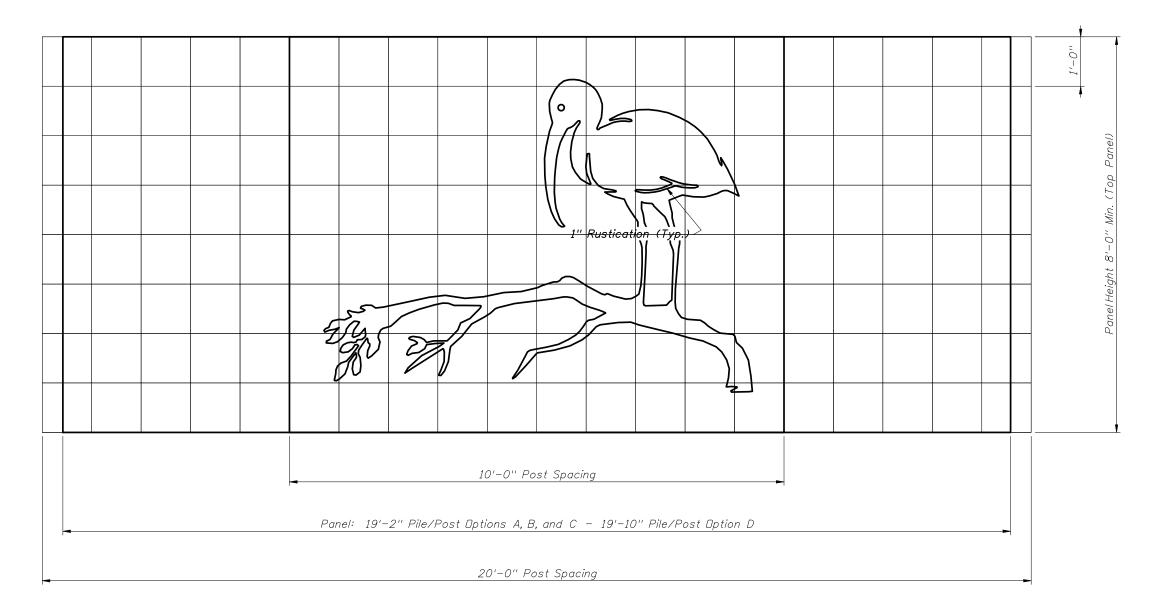


WHITE IBIS (WI-1)





WHITE IBIS (WI-2)





		GEDTECHN	IICAL INFO	RMATION	;	able Date 7–01–06
		Reinforced Soil & Random Backfill	Loose Fine Sand	Firm Fine Sand	Loose Claye Fine Sand	y Firm Clayey Fine Sand
Depth Below Existing	Wall No. 1					
Ground Line (ft.)	Wall No. 2					
Effective Unit	Weight (pcf)					
Cohesior	n (psf)	0				
Internal Fric	tion Angle					

NOTE:

If the unit weight and/or internal friction angle of the fillproposed by the Contractor differs from that shown above, the Project Engineer will contact both the District Geotechnical Engineer and the Wall Designer for a possible redesign.

	RETAINING	WALL VARIA	BLES	Table Date 7-01-08									
Wall Settlement													
Wall No.	Long Term	Short Term	Differentic	al Settlement									
	Settlement (in.)	Settlement (in.)	Longitudinal (%) (ft./100ft.)	Transverse (in.)									
1				N/A									
2				N/A									

NOTE:

Design walls for the settlements noted in the table. Long term settlement is measured from the end of wall fill placement. Transverse differential settlement is measured from the face of wall to the end of the soil reinforcement.

	SOIL REI	NFORCEMENT	LENGTI	HS FO	R EXT	ERNAL	STABI	LITY	Table Date	e 7−01−06
1	Wall Height (ft.)									
Wall No.	Reinforcement Length (ft.)									
Ň	Factored Bearing Resistance (psf)									
~	Wall Height (ft.)									
Wall No.	Reinforcement Length (ft.)									
Ř	Factored Bearing Resistance (psf)									

NOTES:

1. The reinforcement strap lengths shown above are the minimum lengths required for external stability. The reinforcement lengths used in the construction of the retaining walls will be the longer of that required for external or internal stability (determined by proprietary wall companies).

2. The Factored Bearing Resistances shown above are the critical (lowest) values from all the load cases analyzed using LRFD methodology.

NOTES:

- 1. Concrete facing panel surfaces treatment will be ______.
- 2. If required, the soil reinforcement and fasteners for the abutment back wall will be designed and furnished by the proprietary wall company. fasteners will be included in the cost of the Retaining Wall System.
- 3. Applicable FDDT Wall Types for each wall location are listed below. See the Qualified Products List for approved Wall Systems and Design Standards Index No. 5300 for allowable Wall Type substitutions. Wall No. 1 - FDDT Wall Type _____ Wall No. 2 - FDDT Wall Type _____
- 4. See Design Standards Index. No. 5300 for General Notes and Details.

INSTRUCTIONS TO DESIGNER:

- 1. Fill in Notes and add/modify/delete as necessary.
- 2. List each wall in Note 3 separately, showing applicable wall system.
- See Structures Design Guidelines, Chapter 3 for required design based internal friction angle and unit weight of Reinforced Soil and Random Backfill.
- 4. Fill in "Retaining Wall Variables" and "Soil Reinforcement Lengths for External Stability" tables based on requirements for this project. The Wall Heights to be filled in Guidelines Chapter 3 Figures in the Structures Manual for details.
- 6. Work this cell with Design Standards Index No. 5300.

PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING

The soil reinforcement will be designed to resist a factored horizontal load of _____ kips/ft. of back wall width. The cost of soil reinforcement and

3. Fill in the "Geotechnical Information" table based on soil conditions for this project. for the "Soil Reinforcement Lengths for External Stability" table refer to the height above the leveling pad, measured to the top of the wall coping. See Structures Design 5. Transverse Differential Settlement is only applicable for widening of existing embankments.

		GEDTECHN	IICAL INFOR	RMATION	To	able Date 7–01–06
		Reinforced Soil & Random Backfill		Firm Fine Sand	Loose Clayey Fine Sand	/ Firm Clayey Fine Sand
Depth Below Existing	Wall No. 1					
Ground Line (ft.)	Wall No. 2					
Effective Unit	Weight (pcf)					
Cohesio	n (psf)	0				
Internal Fric	tion Angle					

NOTES:

1. See the Qualified Products List for approved Wall Systems (Type 3). 2. See Design Standards Index No. 5301 for General Notes and Details.

NOTE:

If the unit weight and/or internal friction angle of the fill proposed by the Contractor differs from that shown above, the Project Engineer will contact both the District Geotechnical Engineer and the Wall Designer for a possible redesign.

	RETAINING WALL VARIABLES Table Date 1-01-08													
Wall No.	Long Term Settlement (in.)	Short Term Settlement (in.)	Differential Settlement (%) (ft./100ft.)	Air Contaminants Classification										
1														
2														

NOTE:

Design walls for the settlements noted in the table.

Long term settlement is measured from the beginning of wall construction.

	SOIL REI	NFORCEMENT	HS FO	R EXT	ERNAL	STABI	LITY	Table Date 7-01-		
1	Wall Height (ft.)									
Wall No.	Reinforcement Length (ft.)									
M	Factored Bearing Resistance (psf)									
~	Wall Height (ft.)									
Wall No.	Reinforcement Length (ft.)									
Ň	Factored Bearing Resistance (psf)									

NOTES:

1. The reinforcement strap lengths shown above are the minimum lengths required for external stability. The reinforcement lengths used in the construction of the retaining walls will be the longer of that required for external or internal stability (determined by proprietary wall companies).

2. The Factored Bearing Resistances shown above are the critical (lowest) values from all the load cases analyzed using LRFD methodology.

INSTRUCTIONS TO DESIGNER:

- Guidelines Chapter 3 Figures in the Structures Manual for details.
- 4. Work this cell with Design Standards Index No. 5301.

PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING

 Fill in Notes and add/modify/delete as necessary.
 Fill in the "Geotechnical Information" table based on soil conditions for this project. See Structures Design Guidelines, Chapter 3 for required design based internal friction angle and unit weight of Reinforced Soil and Random Backfill. 3. Fill in "Retaining Wall Variables" and "Soil Reinforcement Lengths for External Stability" tables based on requirements for this project. The Wall Heights to be filled in for the "Soil Reinforcement Lengths for External Stability" table refer to the height above the leveling pad, measured to the top of the wall coping. See Structures Design

				CANT	ILEVER	SIGN	STRUCTURES DATA TA	ABLE			NDTES:
			DIME	NSIONS		PANELS		MEMBER SIZES	BACKRAKE	1. Design Wind Speed = mph 2. Bolts (except Anchor Bolts) are	
SIGN ND.	STATION / DFFSET	A		В	С	N	D (CHORD)	E (WEB)	F (UPRIGHT)	G	2. Bolts (except Anchor Bolts) are
		ft	ft	in	in	#	D. D. x Wall Thk. (in)	Angle (in)	D. D. x Wall Thk. (in)	in	
											 FDUNDATION NOTES: Design based on Borings taken sealed by Assumptions and Values used in design: Soil Type Soil Layer Thickness = ft. Soil Friction Angle = deg. Soil Weight = pcf Design Water Table is ft. below surface
											NDTE – Work with Index 11310.

	CANTILEVER SIGN STRUCTURES DATA TABLE (CONT.)																														
								GUS	SSET	PLATE	s												TRUSS	CONNEC	TION			SI	PLICE		
SIGN ND.	GA	GB		GC		GD		GE		GF		GG		GH		(GJ	GK	TA	TB	TC	TD	TE	TF	TG	TH	TJ	SA	SB	SC	SD
	in	in	ft	in	ft	in	ft	in	ft	in	ft	in	f	t in	f	t	in	in	in	#	#	in	in	in	in	in	in	Angle (in)	#	in	#
							+																								
							$ \rightarrow $																							_	
			+				+													_											
																														-	

FG FH size size			
size size	e size	e in	# / :
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		_	

				CAN7	ILEVER	R SIGN	STRUCTURES DATA TA	ABLE			NOTES:
			DIME	NSIONS		PANELS		MEMBER SIZES		BACKRAKE	1. Design Wind Speed = mph 2. Bolts (except Anchor Bolts) are
SIGN ND.	STATION / OFFSET	A		В	С	N	D (CHORD)	E (WEB)	F (UPRIGHT)	G	2. Bolts (except Anchor Bolts) are
		ft	ft	in	in	#	D. D. x Wall Thk. (in)	Angle (in)	D. D. x Wall Thk. (in)	in	
											 FOUNDATION NOTES: Design based on Borings taken sealed by Assumptions and Values used in design: Soil Type Soil Layer Thickness = ft. Soil Friction Angle = deg. Soil Weight = pcf Design Water Table is ft. below surface
											NDTE – Work with Index 11310.

											C,	ANTILE	EVE	R SIG	SN S	STRUCT	URES L	DATA	TAE	BLE	(CDN	IT.)								
								GUS	SET	PLATES	:											TRUSS	CONNEC	TION			SI	PLICE		
SIGN ND.	GA	GB		GC		GD		GE		GF		GG		GH		GJ	GK	TA	TB	TC	TD	TE	TF	TG	TH	TJ	SA	SB	SC	SD
	in	in	ft	in	ft	in	ft	in	ft	in	ft	in	ft	t in	ft	in	in	in	#	#	in	in	in	in	in	in	Angle (in)	#	in	#
																														1
													_				_	_	_											
			++				+																							
																														1
							+						_				_													

						CANTILI	EVER S	SIGN S	TRUCT	URES L	DATA	A TAE	3LE	CONT)						
				B,	4SE	CONNECT	ION				ANG	CHOR			FOO	TING – D	RILLE	D S	HAFT	Г	
SIGN ND.	BA	BB	BC	BD		BE	BF	BG	BH	BJ	L	3K		FA		FB		FC			FD
	in	#	in	in	ft	in	in	in	in	in	ft	in	ft	in	ft	in	#	/ S	ize	ft	in
		_																			

ALTERNATE DRILLED SHAFT FOUNDATION

							SPAN S	IGN STRUCTURES	DATA TABLE					
			DIMENSIONS		PNLS			ME	MBER SIZES			SPLICE		
SIGN#	STATION	A	В	С	D	Ε	F (CHORD)	G (WEB)	H (LEFT UPRIGHT)	J (RIGHT UPRIGHT)	K (CAMBER)	SA	SB	SC SC
		ft	ft	ft	#	in	D. D. x Wall Thk. (in)	Angle (in)	D. D. x Wall Thk. (in)	D. D. x Wall Thk. (in)	in	Angle (in)	#	in

							SPA	AN SIG	GN	STRUC	CT	URES D	ΑΤ	A TAB	LE	(CONT	.)									
		ALT	TERNATE	SPLICE											G	USSET .	PLA	TES	6							
SIGN#	PA	PB	PC	PD	PE	PF	GA	GB		GC		GD		GE		GF			GG		GH		GJ		GK	GL
	in	in	in	in	in	#	in	in	ft	in	ft	in	ft	in	ft	in	fi	t	in	ft	in	ft	in	ft	in	in

					SPAN .	SIGN S	TRUCT	URES I	DATA	TAL	BLE (CONT.)			
			LE	FT UPR	IGHT CO	NNECTION	/				R.	IGHT UF	PRIGHT C	CONNECTI	ON	
SIGN#	LA	LB	LC	LD	LE	LF	LG	LH	RA	RB	RC	RD	RE	RF	RG	RH
	in	#	in	in	in	in	in	in	in	#	in	in	in	in	in	in

NDT	'ES:
1.	Des
2.	Bol
3.	Ere
	То

							SPAN .	SIGN S	STRUCT	URES	DATA	TAB	LE (CONT	.)						
				LEF	ΤE	BASE CONN	VECTION							RIGH	T E	BASE CON	NECTION			
SIGN#	BA	BB	BC	BD		BE	BF	BG	BH	BJ	CA	CB	СС	CD		CE	CF	CG	СН	CJ
	in	#	in	in	ft	in	in	in	in	in	in	#	in	in	ft	in	in	in	in	in

				Sł	PAN S	SIGN S	TRUC	CTURE	S L	ΟΑΤΑ ΤΛ	ABL	E (CDN	Т.)		
				LEFT DRIL	LED S	SHAFT					1	RIGHT DRI	LLED SHAFT		
SIGN#		DA		DB		DC	DD	DE		FA		FB	FC	FD	FE
	ft	in	ft	in	#	/ size	in	in	ft	in	ft	in	# / size	in	in

NUTES:
 Design Wind Speed = mph
 Bolts (except Anchor Bolts and Alt. Splice Bolts) are
 Erection is the Contractor's responsibility. To facilitate erection, the Contractor should consider using two vertical lift points, each located near a panel point approximately 20 to 25% of the truss length from each end.
 'DC' and 'FC' shall include quantity and size of reinforcing steel.

FOUNDATION NOTES: 1. Design based on Borings taken sealed by 2. Assumptions and Values used in design: Soil Type Soil Layer Thickness = ft. Soil Friction Angle = Soil Weight = pc deg. Soil Weight = pcf Design Water Table is ft. below surface

NDTE – Work with Index 11320.

					S	TANDARI	D MAST	ARM A	SSEMBL	IES DAT	TA TABL	E					
STRUCTURE	(1) ASSEMBLY		FIRST ARN	1	S	ECOND ARI	М				PD	ΊLΕ		SF	PECIAL DR.	ILLED SHA	FT ⁽⁴⁾
ID NUMBERS	ASSEMBLY NUMBERS	ARM TYPE	FAA ⁽²⁾ (ft.)	FBA ⁽²⁾ (in.)	ARM TYPE	FAA ⁽²⁾ (ft.)	FBA ⁽²⁾ (in.)	UF (deg)	LL (deg)	POLE TYPE	UAA ⁽³⁾ (ft.)	UB (ft.)	UCA ⁽³⁾ (in.)	DA (ft.)	DB (ft.)	RA	RB

TABLE NOTES:

1. Assembly Number Legend

```
Single Arm:
Arm Type - Pole Type = D# - S#
                   = E# - T#
                    = F # - W #
Double Arm:
```

First Arm Type – Second Arm Type – Pole Type = D# - D# - S# = E# - E# - T#= F# - F# - W#

- 2. If an entry appears in columns "FAA" and "FBA", a shorter arm is required. This is obtained by removing length from the arm tip. For these cases the mast arm length shall be shortened from "FA" to "FAA" and the tip diameter shall be increased from "FB" to "FBA".
- 3. If an entry appears in columns "UAA" and "UCA", a shorter pole is required. This is obtained by removing length from the pole tip. For these cases the pole height shall be shortened from "UA" to "UAA" and the pole tip diameter shall be increased from "UC" to "UCA".
- 4. The foundations for Standard Mast Arm Assemblies are pre-designed and are based upon the following conservative soil criteria which covers the great majority of soil types found in Florida. Only complete the "Special Drilled Shaft" data information if site conditions dictate drilled shafts with additional foundation capacity.

```
Classification = Cohesionless (Fine Sand)
Friction Angle = 30 Degrees (30°)
Unit Weight = 50 lbs. / cu. ft. (assumed saturated)
```

GENERAL NOTES:

- 1. Work this sheet with the Signal Designer's "Mast Arm Tabulation". See "Mast Arm Tabulation" for special instructions that include non-standard Handhole location, paint color, terminal compartment requirement, and pedestrian features.
- 2. Work with Index Nos. 17743 and 17745.

								SPECI	AL MA	ST A	RM AS	SEMBL	LIES I	DATA	TABLE	1								
NUMBER OF	STRUCTURE		FIRS	t ARM		FIR.	ST ARM	EXTEN	SION		SECON	ID ARM		SECC	IND ARM	1 EXTEN	ISION				POLE			
LOCATIONS	NUMBER	FA(ft)	FB(in)	FC(in)	FD(in)	FE(ft)	FF(in)	FG(in)	FH(in)	SA(ft)	SB(in)	SC(in)	SD(in)	SE(ft)	SF(in)	SG(in)	SH(in)	UA(ft)	UB(ft)	UC(in)	UD(in)	UE(in)	UF(deg)	UG(ft)
																								
																							 	
																								<u> </u>

								SPEC	CIAL N	IAST	ARM	ASSEM	BLIES	DATA	TAB	LE (C	ONT.)									
STRUCTURE		F	IRST A	RM CON	NECTIO	V (in)	First Arm Camber Angle = 2 Degrees					SECOND ARM CONNECTION (in)				(in)	Second Arm Camber Angle = 2 Degrees									
NUMBER	#Bolts	HT	FJ	FK	FL	FM	FN	FO	FP	FQ	FR	FS	FT	#Bolts	HT	SJ	SK	SL	SM	SN	SD	SP	SQ	SR	SS	ST

	SPECIAL MAST ARM ASSEMBLIES DATA TABLE (CONT.)																					
STRUCTURE		POL	LE BASE	E CONNE	CTION	(in)		SHAFT AND REINF.				LUMINAIRE AND LUMINAIRE CONNECTION										
NUMBER	#Bolts	BA	BB	BC	BD	BE	BF	DA(ft)	DB(ft)	RA	RB	LA(ft)	LB(ft)	LC(in)	LD(in)	LE	LF(ft)	LG(in)	LH(in)	LJ(in)	LK(in)	LL(deg)

- NDTES:
 1. Work with Index 17745.
 2. Design Wind Speed = mph
 3. Contractor shall coordinate anchor bolt requirements with fabricator.
 4. Contractor shall identify Structures Numbers and submit detailed shop drawings.

FDUNDATION NOTES:
Design based on Borings taken sealed by
Assumptions and Values used in design: Soil Type Soil Layer Thickness = ft. Soil Friction Angle = deg. Soil Weight = pcf Design Water Table is ft. below surfer ft. below surface

PRESTRESSED BEAM TEMPORARY BRACING DATA TABLES

TABLE OF WIND LOAD VARIABLES	Table Date 1-01-10
WIND SPEED, BASIC (MPH)	
WIND SPEED, CONSTRUCTION INACTIVE (MPH)	
WIND SPEED, CONSTRUCTION ACTIVE (MPH)	
VELOCITY PRESSURE EXPOSURE COEFFICIENT	
GUST EFFECT FACTOR	

TABLE OF ASSUMED CONSTRUCTION LOADS (UNFACTORED)	Table Date 1-01-10
BUILD-UP (PLF)	
FORM WEIGHT (PSF)	
FINISHING MACHINE TOTAL WEIGHT (KIP)	
FINISHING MACHINE WHEEL LOCATION BEYOND EDGE OF DECK OVERHANG (IN.)	
DECK WEIGHT (PSF)	
LIVE LOAD (PSF)	
LIVE LOAD AT EXTREME DECK EDGE (PLF)	

		TABLE OF	TEMPORARY BR	RACING VARIABLES	S	Table Date	- 7-01-10
SPAN ND.	L _B , MAXIMUM UNBRACED LENGTH (FT)			OVERTURNING FORCE AT EACH BEAM END AND ANCHOR BRACE (KIP×FT)	OVERTURNING FORCE AT EACH INTERMEDIATE SPAN BRACE (KIPxFT)		TOTAL LINES OF BRACING
						YES/ND	
						YES/ND	
						YES/ND	
						YES/NO	

BEAM TEMPORARY BRACING NOTES:

- Based on investigation of the beam stability, temporary bracing as shown in the 'TABLE OF TEMPORARY BRACING VARIABLES' and Design Standard Index No. 20005 is required. The Table and following information is provided to aid the Contractor in design of beam temporary bracing:
- 1. Design the bracing members and connections to transfer both compressive and tensile forces equal to the horizontal forces given in the 'TABLE OF TEMPORARY BRACING VARIABLES'. Also design bracing members and connections to be capable of resisting the overturning forces given in the Table, non-simultaneously with horizontal forces. Assume that horizontal bracing forces are applied perpendicular to the beam web at mid-height of the beam, and assume that overturning bracing forces are applied at the centerline of the beam at the top of the top flange.
- 2. The horizontal brace forces have been determined by application of the Construction Inactive Wind Load as listed in the 'TABLE OF WIND LOAD VARIABLES'. The overturning brace forces have been determined by application of the Construction Active Wind Load as listed in the 'TABLE OF WIND LOAD VARIABLES' plus the assumed construction loads shown in the 'TABLE OF ASSUMED CONSTRUCTION LOADS'. It is the Contractor's responsibility to re-calculate the bracing requirements if the actual construction loads exceed the assumed loads shown, or if the finishing machine wheel location from the edge of the deck overhang exceeds the value listed.
- 3. The temporary bracing at the ends of the beams shall be installed prior to crane release if indicated in the 'TABLE OF TEMPORARY BRACING VARIABLES'. Beams shall not be left un-braced during non-work hours. Bracing shall remain in place until diaphragm concrete or bridge deck concrete reaches 2500 psi.
- 4. The exposure period (defined as the time period for which temporary load cases of the superstructure exist) is assumed to be less than one year. Horizontal bracing forces, as specified in the 'TABLE OF TEMPORARY BRACING VARIABLES', are not valid if the exposure period is more than one year; for this case the Contractor shall re-calculate bracing requirements. 5. Horizontal and overturning forces are factored per the Strength III limit state for construction.

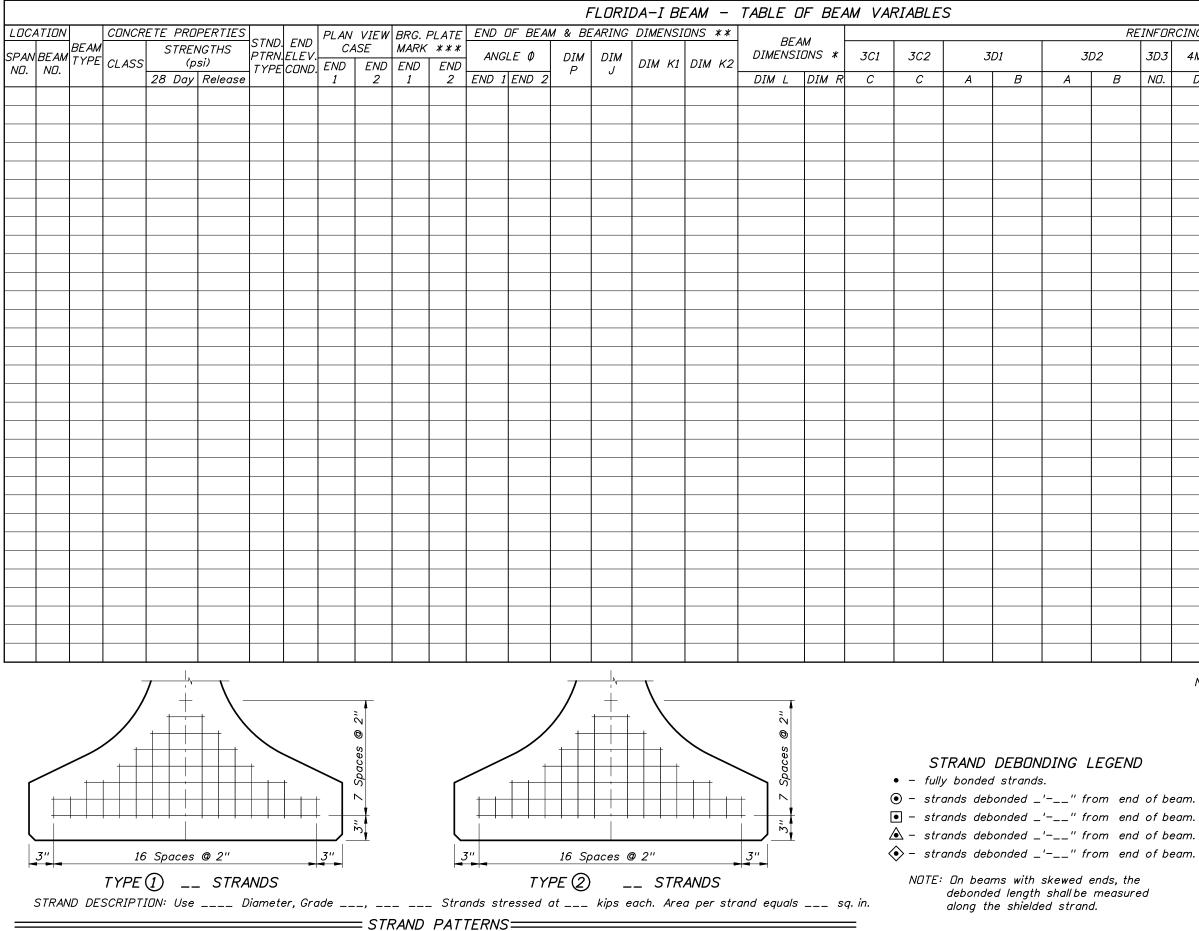


									Table Do	ate 7-01-09
	INFOF	CING S	TEEL							
	3D3	4 <i>M</i> 1	4 <i>M2</i>	4 <i>M3</i>		ND.	BARS	5 51		SP. BARS 5K *
	ND.	D	D	ND.	ND.	S1	<i>S2</i>	S.	3 S4	V1
										-
										-
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1										
										+

NDTE: Work this sheet with Design Standards Index Nos. 20010 and the applicable "Florida–I Beam Standard Details" Index.

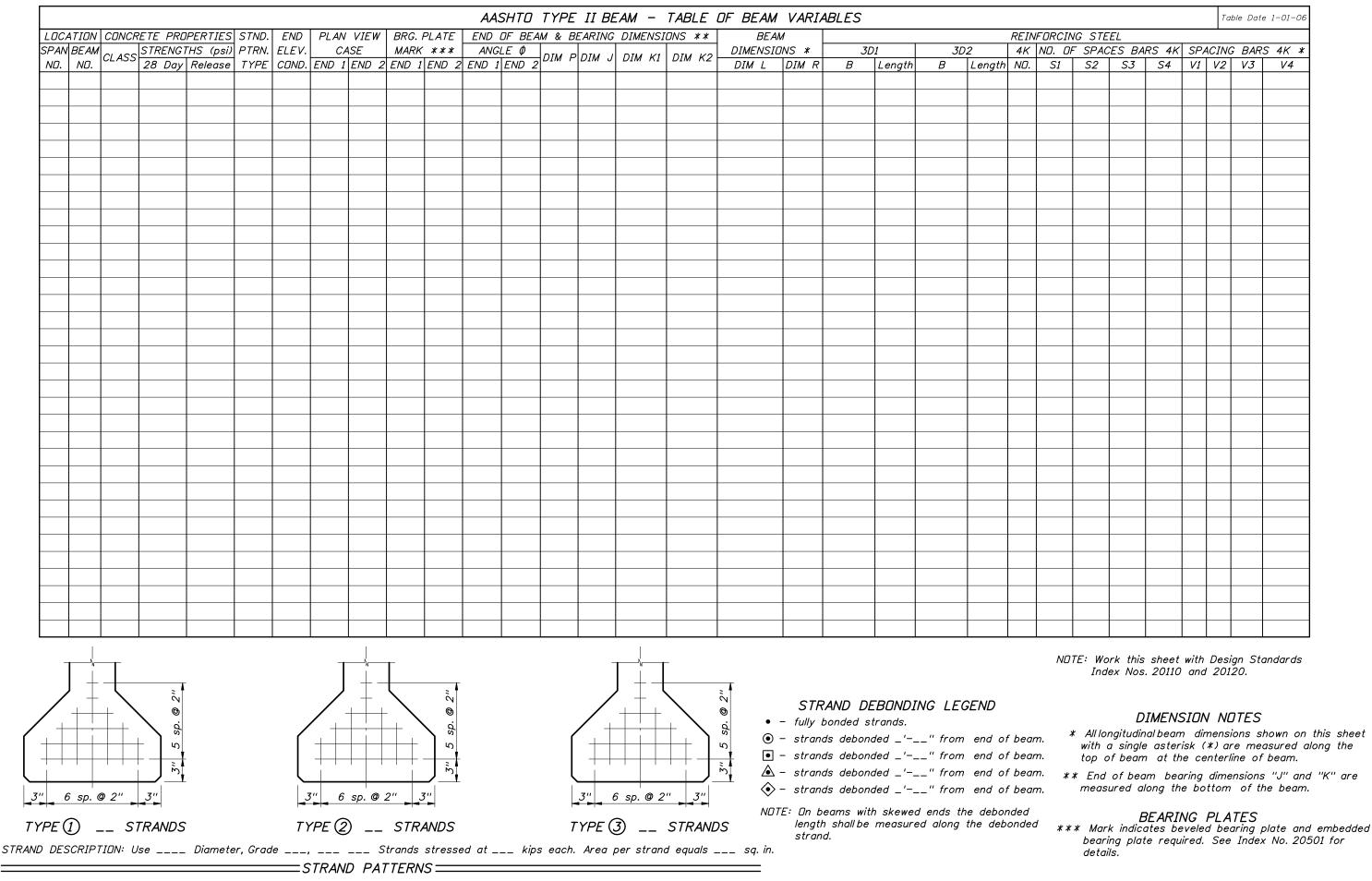
DIMENSION NOTES

* All longitudinal beam dimensions shown on this sheet with a single asterisk (*) are measured along the centerline of beam. Dimension "R" is calculated at mid-height of the beam. ****** End beam bearing dimensions "J" and "K" are

measured perpendicular to *Q* Bearing along the bottom of the beam.

BEARING PLATES

*** See Index No. 20511 and the Bearing Plate Data Table for details.



								le Date			
!N	HURCIN	IG STE	EL						_		
<	FORCIN	- SPAC	ES BA	RS 4K	SPA	1CI	NG	BAR	S	4K	*
1.	S1	<u>S2</u>	S3	<u>S4</u>	V1	V	2	V3		V4	
						-					
											-
						-	+				

NDTE: Work this sheet with Design Standards Index Nos. 20110 and 20120.

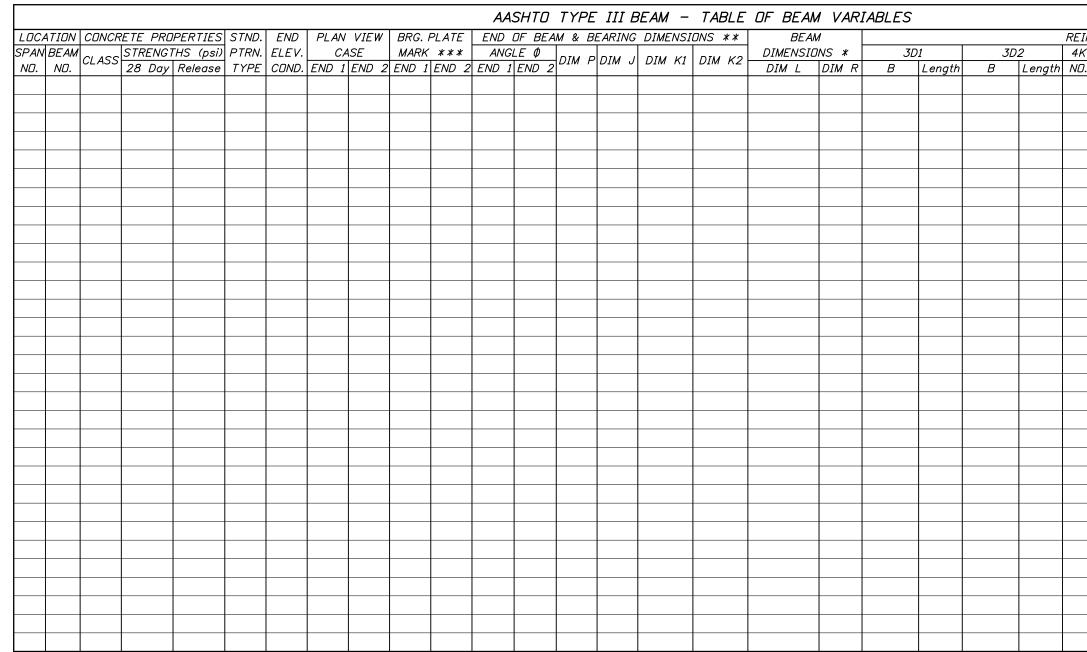
DIMENSION NOTES

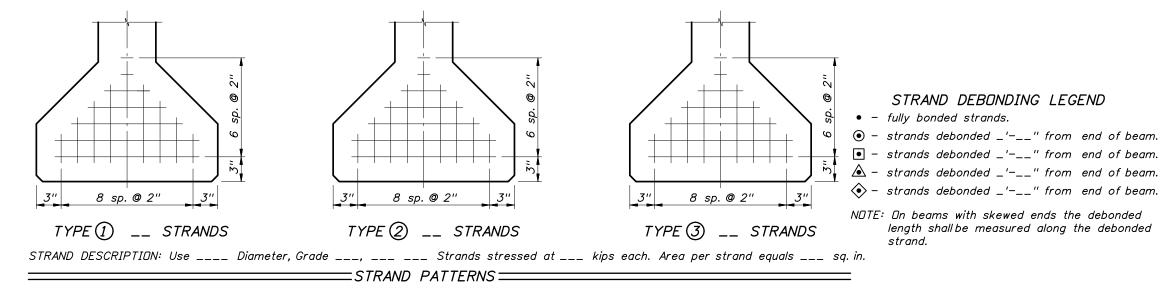
* All longitudinal beam dimensions shown on this sheet with a single asterisk (*) are measured along the top of beam at the centerline of beam.

****** End of beam bearing dimensions "J" and "K" are measured along the bottom of the beam.

BEARING PLATES

bearing plate required. See Index No. 20501 for details.





							Tabi	e Dat	e i	-01-	06
ĪN	FORCIN	IG STE	EL								
< 1.	NO. OF	SPAC	ES BA	RS 4K	SPA	ACI	NG	BAR	S	4K	*
1.	S1	<i>S2</i>	<i>S3</i>	<i>S</i> 4	V1	V.	2	V3		V4	
							_				
							_				
									-		
							+		-		
									-		
							_				
							_		-		

NDTE: Work this sheet with Design Standards Index Nos. 20110 and 20130.

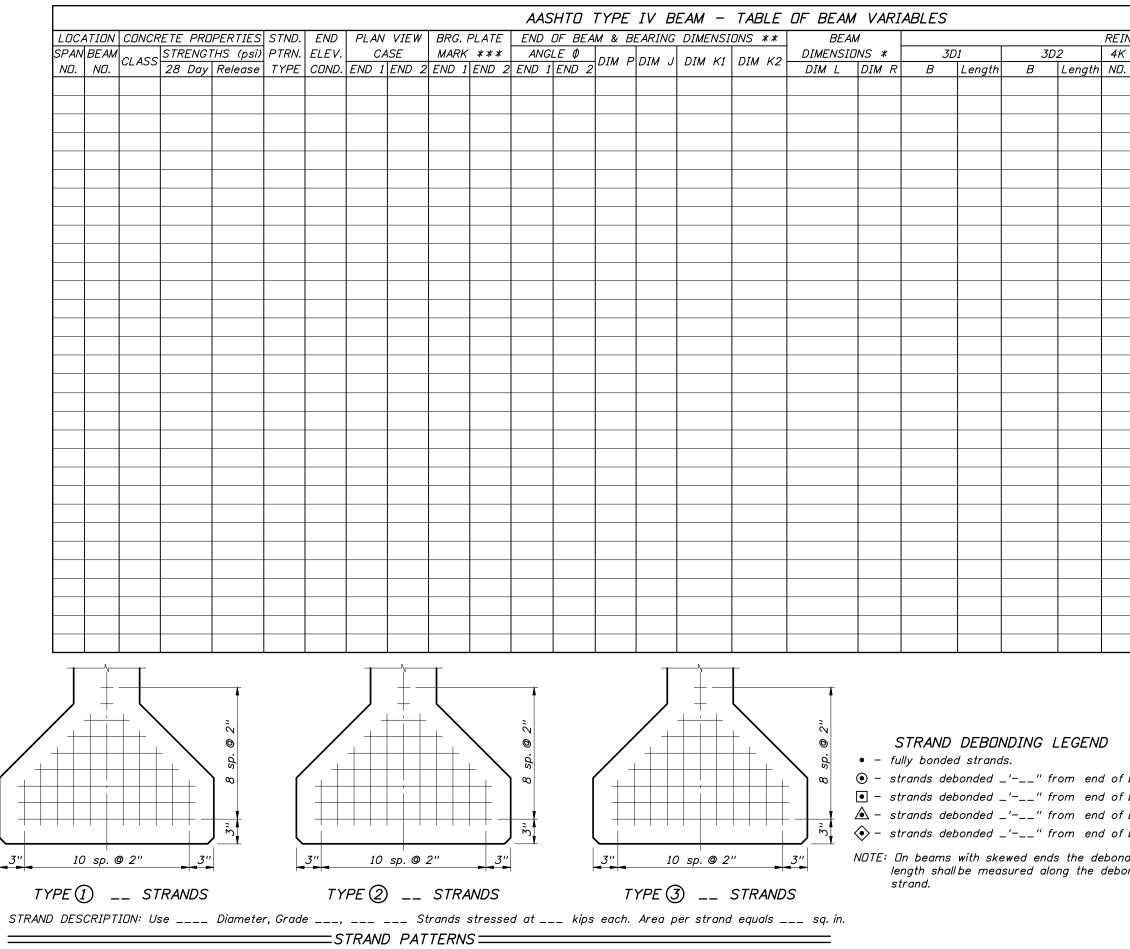
DIMENSION NOTES

т.	*	All longitudinal beam dimensions shown on this sh	eet
<i></i>		with a single asterisk (*) are measured along the	е
п.		top of beam at the centerline of beam.	

****** End of beam bearing dimensions "J" and "K" are measured along the bottom of the beam.

BEARING PLATES

length shall be measured along the debonded *** Mark indicates beveled bearing plate and embedded bearing plate required. See Index No. 20501 for details.

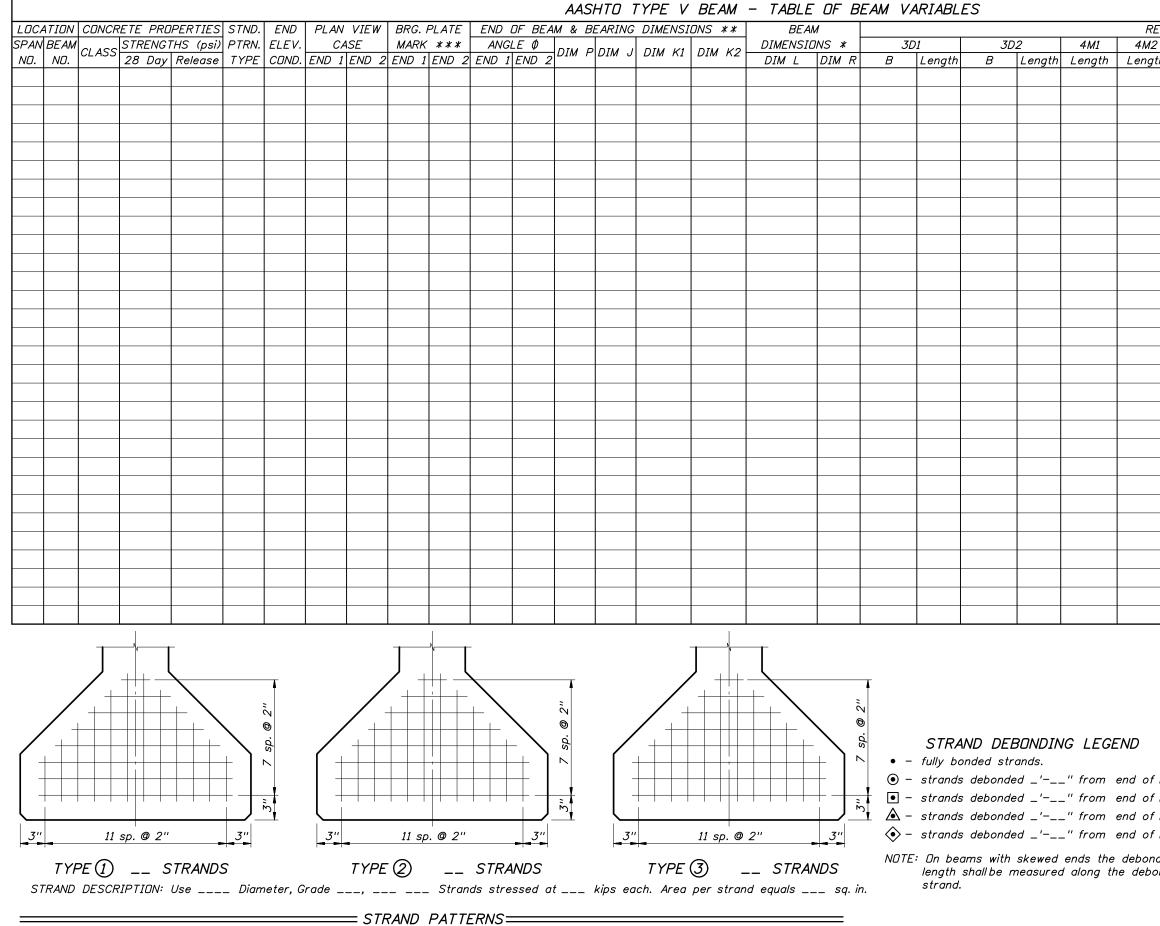


							Tab	le Date	e î	-01-	06
ĪN	FORCIN	IG STE	EL								
<	NO. OF	- SPAC	ES BA	RS 4K	SPA	AC I	ING	BAR	S	4K	*
1.	S1	S2	S3	S4	V1	V	2	V3		V4	
							+				
							_				
							_				
							_				
							_				
							-				
							_				
							_				
							+				
						-	+				
							+				
									-		

NDTE: Work this sheet with Design Standards Index Nos. 20110 and 20140.

DIMENSION NOTES

beam.	* All longitudinal beam dimensions shown on this sheet with a single asterisk (*) are measured along the top of beam at the centerline of beam.
beam.	
beam.	** End of beam bearing dimensions "J" and "K" are measured along the bottom of the beam.
beam.	BEARING PLATES
ded nded	*** Mark indicates beveled bearing plate and embedded bearing plate required. See Index No. 20501 for details.

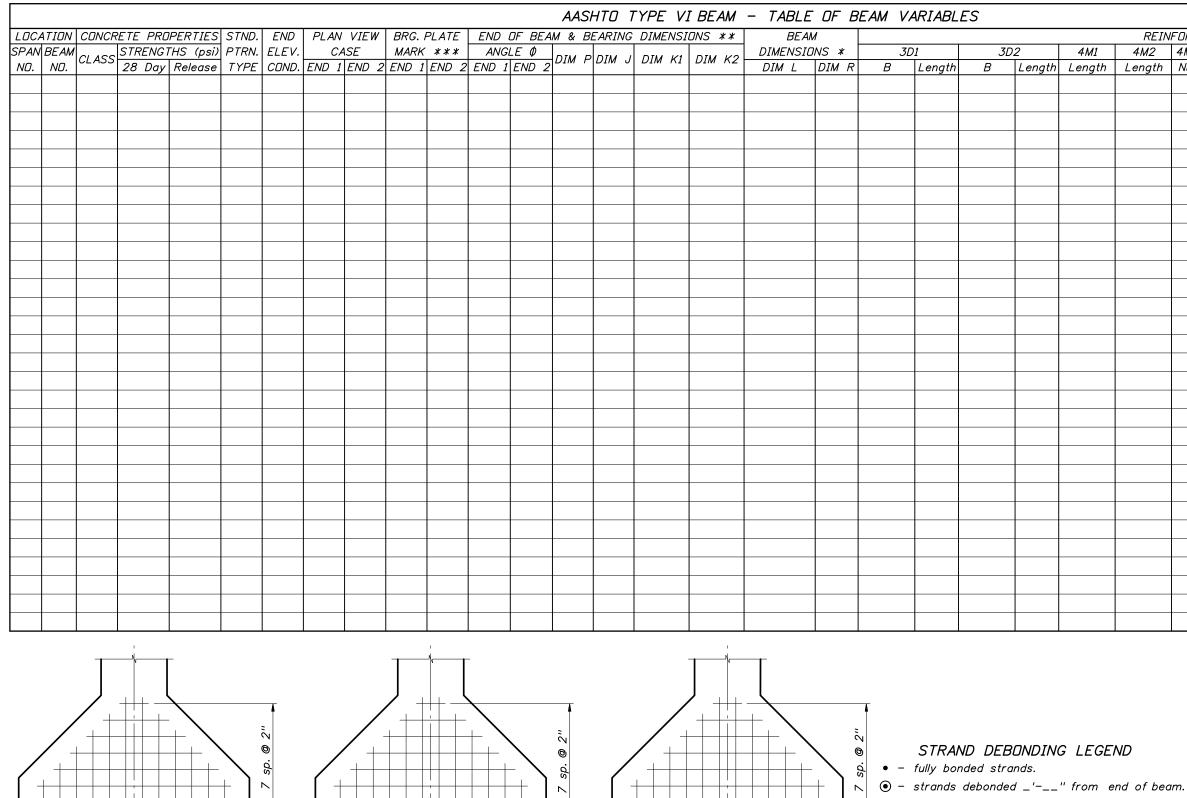


								Tab	le Date	1-01-	06
			STEEL				CDA	074/0	0400		
2 ith	4м3 ND.	эк ND.	ND. DF S1	SPAC	S3	RS 5K S4	SPA	$\frac{V2}{V2}$	BARS	5 5K V4	*
th	NU.	NU.	51	52	- 33	54	VI	VZ	<u>v</u> 3	<u></u>	

NDTE: Work this sheet with Design Standards Index Nos. 20110 and 20150.

DIMENSION NOTES

beam.	* All longitudinal beam dimensions shown on this sheet with a single asterisk (*) are measured along the top of beam at the centerline of beam.
beam.	** End of beam bearing dimensions "J" and "K"
beam.	are measured along the bottom of the beam.
beam.	BEARING PLATES
ded onded	*** Mark indicates beveled bearing plate required. Embedded bearing plates are required on all beams. See Index No. 20501 for details.



ň

3''

3"

__ STRANDS

11 sp. @ 2"

TYPE (3)

3"

__ STRANDS

ž

3"

11 sp. @ 2"

TYPE(1) = STRANDS

3''

TYPE (2)

11 sp. @ 2"

STRAND DESCRIPTION: Use ____ Diameter, Grade ___, ___ Strands stressed at ___ kips each. Area per strand equals ___ sq. in. = STRAND PATTERNS=

- - strands debonded _'-__'' from end of beam.
- ▲ strands debonded _'-__'' from end of beam.
- ♦ strands debonded _'-__' from end of beam.
- NDTE: On beams with skewed ends the debonded length shall be measured along the debonded strand.

								Τc	able Dat	e 1-01-	-06
ĪN			STEEL								
)					CES BA						
th_	NO.	ND.	S1	S2	S3	S4	V1	V2	V3	V4	

NDTE: Work this sheet with Design Standards Index Nos. 20110 and 20160.

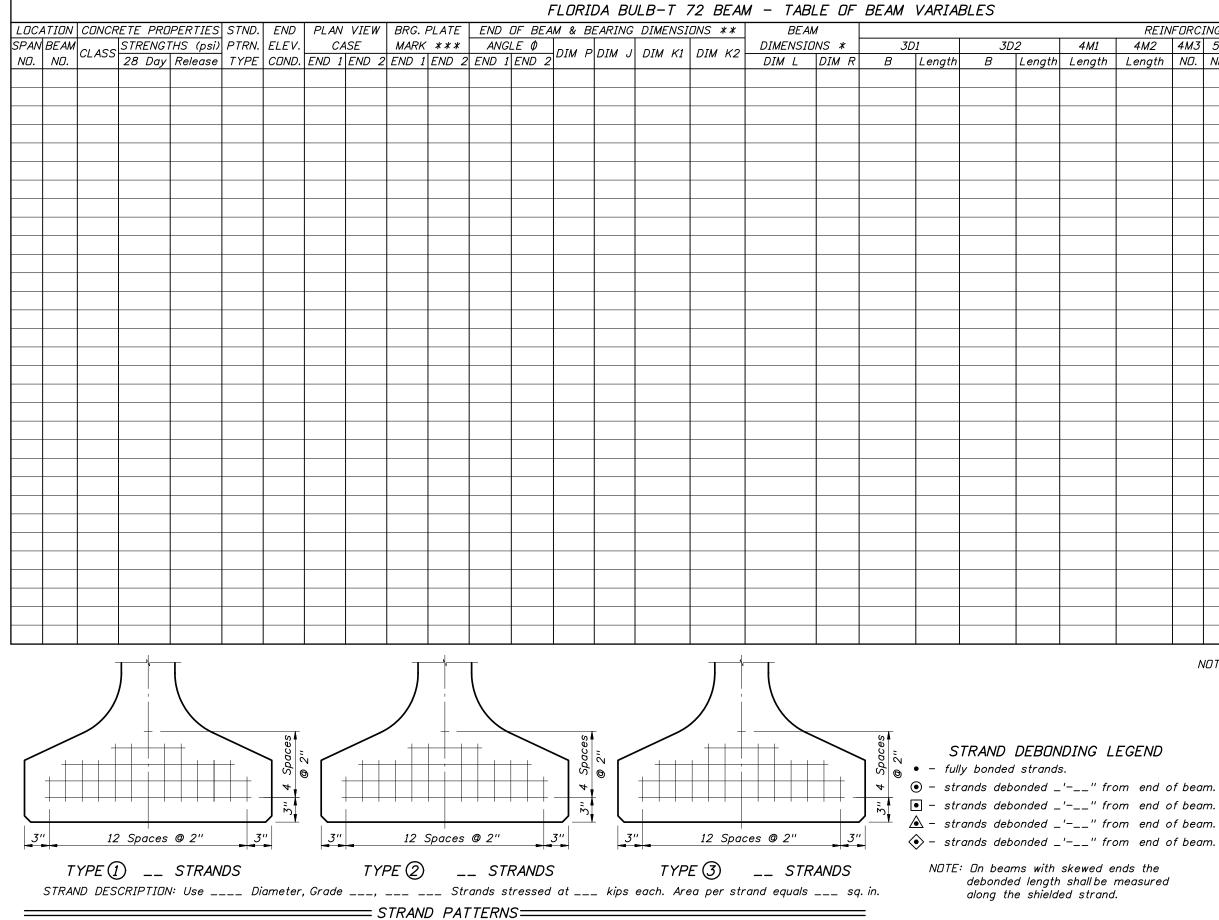
DIMENSION NOTES

* All longitudinal beam dimensions shown on this sheet with a single asterisk (*) are measured along the top of beam at the centerline of beam.

****** End of beam bearing dimensions "J" and "K" are measured along the bottom of the beam.

BEARING PLATES

******* Mark indicates beveled bearing plate required. Embedded bearing plates are required on all beams. See Index No. 20501 for details.



								Та	ble Date	e 1-01-	-06			
IN	INFORCING STEEL 4M3 5K NO. OF SPACES BARS 5K SPACING BARS 5K *													
)	4M3	5K	NO. OF	- SPAC	ES BA	RS 5K	SPA	CINC	; BAR	S 5K	*			
th.	NO.	ND.	S1	S2	S 3	S4	V1	V2	V3	V4				

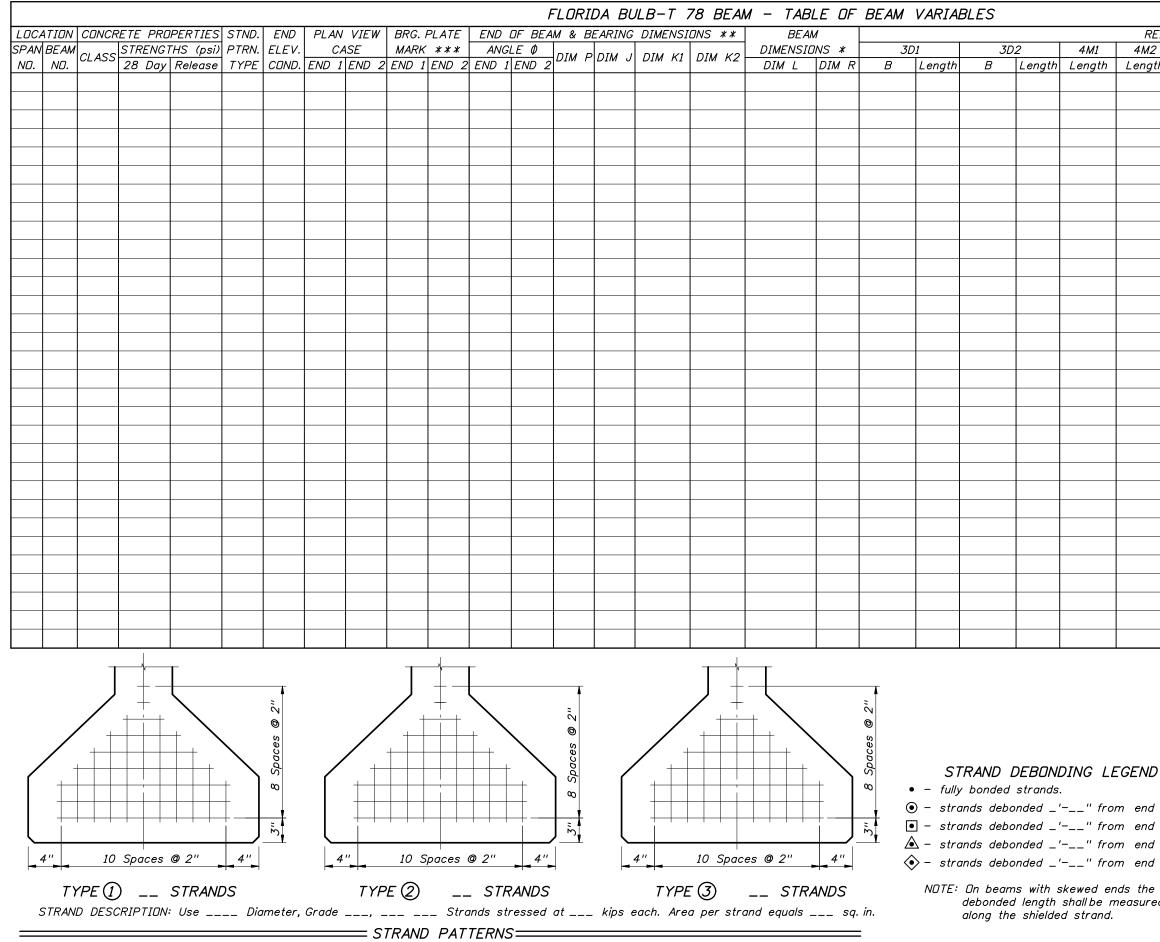
NDTE: Work this sheet with Design Standards Index Nos. 20110 and 20172.

DIMENSION NOTES

STRAND DEBUNDING LEGEND
 fully bonded strands.
 strands debonded _'-__'' from end of beam.
 strands debonded _'-__'' from end of beam.

BEARING PLATES

*** Mark indicates beveled bearing plate required. Embedded bearing plates are required on all beams. See Index No. 20501 for details.



								T	able Dat	e 1-01-	06			
IN	INFORCING STEEL 4M3 5K NO. OF SPACES BARS 5K SPACING BARS 5K *													
,							SPA	<i>ICI</i> N	IG BAR	S 5K	*			
h	ND.	ND.	S1	<i>S2</i>	S3	<i>S</i> 4	V1	V2	V3	V4				
		1												

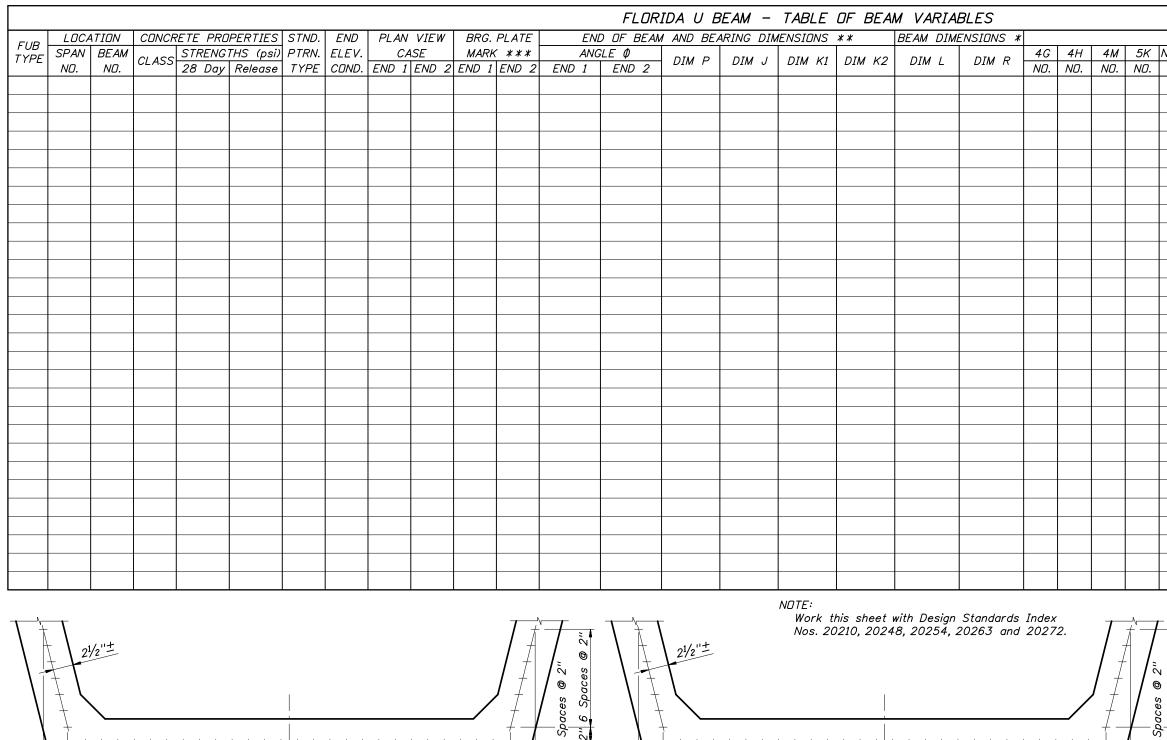
NDTE: Work this sheet with Design Standards Index Nos. 20110 and 20178.

DIMENSION NOTES

)	 All longitudinal beam dimensions shown on this sheet with a single asterisk (*) are measured
l of beam.	along the top of beam at the centerline of beam.
l of beam.	or beam.
l of beam.	** End beam bearing dimensions "J" and "K" are
l of beam.	measured along the bottom of the beam.
5	BEARING PLATES
ed	*** Mark indicates beveled bearing plate required. Embedded bearing plates are required on all beams. See Index No. 20501 for details.

BUILD-UP & DEFLECTION DATA TABLE FOR AASHTO, BULB-T AND FLORIDA-I BEAMS							F	BUILD-UP & DEFLECTION DATA TABLE FOR AASHTO, BULB-T AND FLORIDA-I BEAMS								BUILD-UP & DEFLECTION DATA TABLE FOR AASHTO, BULB-T AND FLORIDA-I BEAMS					IS Table Dc	ate 7-01-09
LOCATION	REQUIRE		TICAL	NET REAM		AD DN BUILD-UP	LDC	ATION	REQUIRI BUILD-U	ED THEORE JP OVER @	TICAL BEAM	NET BEAM CAMBER	DEAD LOAD DEFLECTION	<i>פוו–ח וזו</i> ופ		ATION		ED THEORE JP OVER @		NET BEAM	DEAD LOAD	
SPAN BEAN NO. NO.	AT BEGIN SPAN DIM "B"	AT Q SPAN DIM "C"	AT END SPAN DIM "D"	CAMBER (PRESTRESS – DEAD LOAD DF BEAM) @ 120 DAYS	DECK PO @ 120 DA DIM ''A	JR CASE YS ND. '	SPAN ND.	BEAM NO.	AT BEGIN SPAN DIM ''B''	AT Ç SPAN DIM "C"	AT END SPAN DIM "D"	- DEAD LOAD	Ø DECK POUR Ø 120 DAYS	CASE ND.	SPAN ND.	BEAI	AT BEGIN SPAN DIM "B"	AT Ç SPAN DIM "C"	AT END SPAN DIM "D"	- DEAD LOAD	Ø DECK POUR Ø 120 DAYS	CASE ND.
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NDTES: Work this sheet with Design Standard Index No. 20199.





3"

3"

STRAND DESCRIPTION: Use _____ Diameter, Grade _____, _____ Strands stressed at _____ kips each. Area per strand equals _____ sq. in.

¾''±

3''

3"

<u>∛4''±</u>

25 Spaces @ 2"

TYPE 1 __ STRANDS

'3''

3''

_¾''±

25 Spaces @ 2"

TYPE (2) __ STRANDS

																				-01-	
	REINFORCING STEEL NO. OF SPACES BARS 5K & 4M SPACING BARS 5K & 4M *																				
<	<i>NO</i> .	OF	SP.	ACE	<u>.</u> S	BA	<i>RS</i>	5	5K	&	4M	S	PAC	ING	<i>B,</i>	AR	5	5K	&	4M	*
1.		<i>S1</i>			S.	2				<i>S3</i>			V.	1		l	/2			V3	
												<u> </u>			I						

DIMENSION NOTES

- * All longitudinal beam dimensions shown on this sheet with a single asterisk (*) are measured along the top of beam at the centerline of beam.
- **End of beam bearing dimensions "J" and "K" are measured along the bottom of the beam.

BEARING PLATES

*** Mark indicates beveled bearing plate and embedded bearing plate required. See Index No. 20502 for details.

STRAND DEBONDING LEGEND

• - fully bonded strands.

"

Ñ

0

Spaces

6

2.

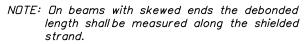
 \sim

3"

3"

¾''±____

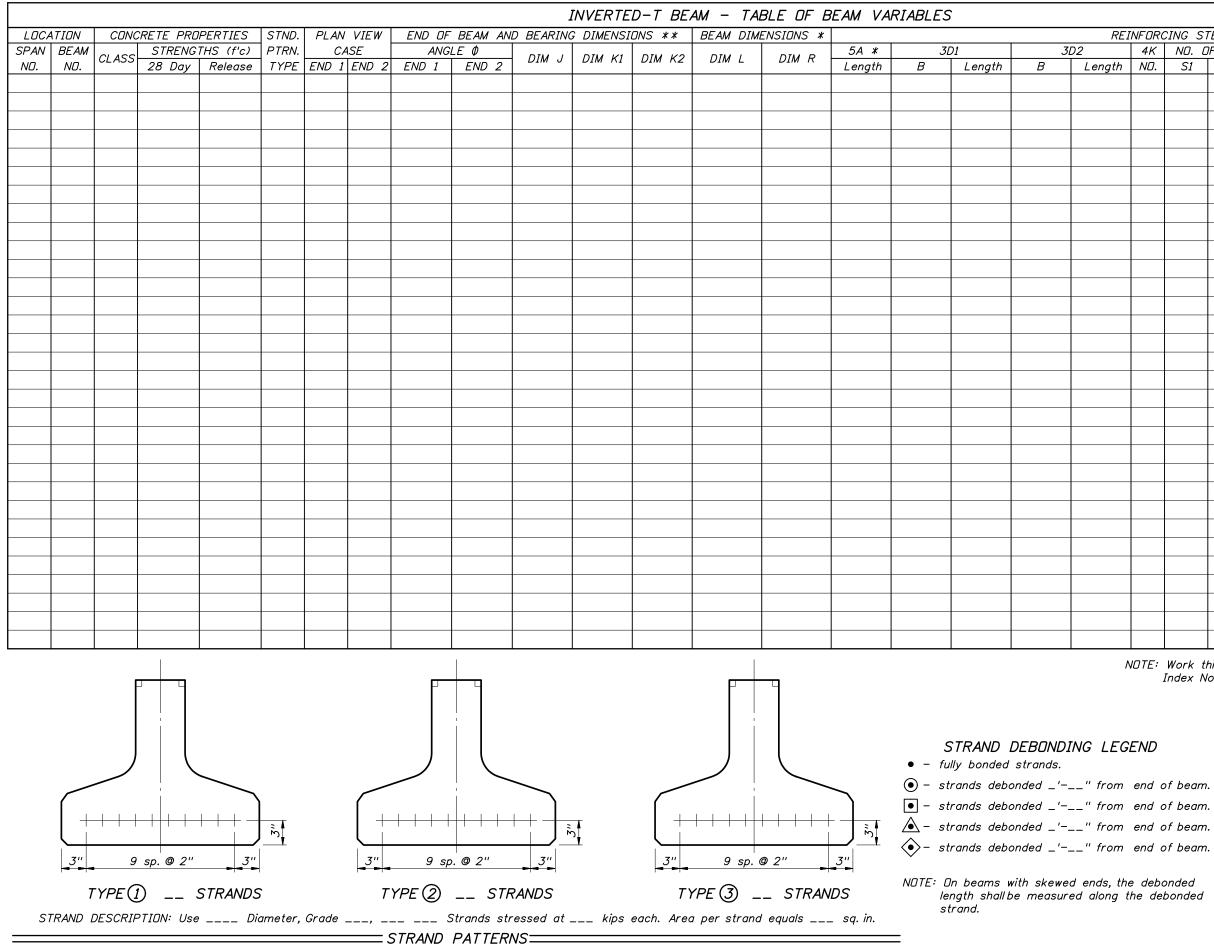
• - str	rands deboi	nded _''	from	end c	of beam.
<u> </u>		nded _''			
🛕 – str	rands deboi	nded _''	from	end c	of beam.
🔶 – str	rands deboi	nded _''	from	end c	of beam.



· · · · · ·											ı —							
	BUI	ILD-UP 8	e DEFLEC	TION DA	TA TABLE	FOR FL	DRIDA U	BEAMS	Table Do	ate 1-01-09			BU	ILD-UP 8	e DEFLEC	TION DA	TA TABLE	E Fi
LOCA	TION	REQUII BUILD-UP	RED THEORI OVER © LE	ETICAL FT FLANGE	REQUI BUILD-UP	RED THEORI OVER © RIG	ETICAL GHT FLANGE	NET BEAM CAMBER (PRESTRESS	DEAD LOAD DEFLECTION			LDCA	TION	REQUII BUILD-UP	RED THEORI OVER © LE	ETICAL FT FLANGE	REQUI BUILD-UP	IRED OVE
SPAN ND.	BEAM	SPAN	AT Q SPAN DIM "C"	SPAN	SPAN		SPAN	- DEAD LOAD	NDECK POUR	CASE ND.			BEAM	AT BEGIN SPAN			AT BEGIN SPAN DIM ''B''	
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OR FLORIDA U	BEAMS	Table Date 1-01-09
THEORETICAL R @ RIGHT FLANGE	NET BEAM CAMBER (PRESTRESS	DEAD LOAD DEFLECTION DURING
AT & AT END SPAN SPAN IM "C" DIM "D"	- DEAD LOAD OF BEAM) @ 120 DAYS	

NDTES: Work this sheet with Design Standard Index No. 20299.



							Tab	le Date .	7-01-05
ORC	CING ST	TEEL							
4K	ND. C	IF SPAC	CES BAF	RS 4K	SPACI	'NG F	OR	BARS	4K *
V <i>D</i> .	S1	S2	S3	S4	V1	V2	2	V3	V4
							-		
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NDTE: Work this sheet with Design Standards Index Nos. 20310 and 20320.

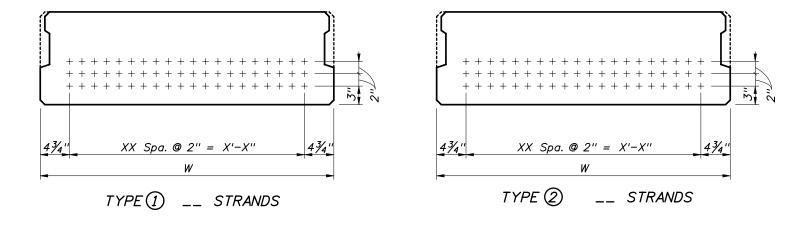
DIMENSION NOTES

* All longitudinal beam dimensions shown on this on this sheet with a single asterisk (*) are measured along the top of beam at the centerline of beam.

** End of beam bearing dimensions "J" and "K" are measured along the bottom of the beam.

									F	PREST	RESSED	CUSTO	M WIL	OTH SLA	B UNI	TS –	TABLE	E OF	VARI	ABLES									Tabl	'e Date 1–01–10
	LOCATION	CONCI	RETE PRO	IPERTIES	STND.	PLAN	' VIEW		E٨	ID OF (UNIT **			UNI									REINFO							
SPAN	SLAB UNIT	01455	STRENG	THS (psi)	PTRN.	C/	ASE	ANG	LE Ø		DIM KI	רא אזם	DIM W	DIMENSI	ONS *	4D1	4D2	4	4D3	5Y1	5Y2	4K	NO. OF	BAR S	SPACES	BAR	SPACI	NG *		REINF. ***
<i>NO</i> .	ND.(S) / TYPE	CLASS	' 28 Day	Release	TYPE	END 1	END 2	2 END 1	END 2				~~~	DIM L	DIM R	DIM D	DIM D	ND.	DIM C	DIM B	DIM B	' <i>NO</i> .	S1	S2	S3	V1	V2	V3	INDEX NO.	CASE DIM XL
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NDTE: Work this sheet with Design Standard Index Nos. 20350, 20353 and 20363.



STRAND DESCRIPTION: Use ____ Diameter, Grade ___, ___ Strands stressed at ___ kips each. Area per strand equals ___ sq. in.

STRAND DEBONDING LEGEND

- – fully bonded strands.
- - strands debonded _'-__" from end of beam.
- - strands debonded _'-__'' from end of beam.
- \triangle strands debonded _'-__'' from end of beam.
- \bigcirc strands debonded _'-__" from end of beam.
- NDTE: On slab units with skewed ends the debonded length shall be measured along the debonded strand.

DIMENSION NOTES

- * All longitudinal slab unit dimensions shown on this sheet with a single asterisk (*) are measured along the top of unit at the centerline of slab unit. Dimension "R" is calculated at mid-height of the slab unit.
- ** End of slab unit bearing dimensions "J" and "K" are measured perpendicular to & Bearing along the bottom of the slab unit.
- ******* See Index No. 20350 for modified reinforcement. See "Prestressed Slab Units – Traffic Railing Reinforcing Layout Table" for railing placement on horizontal curves. Dimension X_L is measured from the bottom left edge of the slab unit to the & of the reinforcement.

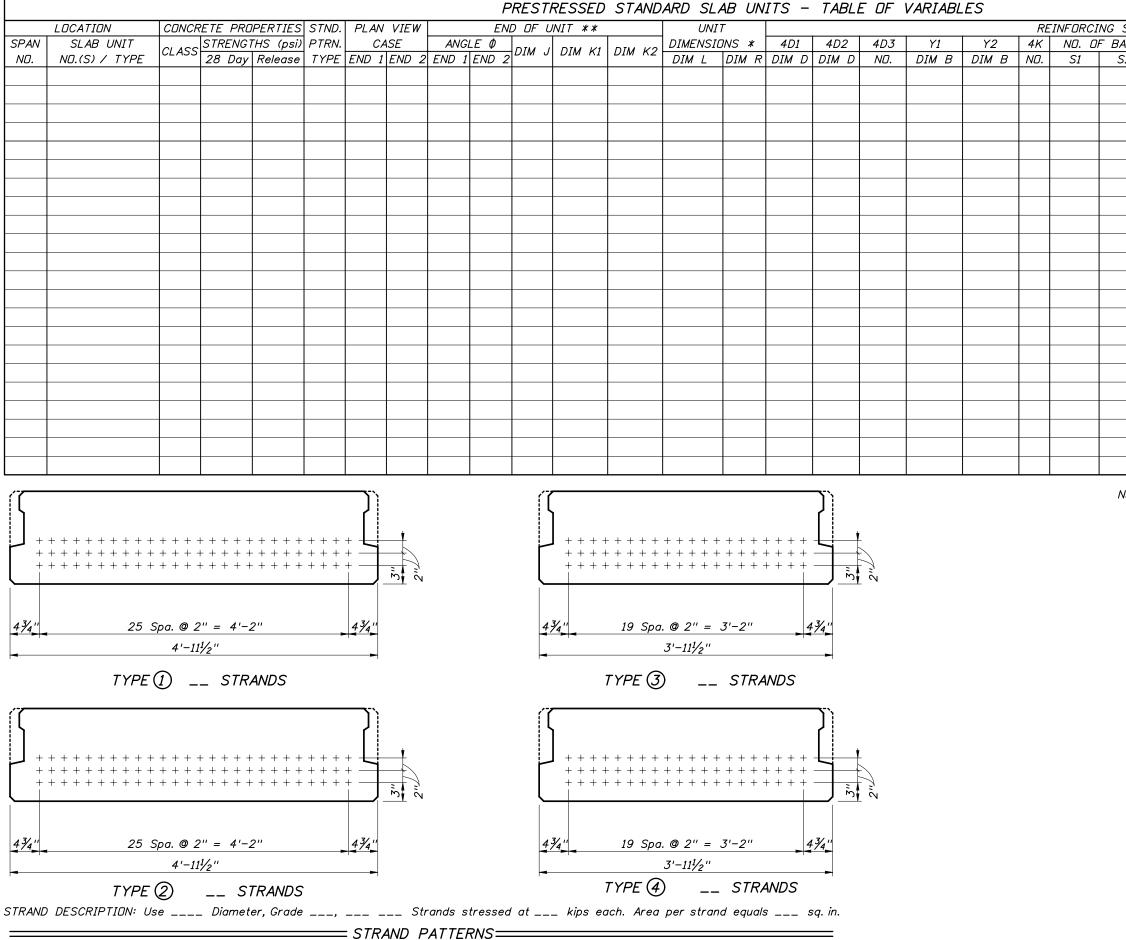


						Table	e Date 1-	-01–10
STEE	Ľ							
	PACES	BAR	SPACI				REINF	
52	<i>S3</i>	V1	V2	V3	INDEX	< ND.	CASE	DIM X_L

NDTE: Work this sheet with Design Standards Index Nos. 20350, 20354, 20355, 20364 and 20365.

STRAND DEBONDING LEGEND

- - fully bonded strands.
- - strands debonded _'-__" from end of beam.
- - strands debonded _'-__" from end of beam.
- ▲ strands debonded _'-__'' from end of beam.
- \bigcirc strands debonded _'-__" from end of beam.
- NDTE: On slab units with skewed ends the debonded length shall be measured along the debonded strand.

DIMENSION NOTES

- * All longitudinal slab unit dimensions shown on this sheet with a single asterisk (*) are measured along the top of unit at the centerline of slab unit. Dimension "R" is calculated at mid-height of the slab unit.
- ** End of slab unit bearing dimensions "J" and "K" are measured perpendicular to & Bearing along the bottom of the slab unit.
- *** See Index No. 20350 for modified reinforcement. See "Prestressed Slab Units – Traffic Railing Reinforcing Layout Table" for railing placement on horizontal curves. Dimension " X_L " is measured from the bottom left edge of slab unit to the \pounds reinforcement.

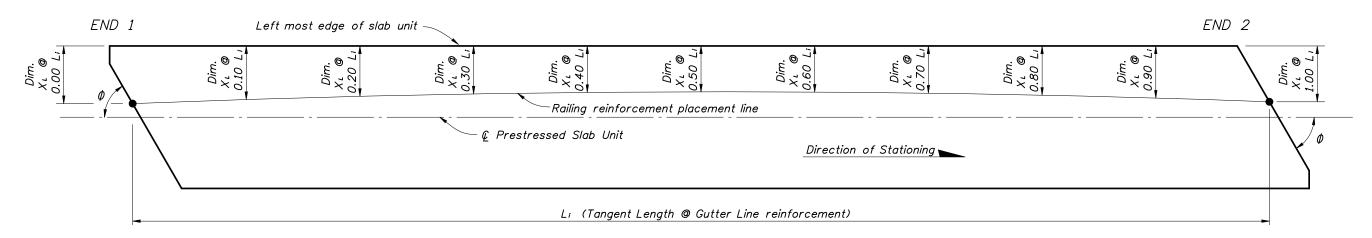
			B UNITS ING LAYI				Table Dat 1-01-09						
Span No.													
Slab Unit No.													
Railing Index No.													
Bar Mark (Mod.)													
Dim. Lı					1								
Dim. X LOCATION (Left Edge Offset to Railing Reinforcement)													
Case (Drientation)													
0.00 L; (END 1)													
0.10 L i													
0.20 Li													
0.30 L;													
0.40 Li													
0.50 L;													
0.60 L;													
0.70 Li													
0.80 Li													
0.90 Li													
1.00 L; (END 2)													

NOTES:

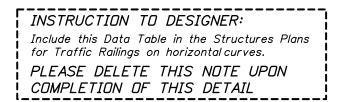
Work this Table with Index No. 20350, Sheet 2 and the Prestressed Slab Unit – Table of Variables in the Structures Plans.

Dim. X_L is measured perpendicular from the left most edge of the slab unit (looking from END 1 towards END 2) to the vertical leg of the Traffic Railing reinforcement.

See Index No. 20350, Sheet 2 for treatment of the Railing and Parapet reinforcement and Case "Left" or "Right" placement orientation of the modified railing bars.



SCHEMATIC PLAN VIEW OF MODIFIED RAILING REINFORCEMENT PLACEMENT



		ERLAY & FOR PRE			TA TABLE UNITS	Table Do	ate 7-01-09				DEFLEC		ATA TABLE UNITS	Table D	ate 7-01-09		OVI	ERLAY FOR PI
LOC	A <i>TION</i>		RED THEOR IVERLAY D SLAB UN	NN	NET BEAM CAMBER (PRESTRESS	DEAD LOAD DEFLECTION DURING	OVERLAY	LOCA	A <i>TION</i>		RED THEOR OVERLAY O SLAB UNI	NN	NET BEAM CAMBER (PRESTRESS	DEAD LOAD DEFLECTION DURING	 OVERLAY	LOC	ATION	REQ
SPAN ND.	SLAB UNIT ND.	AT BEGIN SPAN DIM "B"	SPAÑ	AT END SPAN DIM "D"	- DEAD LOAD DF SLAB UNIT) @ 120 DAYS	POUR	CASE ND.	SPAN ND.	SLAB UNIT ND.	AT BEGIN SPAN DIM "B"	SPAN	AT END SPAN DIM "D"	- DEAD LOAD DF SLAB UNIT) @ 120 DAYS	POUR @ 120 DAYS	CASE ND.	SPAN ND.	SLAB UNIT ND.	AT BEG SPAN DIM "E
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Q.		את אחדי	TA TABLE			
					Table Da	te 7-01-09
'RE	STRESSE	ED SLAB	UNITS			
	RED THEOR		NET BEAM	DEAD	LOAD	
	VERLAY D		CAMBER		ECTION	
C	SLAB UNI	T	(PRESTRESS	וטס	RING	OVERLAY
			- DEAD LOAD		RLAY	CASE
SIN	AT Ç	AT END				
			OF		JUR	ND.
/ 9''	SPAÑ	SPAN	SLAB UNIT)	@ 120) DAYS	
3"	DIM "C"	DIM "D"	@ 120 DAYS	עז מ	/ ''A''	
			WIZU DAIS		A	
						├─────┨
						<u> </u>
				I		

NDTE: Work this sheet with Design Standard Index No. 20399.

CDNCF			DATA TAB		le Date 7-01-06							
TYPE (See Detail A)	NUMBER REQUIRED	(Ft.)	T (In.)	(Ft.)	Ø (Degrees)							
NOTE:												
Work Concrete Sheet Pile Data Table with Standard Index No. 20400.												

BEA	RING PAD DA	TA TABL	Ε	Table L	Date 1-01-08
SPAN ND(s).	BEAM ND(s).	PAD TYPE	BEAM TYPE		BEAM END *

	D BEARING P ANTITIES	PAD
PAD TYPE	NUMBER REQUIRED	QU

NDTE:

Work this table with Index No. 20500 for Pad Types A, B & C and/or any project specific bearing pads.

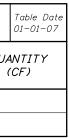
* END 1 = Begin Bridge end of beam (Back station).
 END 2 = End Bridge end of beam (Ahead station).

INSTRUCTIONS TO DESIGNER:

This table is intended for use with prestressed beam bridges, but may be modified

for steel girder or other bridge types. Supplement the BEARING PAD DATA TABLE with additional columns or notes as required to clearly identify the location and type of bearing pads.

PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING



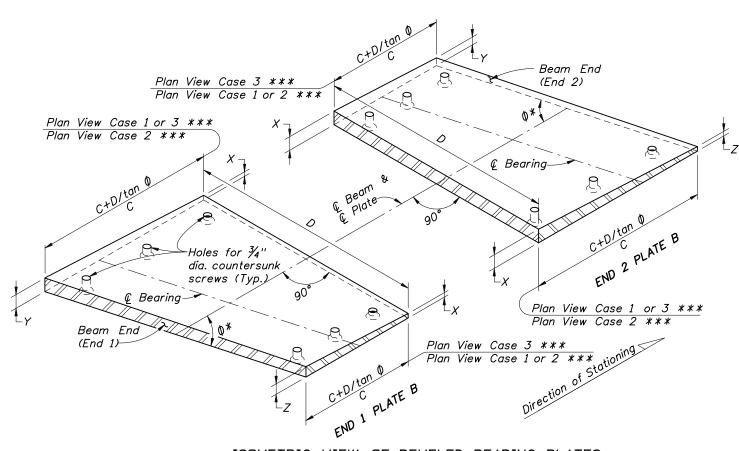
						BEAR	RING P	LATE	DATA T	TABLE						Table Date	e 1-01-08		
	GENE	RAL BEAR	RING PL	ATE D	ATA				IBEDDED		BEVELED	В	EVELED	PLATE DIMEN		(PLATE	B)		
BRG. PLATE	SPAN	BEAM	PAD	BEAM	PLAN VIEW	SLOPE	ANGLE			(in shan)			(inches)						
MARK ***	ND(s).	ND(s).	TYPE	END	CASE	(%) **	Ø *	С	D	C+D/TAN Ø	(Yes/No)	С	D	C+D/TAN Ø	X	Y	Z		

NOTES:

 ϕ = Acute angle (\leq 90°) measured from left or right side of ϕ Beam as required. *

** Slope measured along Q of Beam at Q of Bearing.
 *** See "TABLE OF BEAM VARIABLES" and Index No. 20110.

See Index No. 20501 for additional notes and details.



ISOMETRIC VIEW OF BEVELED BEARING PLATES (SKEWED PLATES SHOWN, NON-SKEWED PLATES SIMILAR)

INSTRUCTIONS TO DESIGNER:

requires decimal units and correct sign convention:

END 1

	END E X = Y = END E X =	ELEVA 0.5" Z = ELEVA	ATION + ((0.5(ATION 0''	ום <i>כ</i> י כ) x ייסל וםכי ו	Sloj NDI :	be TIO
	END E X = Y = Z = END E X =	LEVA 0.5" 0.50 0.5" ELEVA 0.50 0.5"	ATION + (0 0'' + (1 ATION 0'' - (0	, CD C + C / C CD C +	D tan NDI D	φ ΤΙΟ / 1
	END E X = Y = Z = END E X = Y =	ELEVA 0.5" 0.5" 0.50 ELEVA	ATION + ((+ () 0'' ATION 0'' - ((ו כם כ + ס / ו כם כ) x	NDI D tan NDI Sloj	γ φ TID pe
PLEASE	DEL	ETE	TH.	IS I	NDT	ΤE

1. Fill in the table to correspond with data on the 'TABLE OF BEAM VARIABLES' using inch units for Beveled Plate dimensions 'X', 'Y' & 'Z' rounded to $\frac{1}{16}$ th of an inch. 2. Use the following equations to determine the Beveled Plate thicknesses for 'PLAN VIEW CASES' and 'END ELEVATION CONDITIONS' corresponding to those shown on Design Standards Index No. 20110. The Slope parameter in these equations END 2 DN 1 or 2 (Positive Slope) X = 0.500'' $Y = Z = 0.5'' + (C) \times Slope$ DN 3 (Negative Slope) $X = 0.5'' - (C) \times Slope$ Y = Z = 0.500''Slope DN 1 or 2 (Positive Slope) $tan \phi$ x Slope X = 0.500" $Y = 0.5'' + (C) \times Slope$ $Z = 0.5'' + (C + D / tan \phi) \times Slope$) x Slope ON 3 (Negative Slope) $\dot{X} = 0.5'' - (C + D / tan \phi) \times Slope$ $Y = 0.5'' - (D / tan \phi) \times Slope$ tan Φ) x Slope Z = 0.500''DN 1 or 2 (Positive Slope) $tan \phi$) x Slope X = 0.500" $Y = 0.5'' + (C + D / tan \phi) \times Slope$) x Slope $Z = 0.5'' + (C) \times Slope$ DN 3 (Negative Slope) $\dot{X} = 0.5'' - (C + D / tan \phi) \times Slope$ Y = 0.500'' $tan \phi$ x Slope $Z = 0.5'' - (D / tan \phi)$ x Slope UPON COMPLETION OF THIS DRAWING

		GENERA	BEARING	PIAT	F DAT	1		ĺ		ATA T.	D PLATE							<u> </u>	
BRG. PLATE	SPAN	BEAM	BEARING		PLAN	CROSS	SLOPE	ANGLE			(PLATE A)	BEVELED PLATE REQUIRED	E	BEVELED	PLATE DIMEI (inche		(PLATE	B)	
MARK ***		ND(s).	TYPE	END		SLOPE (%) ##	1111 44	Ø *	С	D	C+D/TAN Ø	1 ~ 1	С	D	C+D/TAN Ø	W	X	Y	Z
					-					-									-
		View Ca 3 ***	<u>se 3 **:</u> se 1 or 2 X _{Left}	***	eft Plat	Wieft	YL 90°	eft 90°	Peam Ei End 2)		LY RI	ant Paring		Right					
	C+D/ton C	dia. co	for ¾" puntersunk s (Typ.)	0	3'ope	Beom E Single	plate		ight Right	Plate —	WRight	END 2 PLA C 2 PLA END 2 Bear (Double Bear Single	TES B ing simili ting	ar) Ini					
		The second se	0*	90°	Bearir	ng e	W			(Plan View C Plan View C	ase i or 5 4	***						
Lγ (E	am End nd 1)	~~		~ ~			Plan V	iew Case	3 ***	*	oning								

ISOMETRIC VIEW OF BEVELED BEARING PLATES FOR FLORIDA U-BEAMS (SKEWED PLATES SHOWN, NON-SKEWED PLATES SIMILAR)

ER (PART 1): with data on the 'TABLE OF BEAM VARIABLES' using inch units N', 'X', 'Y' & 'Z' rounded to $\frac{1}{16}$ th of an inch. slope perpendicular to Q of beam from End 1 and End 2, for the ith superelevation transitions. determine the Beveled Plate thicknesses for 'PLAN VIEW CASES' and corresponding to those shown on Design Standards Index No. 20210, beneath the beam ends. For split pedestals beneath double estal elevation to utilize the same thickness bearing plate on the m as shown in paragraphs (i) and (ii) below. Slope and Cross Slope require decimal units and correct sign convention: END 2 v): 1 (Positive Slope) Bearing & Left Side Double Bearing (D) x Cross Slope W = 0.5'' + (D) x Cross Slope X = 0.5'' $Y = 0.5'' + (C) \times Slope$ $Z = 0.5'' + (C) \times Slope + (D) \times Cross Slope$ ope le Bearing & Right Side Double Bearing W = 0.5''X = 0.5'' - (D) x Cross Slope (D) x Cross Slope $Y = 0.5'' + (C) \times Slope - (D) \times Cross Slope$ ope $Z = 0.5'' + (C) \times Slope$ Side Double Bearing $(2D+E) \times Cross \ Slope \quad W = 0.5'' + (2D+E) \times Cross \ Slope$ (D+E) x Cross Slope $X = 0.5'' + (D+E) \times Cross Slope$ $Y = 0.5'' + (C) \times Slope + (D+E) \times Cross Slope$ Slope $Z = 0.5'' + (C) \times Slope + (2D+E) \times Cross Slope$ s Slope Side Double Bearing (D+E) x Cross Slope $W = 0.5'' - (D+E) \times Cross Slope$ $\begin{array}{l} x = 0.5" - (D+E) \times Cross Slope \\ X = 0.5" - (2D+E) \times Cross Slope \\ Y = 0.5" + (C) \times Slope - (2D+E) \times Cross Slope \\ Z = 0.5" + (C) \times Slope - (D+E) \times Cross Slope \end{array}$ (2D+E) x Cross Slope s Slope Slope 3 (Negative Slope) Bearing & Left Side Double Bearing lope W = 0.5" - (C) x Slope + (D) x Cross Slope $X = 0.5'' - (C) \times Slope$ Y = 0.5''(D) x Cross Slope $Z = 0.5'' + (D) \times Cross Slope$ le Bearing & Right Side Double Bearing W = 0.5'' - (C) x Slope $X = 0.5'' - (C) \times Slope - (D) \times Cross Slope$ ne $Y = 0.5'' - (D) \times Cross Slope$ (D) x Cross Slope Z = 0.5''Side Double Bearing $W = 0.5'' - (C) \times Slope + (2D+E) \times Cross Slope$ s Slope $X = 0.5'' - (C) \times Slope + (D+E) \times Cross Slope$ Slope $Y = 0.5'' + (D+E) \times Cross Slope$ (D+E) x Cross Slope (2D+E) x Cross Slope $Z = 0.5'' + (2D+E) \times Cross Slope$ Side Double Bearing Slope $W = 0.5'' - (C) \times Slope - (D+E) \times Cross Slope$ $X = 0.5'' - (C) \times Slope - (2D+E) \times Cross Slope$ Slope $Y = 0.5'' - (2D+E) \times Cross Slope$ (2D+E) x Cross Slope (D+E) x Cross Slope $Z = 0.5'' - (D+E) \times Cross Slope$ E UPON COMPLETION OF THIS DRAWING

INSTRUCTIONS TO DESIGNER (PART 2):

END 1

(II) PLAN VIEW CASE 2:

END 2

(a) END ELEVATION CONDITION 1 OR 2 (Positive Slope) (i) Positive Cross Slope, Single Bearing & Left Side Double Bearing $W = 0.5'' + (C+D/tan \phi) \times Slope + (D) \times Cross Slope$ $W = 0.5'' + (D) \times Cross Slope$ $X = 0.5'' + (C+D/tan \phi) \times Slope$ X = 0.5''Y = 0.5'' $Y = 0.5'' + (C) \times Slope$ $Z = 0.5'' + (D/tan \phi) \times Slope + (D) \times Cross Slope$ $Z = 0.5'' + (C+D/tan \phi) \times Slope + (D) \times Cross Slope$ (ii) Negative Cross Slope, Single Bearing & Right Side Double Bearing $W = 0.5'' + (C) \times Slope$ W = 0.5'' $X = 0.5'' + (C) \times Slope - (D) \times Cross Slope$ $X = 0.5'' - (D) \times Cross Slope$ ** $Y = 0.5'' - (D/tan \phi) \times Slope - (D) \times Cross Slope$ $Y = 0.5'' + (C) \times Slope - (D) \times Cross Slope$ Z = 0.5'' $Z = 0.5'' + (C+D/tan \phi) \times Slope$ (iii) Positive Cross Slope, Right Side Double Bearing $W = 0.5'' + [(2D+E)/tan \phi + C] \times Slope + (2D+E) \times Cross Slope$ $W = 0.5'' + (D+E)/tan \phi x Slope + (2D+E) x Cross Slope$ $X = 0.5'' + [(2D+E)/tan \phi + C] \times Slope + (D+E) \times Cross Slope$ $X = 0.5'' + (D+E)/tan \phi \times Slope + (D+E) \times Cross Slope$ $Y = 0.5'' + (D+E)/tan \phi x Slope + (D+E) x Cross Slope$ $Y = 0.5'' + [(D+E)/tan \phi + C] \times Slope + (D+E) \times Cross Slope$ $Z = 0.5'' + (2D+E)/tan \phi \times Slope + (2D+E) \times Cross Slope$ $Z = 0.5'' + [(2D+E)/tan \phi + C] \times Slope + (2D+E) \times Cross Slope$ (iv) Negative Cross Slope, Left Side Double Bearing W = 0.5" + [C - (D+E)/tan @] x Slope - (D+E) x Cross Slope ** W = 0.5" - (D+E)/tan @ x Slope - (D+E) x Cross Slope X = 0.5" + [C - (D+E)/tan Ø] x Slope - (2D+E) x Cross Slope ** X = 0.5" - (D+E)/tan Ø x Slope - (2D+E) x Cross Slope ** $Y = 0.5'' - (2D+E)/tan \phi x$ Slope - (2D+E) x Cross Slope $Y = 0.5'' + [C - (D+E)/tan \phi] \times Slope - (2D+E) \times Cross Slope$ ** $Z = 0.5'' - (D+E)/tan \phi \times Slope - (D+E) \times Cross Slope$ Z = 0.5'' + [C - E/tan] x Slope - (D+E) x Cross Slope(b) END ELEVATION CONDITION 3 (Negative Slope) (i) Positive Cross Slope, Single Bearing & Left Side Double Bearing $W = 0.5'' + (D) \times Cross Slope$ $W = 0.5'' - (C) \times Slope + (D) \times Cross Slope$ $X = 0.5'' - (C) \times Slope$ X = 0.5'' $Y = 0.5'' - (C+D/tan \phi) \times Slope$ Y = 0.5'' $Z = 0.5'' - (C) \times Slope + (D) \times Cross Slope$ ** $Z = 0.5'' + (D/tan \phi) \times Slope + (D) \times Cross Slope$ (ii) Negative Cross Slope, Single Bearing & Right Side Double Bearing $W = 0.5'' - (C+D/tan \phi) \times Slope$ W = 0.5'' $X = 0.5'' - (D) \times Cross Slope$ $X = 0.5'' - (C+D/tan \phi) \times Slope - (D) \times Cross Slope$ $Y = 0.5'' - (C+D/tan \phi) \times Slope - (D) \times Cross Slope$ $Y = 0.5'' - (D/tan \phi) \times Slope - (D) \times Cross Slope$ $Z = 0.5'' - (C) \times Slope$ Z = 0.5''(iii) Positive Cross Slope, Right Side Double Bearing ** $W = 0.5'' + (D+E)/tan \phi x Slope + (2D+E) x Cross Slope$ $W = 0.5'' - [C - (D+E)/tan \phi] \times Slope + (2D+E) \times Cross Slope$ ** $X = 0.5'' + (D+E)/tan \phi \times Slope + (D+E) \times Cross Slope$ $X = 0.5'' - [C - (D+E)/tan \phi] \times Slope + (D+E) \times Cross Slope$ $Y = 0.5'' - [C-E/tan 0] \times Slope + (D+E) \times Cross Slope$ ** Y = 0.5" + (D+E)/tan Ø x Slope + (D+E) x Cross Slope Z = 0.5" - [C - (D+E)/tan \$\overline{d}]x Slope + (2D+E)x Cross Slope ** Z = 0.5" + (2D+E)/tan \$\overline{d} x Slope + (2D+E)x Cross Slope (iv) Negative Cross Slope, Left Side Double Bearing $W = 0.5'' - (D+E)/tan \phi x Slope - (D+E) x Cross Slope$ $W = 0.5'' - [C + (2D+E)/tan \Phi] \times Slope - (D+E) \times Cross Slope$ $X = 0.5'' - (D+E)/tan \phi \times Slope - (2D+E) \times Cross Slope$ $X = 0.5'' - [C + (2D+E)/tan \phi] \times Slope - (2D+E) \times Cross Slope$ Y = 0.5" - (2D+E)/tan ϕ x Slope - (2D+E) x Cross Slope $Y = 0.5'' - [C + (2D+E)/tan \phi] \times Slope - (2D+E) \times Cross Slope$ $Z = 0.5'' - [C + (D+E)/tan \phi] \times Slope - (D+E) \times Cross Slope$ $Z = 0.5'' - (D+E)/tan \phi \times Slope - (D+E) \times Cross Slope$ ** Could be less than 0.5" for steep slopes. Adjust plate thickness equally at all corners of both left and right side plates to provide a minimum 0.5" thickness.

PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING

END 1 (III) PLAN VIEW CASE 3: (a) END ELEVATION CONDITION 1 OR 2 (Positive Slope) (i) Positive Cross Slope, Single Bearing & Left Side Double Bearing $W = 0.5'' + (C) \times Slope + (D) \times Cross Slope$ $X = 0.5'' + (C) \times Slope$ Y = 0.5'' $** Z = 0.5'' - (D/tan \phi) \times Slope + (D) \times Cross Slope$ (ii) Negative Cross Slope, Single Bearing & Right Side Double Bea $W = 0.5'' + (C+D/tan \phi) \times Slope$ $X = 0.5'' + (C+D/tan \phi) \times Slope - (D) \times Cross Slope$ $Y = 0.5'' - (D/tan \phi) \times Slope - (D) \times Cross Slope$ Z = 0.5''(iii) Positive Cross Slope, Right Side Double Bearing $W = 0.5'' + [C - (D+E)/tan \phi] \times Slope + (2D+E) \times Cross$ $X = 0.5'' + [C - (D+E)/tan \phi] \times Slope + (D+E) \times Cross Sl$ ** Y = $0.5'' - (D+E)/tan \phi \times Slope + (D+E) \times Cross Slope$ ** $Z = 0.5'' - (2D+E)/tan \phi \times Slope + (2D+E) \times Cross Slope$ (iv) Negative Cross Slope, Left Side Double Bearing $W = 0.5'' + [C + (2D+E)/tan @] \times Slope - (D+E) \times Cross$ $X = 0.5'' + [C + (2D+E)/tan \emptyset] \times Slope - (2D+E) \times Cross$ Y = 0.5" + (2D+E)/tan Ø x Slope - (2D+E) x Cross Slope $Z = 0.5'' + (D+E)/tan \phi \times Slope - (D+E) \times Cross Slope$ (b) END ELEVATION CONDITION 3 (Negative Slope) (i) Positive Cross Slope, Single Bearing & Left Side Double Beari $W = 0.5'' + (D) \times Cross Slope$ X = 0.5'' $Y = 0.5'' - (C) \times Slope$ $Z = 0.5'' - [C+D/tan \phi] \times Slope + (D) \times Cross Slope$ (ii) Negative Cross Slope, Single Bearing & Right Side Double Bea W = 0.5'' $X = 0.5'' - (D) \times Cross Slope$ $Y = 0.5'' - (C) \times Slope - (D) \times Cross Slope$ $Z = 0.5'' - (C+D/tan \theta) \times Slope$ (iii) Positive Cross Slope, Right Side Double Bearing $W = 0.5'' - (D+E)/tan \phi x$ Slope + (2D+E) x Cross Slope $X = 0.5'' - (D+E)/tan \phi \times Slope + (D+E) \times Cross Slope$ $Y = 0.5'' - [C + (D+E)/tan 0] \times Slope + (D+E) \times Cross Sl$ $Z = 0.5'' - [C + (2D+E)/tan \phi] \times Slope + (2D+E) \times Cross$ (iv) Negative Cross Slope, Left Side Double Bearing ** $W = 0.5'' + (D+E)/tan \phi x Slope - (D+E) x Cross Slope$ ** $X = 0.5'' + (D+E)/tan \phi \times Slope - (2D+E) \times Cross Slope$ Y = 0.5" - [C - (D+E)/tan ØJ x Slope - (2D+E) x Cross S $Z = 0.5'' - [C - (E)/tan \phi] \times Slope - (D+E) \times Cross Slope$ ****** Could be less than 0.5" for steep slopes. Adjust plate thickness

minimum 0.5" thickness.

INSTRUCTIONS TO DESIGNER (PART 3):

<u>END 2</u>

ring W = 0.5" + (D) x Cross Slope X = 0.5" Y = 0.5" + (C+D/tan Φ) x Slope Z = 0.5" + (C) x Slope + (D) x Cross Slope	
earing W = 0.5" X = 0.5" - (D) x Cross Slope Y = 0.5" + (C+D/tan Ø) - (D) x Cross Slope Z = 0.5" + (C) x Slope	
s Slope ** W = 0.5'' - (D+E)/tan Ø x Slope + (2D+E) x Cross Slope Slope ** X = 0.5'' - (D+E)/tan Ø x Slope + (D+E) x Cross Slope Y = 0.5'' + (C-E/tan Ø] x Slope + (D+E) x Cross Slope e Z = 0.5'' + [C - (D+E)/tan Ø] x Slope + (2D+E) x Cross Slope	
Slope $W = 0.5'' + (D+E)/tan \phi x Slope - (D+E) x Cross Slope$ s Slope $X = 0.5'' + (D+E)/tan \phi x Slope - (2D+E) x Cross Slope$ $Y = 0.5'' + [C + (2D+E)/tan \phi] x Slope - (2D+E) x Cross Slope$ $Z = 0.5'' + [C + (D+E)/tan \phi] x Slope - (D+E) x Cross Slope$	
ring W = 0.5" - (C+D/tan Ø) x Slope + (D) x Cross Slope X = 0.5" - (C+D/tan Ø) x Slope Y = 0.5" Z = 0.5" - (D/tan Ø) x Slope + (D) x Cross Slope	
earing $W = 0.5'' - (C) \times Slope$ $X = 0.5'' - (C) \times Slope - (D) \times Cross Slope$ $Y = 0.5'' + (D/tan \phi) \times Slope - (D) \times Cross SlopeZ = 0.5''$	
W = 0.5" - [C + (2D+E)/tan Ø] x Slope + (2D+E) x Cross Slope X = 0.5" - [C + (2D+E)/tan Ø] x Slope + (D+E) x Cross Slope Slope Y = 0.5" - (D+E)/tan Ø x Slope + (D+E) x Cross Slope s Slope Z = 0.5" - (2D+E)/tan Ø x Slope + (2D+E) x Cross Slope	
W = 0.5" - [C - (D+E)/tan \$\vert J\$ x Slope - (D+E) x Cross Slope X = 0.5" - [C - (D+E)/tan \$\vert J\$ x Slope - (2D+E) x Cross Slope Slope ** Y = 0.5" + (2D+E)/tan \$\vert x Slope - (2D+E) x Cross Slope e ** Z = 0.5" + (D+E)/tan \$\vert x Slope - (D+E) x Cross Slope	
ss equally at all corners of both left and right side plates to provide a	

PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING

BEA	RING PAD DA	TA TABL	E	Table [Date 7-01-09
SPAN ND(s).	BEAM ND(s).	PAD TYPE	BEAM TYPE		BEAM END *

NDTE: Work this table with Index No. 20510 for Pad Types D, E, F, G, H, J & K, and/or any project specific bearing pads. * END 1 = Begin Bridge end of beam (Back station). END 2 = End Bridge end of beam (Ahead station).

INSTRUCTIONS TO DESIGNER:

This table is intended for use with prestressed beam bridges, but may be modified for steel girder or other bridge types. Supplement the BEARING PAD DATA TABLE with additional columns or notes as required to clearly identify the location and type of bearing pads.

PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING

ESTIMATEL QU/	Table Date 07-01-09			
PAD TYPE	NUMBER REQUIRED		NTITY CF)	

	BEARING PLATE DATA TABLE														Table Date 7-01-09		
	GENE	RAL BEAR	RING PL	LATE D	ATA			EMBEDDED PLATE DIMENSIONS (PLATE A)			BEVELED	B	EVELED	PLATE DIMEN	VSIDNS	PLATE I	3)
BRG. PLATE	SPAN	BEAM	PAD	BEAM	PLAN VIEW	SLOPE	ANGLE	E (inches)		PLATE REQUIRED			(inches	5)			
MARK ***	ND(s).	ND(s).	TYPE	END	CASE	(%) **		С	D	C+D/TAN Ø	(Yes/No)	С	D	C+D/TAN Ø	X	Y	Ζ

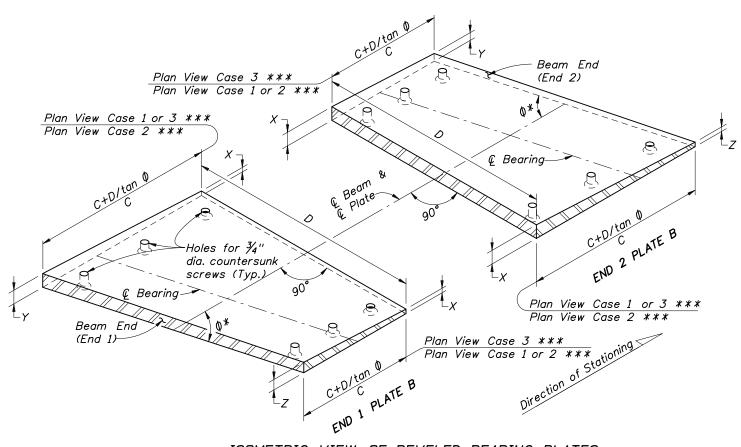
NOTES:

 ϕ = Acute angle (\leq 90°) measured from left or right side of ϕ Beam as required. *

** Slope measured along & of Beam at & of Bearing.

*** See "TABLE OF BEAM VARIABLES" and Index No. 20010.

See Index No. 20511 for additional notes and details.



ISOMETRIC VIEW OF BEVELED BEARING PLATES (SKEWED PLATES SHOWN, NON-SKEWED PLATES SIMILAR)

INSTRUCTIONS TO DESIGNER:

- requires decimal units and correct sign convention:

END 1

	END EL X = 0 Y = . END EL X = 0	LEVAT. D.5" + Z = C LEVAT. D.500"	ION CL (C) x 0.500'' ION CL	Slope
	END EL X = (Y = (Z = (END EL X = (Y = (LEVAT. 0.5'' + 0.500' 0.5'' + LEVAT. 0.500'' 0.5'' -	ION CL (C + (D / ION CL	NDITI D / tan (NDITI
	END EL X = (Y = (Z = (END EL X = (Y = (LEVAT. 0.5" + 0.500" 1.500" LEVAT. 0.500" 0.5" -	ION CL (C + (D / ION CL	NDITI D/ tan NDITI Slope
PLEASE	DELE	TE	THIS	ΝΟΤΙ

1. Fill in the table to correspond with data on the 'TABLE OF BEAM VARIABLES' using inch units for Beveled Plate dimensions 'X', 'Y' & 'Z' rounded to $\frac{1}{16}$ th of an inch. 2. Use the following equations to determine the Beveled Plate thicknesses for 'PLAN VIEW CASES' and 'END ELEVATION CONDITIONS' corresponding to those shown on Design Standards Index No. 20010. The Slope parameter in these equations

END 2

TIDN 1 or 2 (Positive Slope) X = 0.500''oe. $Y = Z = 0.5'' + (C) \times Slope$ IDN 3 (Negative Slope) $\dot{X} = 0.5'' - (C) \times Slope$ Y = Z = 0.500''Slope IDN 1 or 2 (Positive Slope) f tan ϕ) x Slope X = 0.500" $Y = 0.5'' + (C) \times Slope$ ϕ) x Slope $Z = 0.5'' + (C + D / tan \phi) \times Slope$ IDN 3 (Negative Slope) $\dot{X} = 0.5'' - (C + D / tan \phi) \times Slope$ tan Φ) x Slope Y = 0.5" - (D / tan Φ) x Slope Z = 0.500" e TIDN 1 or 2 (Positive Slope) $tan \phi$ x Slope X = 0.500" $Y = 0.5'' + (C + D / tan \phi) \times Slope$ Ø) x Slope $Z = 0.5'' + (C) \times Slope$ IDN 3 (Negative Slope) $X = 0.5'' - (C + D / tan \phi) \times Slope$ Y = 0.500'' $tan \phi$) x Slope $Z = 0.5'' - (D / tan \phi)$ x Slope

ASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING

	BEARING PLATE DATA TABLE												ible Date	7-01-10				
	GENI	ERAL BEA	RING PLATE			1	EMBEDDE DIMENSIONS		BEVELED PLATE	Б	BEVELE	D PLA		IENSIONS hes)	(PLATE	B)		
BRG. PLATE MARK ***	SPAN ND(s).	BEAM ND(s).	PAD BEA TYPE EN	M PLAN VIEW	/ , SLOPE _ (%) * *	ANGLE	(inc) G	hes) F	REQUIRED		D	E	F	W X	Y	Z		
				CASE			6	,					/			2		
NOTES:] CTIONS TO DESIGNER:	
*** See	"TABLE DI	BEAM V	of Beam c 'ARIABLES'' ionalnotes c	and Inde	x No. 20	010.		Y		am Eno	d	0			 2. 	Bevel Use the and ' The S For all o	The table to correspond with data on the 'TABLE DF we have to correspond with data on the 'TABLE DF we have to the second to the second to the second secon	n of an inch. thicknesses for 'PLAN VIEW CASES' s shown on Design Standards Index No. 20010. units and correct sign convention:
						E				F							END 1	<u>END 2</u>
Holes for ¾'' dia. countersur screws (Typ.)	k		X _	9	X			8. F Ç Beam & Ç Plate	0*			¢ Bea	\checkmark	ATEB		(a) E (b) E (II) PL, (a) E	Where VIEW CASE 1: END ELEVATION CONDITION 1 or 2 (Positive Slope) $W = X = 0.5'' + (C) \times Slope$ Y = Z = 0.5'' END ELEVATION CONDITION 1 or 3 (Negative Slope) W = X = 0.5'' $Y = Z = 0.5'' - (C) \times Slope$ AN VIEW CASE 2: END ELEVATION CONDITION 1 or 2 (Positive Slope) $W = 0.5'' + (C/sin \phi + D/tan \phi) \times Slope$	W = X = 0.5" Y = Z = 0.5" + (C) x Slope W = X = 0.5" - (C) x Slope Y = Z = 0.5" W = 0.5" + (D/tan Φ) x Slope
Y J	E			0*	F		£ Bearing	y rise	Direc	tion of	Stationin	19				(b) E	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{llllllllllllllllllllllllllllllllllll$
Skew Angle - Ø Skew Ang	\rightarrow	90°		Beam (End 1)	End		or Q	t Face of Bo Pier or Ben	rckwall t							(а) Е (Б) Е	LAN VIEW CASE 3: END ELEVATION CONDITION 1 or 2 (Positive Slope) $W = 0.5'' + (C/sin \ 0) \times Slope$ $X = 0.5'' + (D/tan \ 0) \times Slope$ $Z = 0.5'' + (D/tan \ 0) \times Slope$ END ELEVATION CONDITION 1 or 3 (Negative Slope) $W = 0.5'' - (D/tan \ 0) \times Slope$ X = 0.5'' $Y = 0.5'' - (C/sin \ 0) \times Slope$	$ \begin{array}{llllllllllllllllllllllllllllllllllll$
							ED BEARIN IOWN, NON-					BEAMS	5				$Z = 0.5'' - (C/sin \phi + D/tan \phi) \times Slope$ DELETE THIS NOTE UPON COMPLETION (2)	Z = 0.5" - (D/tan Ø) x Slope JF THIS DRAWING

	W = X = 0.5" Y = Z = 0.5" + (C) x Slope
gative Slope)	W = X = 0.5" - (C) x Slope Y = Z = 0.5"

sitive Slope)	
Slope	W = 0.5" + (D/tan Ø) x Slope X = 0.5"
	Y = 0.5" + (C/sin Φ) x Slope
	$Z = 0.5'' + (C/\sin \phi + D/\tan \phi) \times Slope$
gative Slope)	
	W = 0.5" - (C/sin Φ) x Slope
	$X = 0.5'' - (C/\sin \phi + D/\tan \phi) \times Slope$
Slope	$Y = 0.5'' - (D/tan \Phi) \times Slope$
1	Z = 0.5''

sitive Slope)	
Slope	W = 0.5'' X = 0.5'' + (D/tan Φ) x Slope Y = 0.5'' + (C/sin Φ + D/tan Φ) x Slope
gative Slope)	$Z = 0.5'' + (C/\sin \phi) \times Slope$
	W = 0.5" - (C/sin Ø + D/tan Ø) x Slope X = 0.5" - (C/sin Ø) x Slope Y = 0.5"
Slope	$Z = 0.5'' - (D/tan \phi) \times Slope$
MPLETION OF	THIS DRAWING

\sim INSTRUCTION TO DESIGNER. Change to "PILE ORDER LENGTH (ft.)" for projects without Test Piles \mathcal{M} Λ

								\frown													
								Ĥ	PILE DATA	TABLE											
		1	NSTALLATI	ION CRITE	RIA				DESIG	N CRITERI	4										
PIER or BENT NUMBER	PILE SIZE (in.)	NOMINAL BEARING RESISTANCE (tons)	TENSION RESISTANCE (tons)	MINIMUM TIP ELEVATION (ft.)	TEST PILE LENGTH (ft.)	REQUIRED JET ELEVATION (ft.)	FACTORED DESIGN LOAD (tons)	DDWN DRAG (tons)	DECISTANCE	NET SCDUR RESISTANCE (tons)	100– YEAR SCOUR ELE VATION (ft.)	LDNG TERM SCDUR ELEVATIDN (ft.)	RESISTANCE FACTOR-Ø	PILE 1	PILE 2	F					

PILE INSTALLATION NUTES:	EMBEDDED DATA COLLECTOR NOTE:
Contractor to verify location of all utilities prior to any pile driving.	Provide Embedded Data Collector (EDC) Instrumentation in all piles in accordance with Design Standard Index No. 20602.
Minimum Tip Elevation is required for lateral stability.	
When a required jetting elevation is shown, the jet shall be	
differ from those shown on the table, the Engineer shall be responsible	
for determination of the required driving resistance.	
No jetting will be allowed without the approval of the Engineer.	
The Contractor should not anticipate being allowed to jet piles	
below the 100-year scour elevation or required jet elevation, whichever is deeper.	INSTRUCTIONS TO DESIGNER:
At each Bent, pile driving is to commence at the center of the Bent and proceed outward.	Modify table and notes as required to accommodate the required number of piles, piers and/or bents, use of Test Piles and EDC
	Minimum Tip Elevation is required for lateral stability. When a required jetting elevation is shown, the jet shall be lowered to the elevation and continue to operate at this elevation until the pile driving is completed. If jetting or preforming elevations differ from those shown on the table, the Engineer shall be responsible for determination of the required driving resistance. No jetting will be allowed without the approval of the Engineer. The Contractor should not anticipate being allowed to jet piles below the 100-year scour elevation or required jet elevation, whichever is deeper. At each Bent, pile driving is to commence at the center of the Bent

and notes as required to accommodate the required iles, piers and/or bents, use of Test Piles and EDC instrumentation.

DO NOT INCLUDE THIS "INSTRUCTIONS TO DESIGNER" NOTE IN PLANS

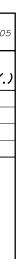
Table Date 7-01-1 PILE CUT-OFF ELEVATIONS PILE 3 PILE 4 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 4 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 4 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 4 PILE 5 PILE 6 PILE 7 PILE 8 PILE							
PILE CUT-OFF ELEVATIONS PILE 3 PILE 4 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 4 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 4 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 4 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 5 PILE 6 PILE 7 PILE 8 PILE PILE 3 PILE 5 PILE 6 PILE 7 PILE 8 PILE						Table Date	7-01-10
PILE 3 PILE 4 PILE 5 PILE 6 PILE 7 PILE 8 PILE	PILE CUT-OFF ELEVATIONS						
	PILE 3	PILE 4	ILE 4 PILE 5	PILE 6	PILE 7	PILE 8	PILE 9

IONS TO DESIGNER:

	ATION DIMENSIONS ANGLE O REINFORCING CLASS II L 1 L 2 M1 M2 N ANGLE O STEEL (Lbs.) CONCRETE (C.Y.		DIMENSIONS				SS II		
LOCATION	L 1	L 2	M1	M2	N	$ANGLE \varphi$	STEEL (Lbs.)	CONCRE	TE (C.Y.)
Dimension and Quantity Notes									

Quantities shown are for one Approach Slab and where applicable, raised sidewalks. Quantities do not include items placed on the slab such as Traffic Railing, Pedestrian/Bicycle Railings or Traffic Separators.

For Traffic Railing, Pedestrian/Bicycle Railing and Traffic Separator Quantities see Bid Item List.



		DIMENSIONS					REINFORCING	CLA
LOCATION	L 1	L 2	M1	M2	N	ANGLE Ø	STEEL (Lbs.)	CONCRE
Dimension and Quantity Notes: Dimensions 'L 1' & 'L 2' are Dimensions 'L 1' & 'L 2' are					parapet or	inside face	of railing on raised	sidewalks.
Quantities shown are for on placed on the slab such as							s do not include iter	ms
For Traffic Railing, Pedestria	n/Piavala	Dailing and	Traffic So	naratar Ou	antition on	a Rid Itama	list	



		STRIP SEAL EXI IN	PANSION JOII IDEX NO. 2110		LE			Table Date 7–
	TOTA	L DESIGN MOVEM	ENT	MOVEMENT	SKEW	ANGLE		DIM. "/
LOCATION	IN DIRECTION OF MOVEMENT	PERPENDICULAR TO & JOINT	PARALLEL TO & JOINT	ANGLE	LEFT SIDE	RIGHT SIDE	DIM. ''A'' @ 70°F	ADJUSTM PER 10
NATE:		·		•	•	•	•	•

NDTE: Dim. "A" adjustment per 10°F shown is measured perpendicular to & Expansion Joint. For theoretical direction of movement, see Index No. 21100, Sheet 2 of 3.

INSTRUCTIONS TO DESIGNER:
1. TotalDesign Movement shallbe the factored movement.
 2. Dimension "A" @ 70°F is normally set at 2" to accommodate installation of the neoprene seal and a total design movement up to 3". The designer should adjust Dimension "A" when necessary to account for skews or greater design movement with the following considerations: (a) the minimum joint opening in the direction of movement is ¹/₂" for the factored movement; (b) the maximum joint opening in the direction of travel is 4" for the factored movement;
3. Dimension "A" Adjustments for 10°F shallbe based on the unfactored movements.
PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING



POURED	Table Date 1-01-09					
LOCATION	DIM. ''A'' @ 70°F	TOTAL DESIGN MOVEMENT		" ADJUSTMENT ER 10°F		
NDTE: Dim. "A" adjustment per 10°F shown is measured perpendicular to Q Expansion Joint. Work this table with Design Standards Index No. 21110.						

INSTRUCTIONS TO DESIGNER: 1. Total Design Movement shall be the factored movement. 2. Dimension "A" @ 70°F is normally set at 2" for a total design movement up to 2" for non-skewed joints. The designer may reduce Dimension "A" when necessary to account for skews or smaller design movement with the following considerations: (a) the design joint opening (Dimension "A") should not be less than twice the joint contraction; (b) the minimum joint opening in the direction of movement is ½" for the factored movement; (c) the maximum joint opening in the direction of travelis 3" for the factored movement; (d) the minimum joint opening recommended by manufacturers at the time of installation is 1". 3. Dimension "A" Adjustments for 10°F shall be based on the unfactored movements. PLEASE DELETE THIS NOTE UPON COMPLETION OF THIS DRAWING

FEND	ER SYST	RILL OF MA EM - HEAN RDS INDEX	IY DUTY	Table Date 01–01–06
MARK	ND. REQ'D.	UNIT	QUANT	TITY
A1		MB		
A2		MB		
A3		MB		
A4		MB		
A5		MB		
A6		MB		
В		MB		
С		MB		
D		MB		
* E		MB		
F1		MB		
F2		MB		
F3		MB		
F4		MB		
F5		MB		
F6		MB		
G1		MB		
G2		MB		
H1		MB		
H2		MB		

FENDER SY TABLE OF VAI INDEX NO	RIABLES	able Date 01-01-06
CONTROL POINTS	STATION	OFFSET Lt. or Rt.
A		
В		
С		
D		
DIMENSION "L"		
CLEAR CHANNEL WIDTH		
CHANNEL SKEW ANGLE		
MHW or NHW ELEVATION		
MLW or NLW ELEVATION		
PILE CUTOFF ELEVATION		
MINIMUM PILE TIP ELEVATION LEFT FENDER		
PILE LENGTH LEFT FENDER		
MINIMUM PILE TIP ELEVATION RIGHT FENDER		
PILE LENGTH RIGHT FENDER		
NUMBER OF WALE ROWS		

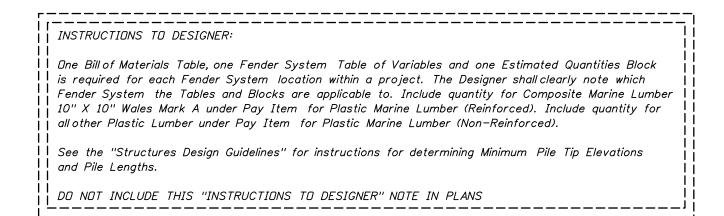
ESTIMATED QUANTITIES, INDEX	ND. 21910		Table Date 01-01-06
MARK	UNIT	Q	UANTITY
Plastic Marine Lumber (Reinforced)	MB		
Plastic Marine Lumber (Non-Reinforced)	MB		
Plastic Marine Composite Piles 16'' ϕ	LF		

NDTE: Estimated Quantities are for one entire fender system (left and right fenders).

NDTE: For Member Marks, Sizes and Dimensions see Design Standards Index No. 21910, Sheet 5.

Bill of Materials Table above is for an entire fender system (left and right fenders).

* Provide 2'-6" wide Fiberglass Open Grating for full length of fender in lieu of 2" X 12" Plastic Lumber when called for in Plans. Provide Stainless Steel Mounting Hardware and install per Manufacturer's recommendations. See Index Nos. 21900 & 21910 for notes. Include the cost of Fiberglass Open Grating and miscellaneous items required to install the grating in the price for Plastic Marine Lumber (Non-Reinforced).



NDTE: Work this Table with Design Standards Index Nos. 21900 and 21910.

FEND	ER SYST	BILL OF MA EM – MEDI NRDS INDEX		Table Date 01–01–06
MARK	ND. REQ'D.	UNIT	QUANT.	ΙΤΥ
A1		MB		
A2		MB		
A3		MB		
A4		MB		
A5		MB		
A6		MB		
В		MB		
С		MB		
D		MB		
* E		MB		
F1		MB		
F2		MB		
F3		MB		
F4		MB		
F5		MB		
F6		MB		
G1		MB		
G2		MB		
H1		MB		
H2		MB		

FENDER SY TABLE OF VAN INDEX NO. 2	RIABLES	able Date 1-01-06
CONTROL POINTS	STATION	DFFSET Lt. or Rt.
А		
В		
С		
D		
DIMENSION "L"		
CLEAR CHANNEL WIDTH		
CHANNEL SKEW ANGLE		
MHW or NHW ELEVATION		
MLW or NLW ELEVATION		
PILE CUTOFF ELEVATION		
MINIMUM PILE TIP ELEVATION LEFT FENDER		
PILE LENGTH LEFT FENDER		
MINIMUM PILE TIP ELEVATION RIGHT FENDER		
PILE LENGTH RIGHT FENDER		
NUMBER OF WALE ROWS		

NDTE: Work this Table with Design Standards Index Nos. 21900 and 21920.

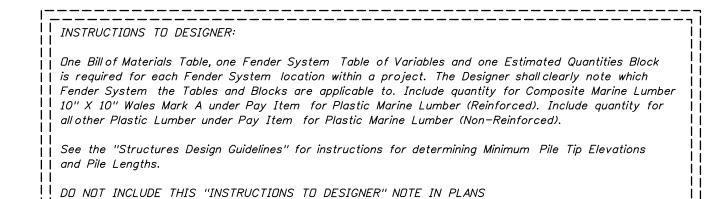
ESTIMATED QUANTITIES, INDEX NO. 21920			Table Date 01-01-06
MARK	UNIT	Q	UANTITY
Plastic Marine Lumber (Reinforced)	MB		
Plastic Marine Lumber (Non-Reinforced)	MB		
Plastic Marine Composite Piles 16'' Ø	LF		
NATE: Estimated Quantities are for one entire fender			

UIE: Estimated Quantities are for one entire fende system (left and right fenders).

NDTE: For Member Marks, Sizes and Dimensions see Design Standards Index No. 21920, Sheet 5.

Bill of Materials Table above is for an entire fender system (left and right fenders).

* Provide 2'-6" wide Fiberglass Open Grating for full length of fender in lieu of 2" X 12" Plastic Lumber when called for in Plans. Provide Stainless Steel Mounting Hardware and install per Manufacturer's recommendations. See Index Nos. 21900 & 21920 for notes. Include the cost of Fiberglass Open Grating and miscellaneous items required to install the grating in the price for Plastic Marine Lumber (Non-Reinforced).

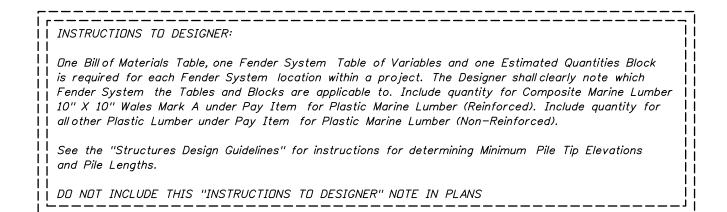


FEND	ESTIMATED BILL OF MATERIALS FENDER SYSTEM – LIGHT DUTY DESIGN STANDARDS INDEX NO. 21930				
MARK	ND. REQ'D.	UNIT	QUANT	ΊΤΥ	
A1		MB			
A2		MB			
A3		MB			
A4		MB			
A5		MB			
A6		MB			
В		MB			
С		MB			
D		MB			
* E		MB			
F1		MB			
F2		MB			
F3		MB			
F4		MB			
F5		MB			
F6		MB			
G1		MB			
G2		MB			
H1		MB			
H2		MB			

NDTE: For Member Marks, Sizes and Dimensions see Design Standards Index No. 21930, Sheet 5.

Bill of Materials Table above is for an entire fender system (left and right fenders).

* Provide 2'-6" wide Fiberglass Open Grating for full length of fender in lieu of 2" X 12" Plastic Lumber when called for in Plans. Provide Stainless Steel Mounting Hardware and install per Manufacturer's recommendations. See Index Nos. 21900 & 21930 for notes. Include the cost of Fiberglass Dpen Grating and miscellaneous items required to install the grating in the price for Plastic Marine Lumber (Non-Reinforced).



ן FENDER S
TABLE OF VA
INDEX NO.
CONTROL POINTS
А
В
С
D
DIMENSION "L"
CLEAR CHANNEL WIDTH
CHANNEL SKEW ANGLE
MHW or NHW ELEVATION
MLW or NLW ELEVATION
PILE CUTOFF ELEVATION
MINIMUM PILE TIP ELEVATION LEFT FENDER
PILE LENGTH LEFT FENDER
MINIMUM PILE TIP ELEVATION RIGHT FENDER
PILE LENGTH RIGHT FENDER
NUMBER OF WALE ROWS

ESTIMATED QUANTITIES, INDEX NO. 21930			Table Date 01-01-06
MARK	UNIT	Q	UANTITY
Plastic Marine Lumber (Reinforced)	MB		
Plastic Marine Lumber (Non-Reinforced)	MB		
14" Sq. Prestressed Concrete piles	LF		

NDTE: Estimated Quantities are for one entire fender system (left and right fenders).

4/	STEM RIABLES 21930	T C	able Date 1-01-06
s	STATION		DFFSET Lt. or Rt.
-			
'			
,			
1			

NDTE: Work this Table with Design Standards Index Nos. 21900 and 21930.