

# Application of Microbial Induced Calcite Precipitation (MICP) to Stabilize Florida High-Organic Matter Soils for Roadway Construction

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# Motivation

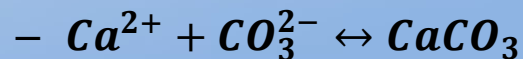
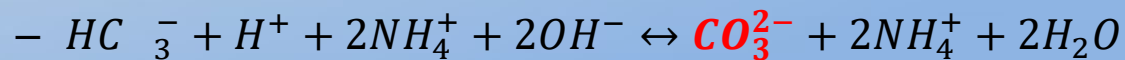
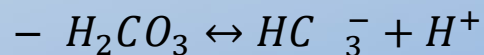
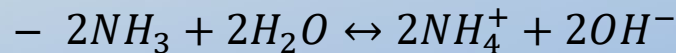
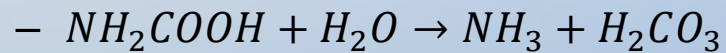
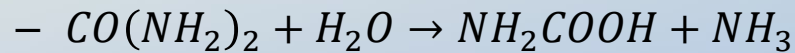
- High organic content (OC) soil needs to be stabilized and treated to mitigate settlement
- Previous studies/attempts
  - Surcharging – expensive (Wei et al. 1989)
  - Cut-and-replace – often expensive and not feasible (Mullins 1996)
  - Geogrids and geotextiles tied to cement stabilized columns – excessive differential settlements and column protrusions (Greene et al. 2013)
  - Soil mixing – expensive and causes creep (Mullins and Gunaratne 2014)
  - Dynamic replacement – effective at improving settlement and strength properties (Gunaratne et al. 1997)
  - Large amounts of binder (e.g., cement, lime kiln dust) may be necessary for high OC soil
  - Binder (lime kiln dust) may be a carcinogen (Button 2003)
- Need an effective, economically feasible, and sustainable solution!

# Objectives

- Determine Microbial Induced Calcite Precipitation (MICP) feasibility as an environmentally-friendly and sustainable method for treating Florida's OC soil for roadway construction
- Establish procedure to create/test MICP stabilized soil
- Determine procedure and optimal conditions for microbes to stabilize FL OC soil
- Recommendations and guidelines for field test site/application (e.g. pilot project)

# MICP – Governing Chemical Reactions

- Governing Reactions (Ureolytic Microbes):



# Treatment Setup



UF Treatment Cells

- Components:
  - Acrylic test cells that split down the middle
  - Peristaltic pump that pumps feed stock (urea & calcium chloride solution) to the specimens
  - Erlenmeyer flasks for effluent after feeding

# Generalized Treatment Procedure

1. Plate and grow bacteria (*Sporosarcina pasteurii*) using growth media (yeast, ammonium sulfate, and tris)
2. Autoclave fluid and add bacteria
3. Pump bacteria onto soil; wait so that bacteria have time to attach to soil particles
4. Feed bacteria every 6 of hours with nutrient broth (urea solution)

# Sand Treatments – Preliminary Testing

- 66 columns tested with varying conditions including different
  - pHs
  - Number of feed times
  - Bacteria strains
  - Pumping methods (top versus bottom of tube)
  - Grain sizes
  - Bacteria attachment times
  - Aeration
  - Bacteria concentrations/volumes
  - Initial growth media
- Once methodology had been determined, 14 additional columns treated for physical property testing

# Preliminary Testing – Lessons Learned

- Organism health/vitality appears to play a critical role cementation success
- Attachment time also appears to be critically important
- Aeration appeared to have little effect
- Four feedings per day produces more cementation than two feedings per day
- Much cementation/precipitation variability observed as a function of specimen height; thought to be the result of pore clogging



# Treated Sand – Selected Photographs

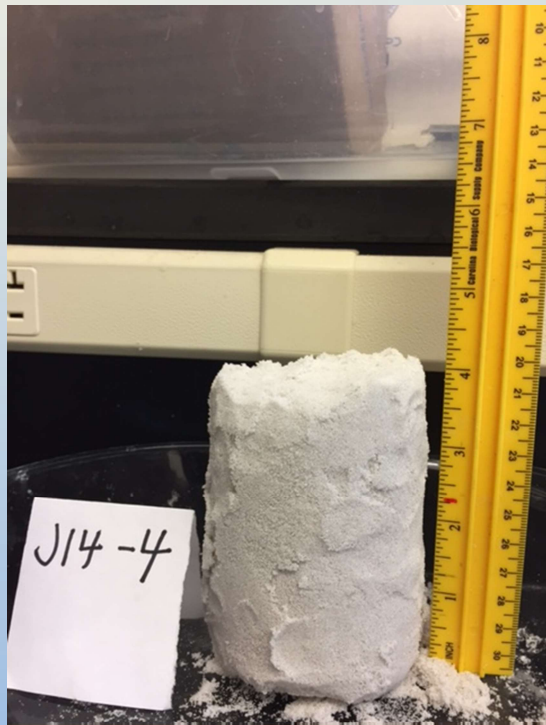
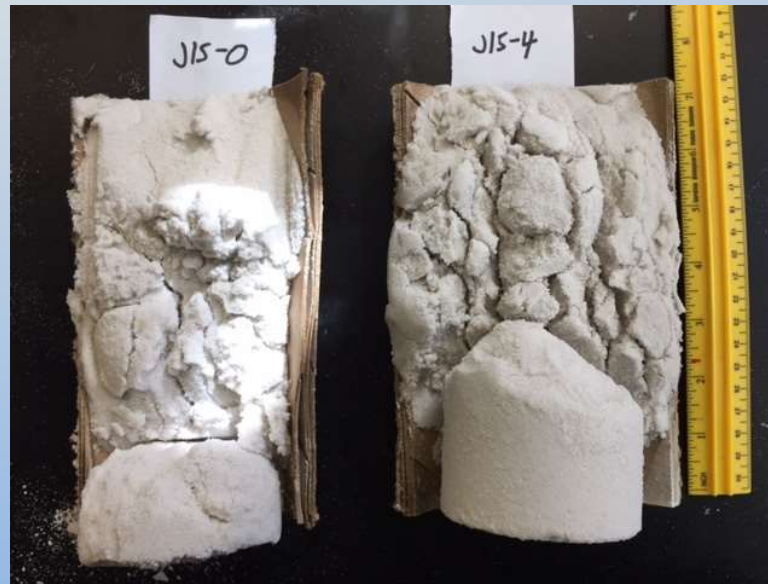
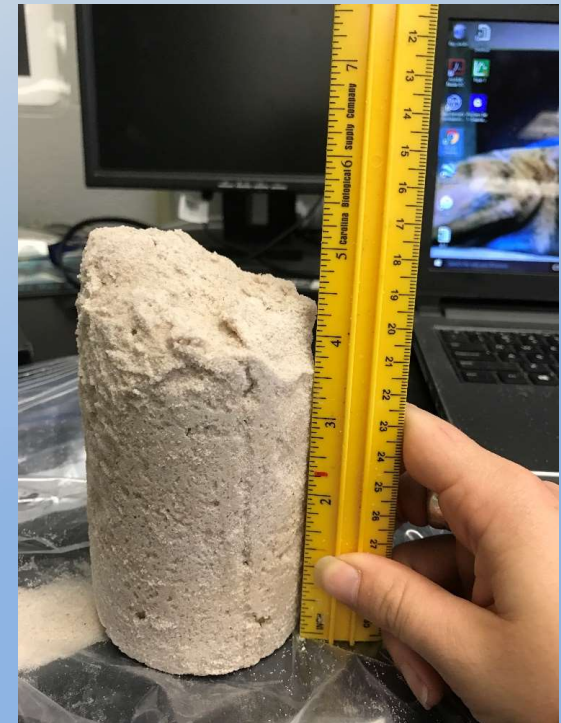


Figure 1-2. Specimen J14-4 after treatment

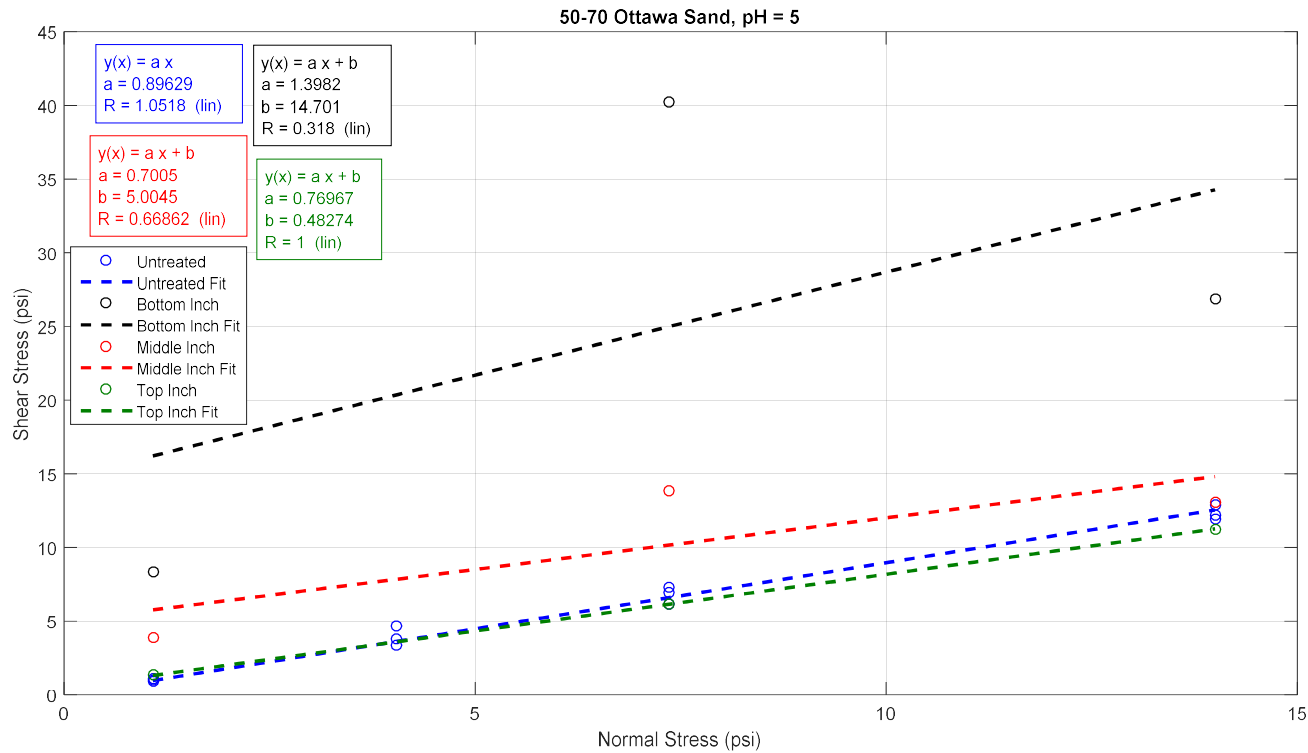


Specimens J15-0 and J15-4 after treatment



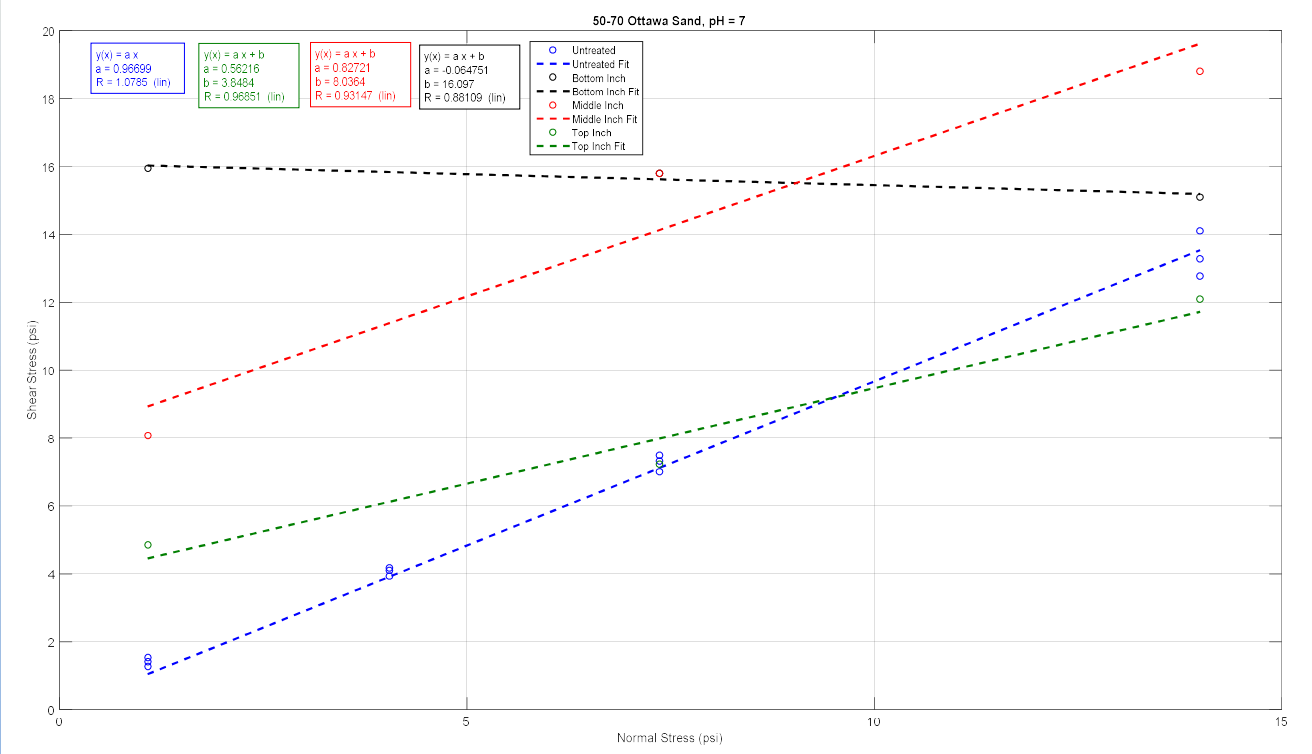
Specimen J11-X after treatment

# Direct Shear Test Results



Shear Stress vs. Normal Stress for 50-70 Ottawa Sand, pH = 5

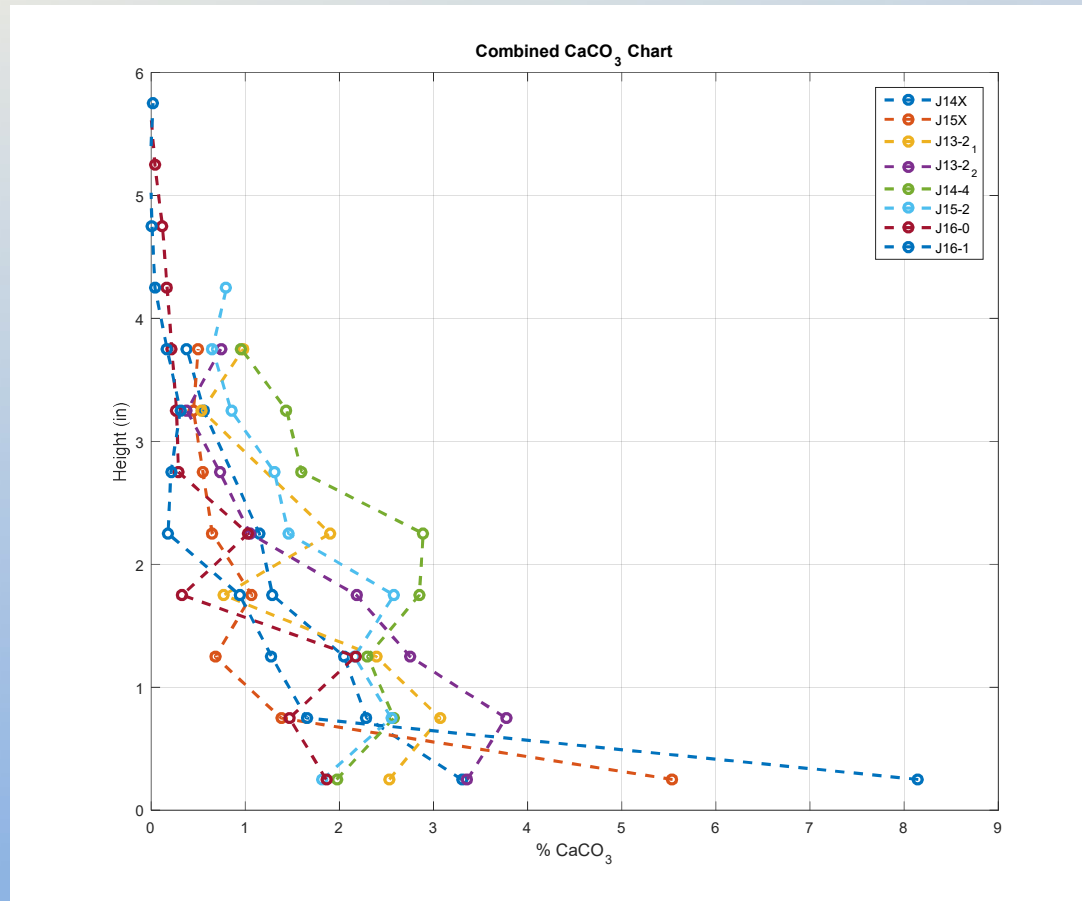
# Direct Shear Results



Shear Stress vs. Normal Stress for 50-70 Ottawa Sand, pH = 7



# Treated Sand – Variability in Precipitate



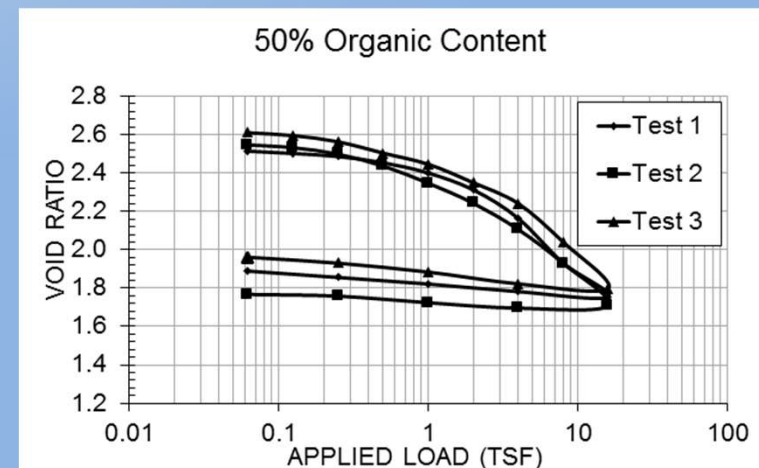
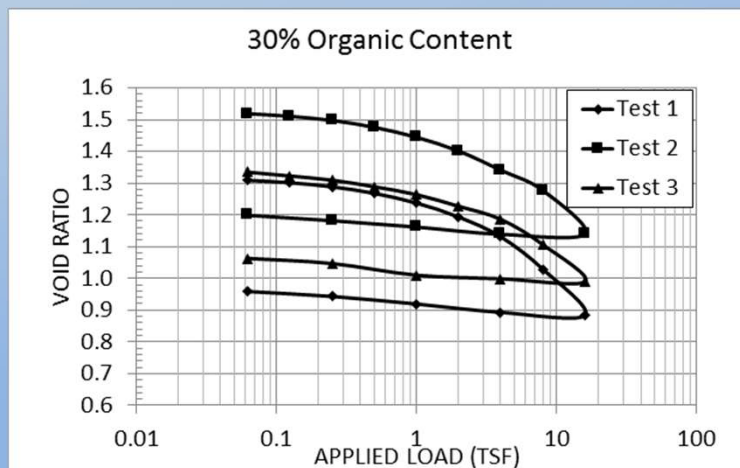
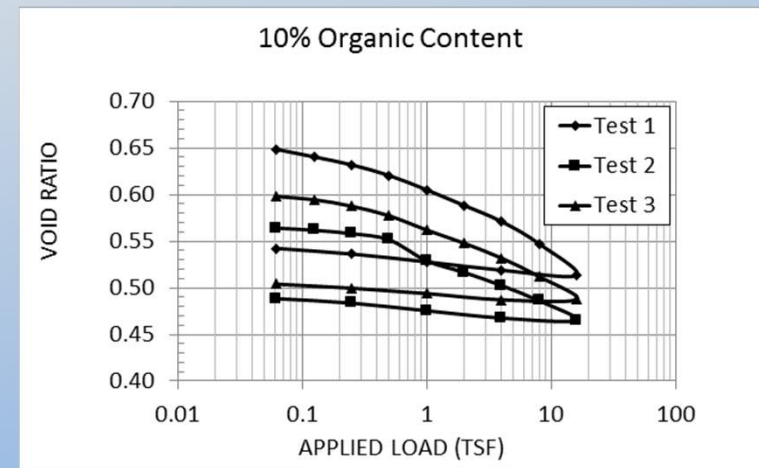
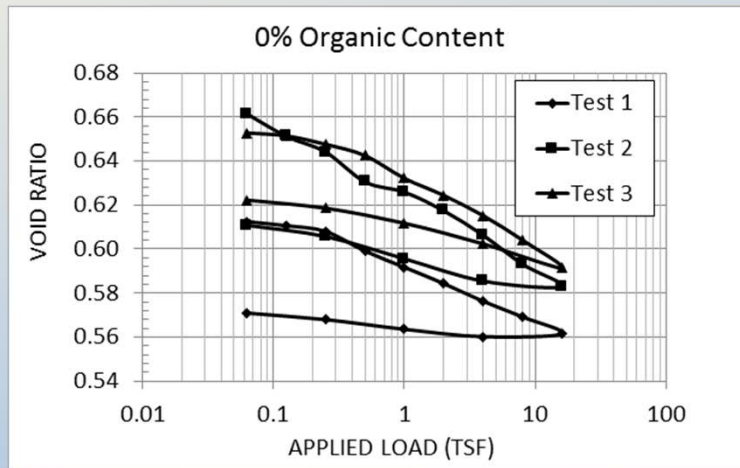
% CaCO<sub>3</sub> vs. Height for various sand specimens

- Maximum cementation at the bottom of specimens due to pore clogging
- After ~4 inches – very little cementation
- Need to examine physical property tests as a function of specimen height as well

# Preliminary Organic Treatment

- 27 Columns treated with OC varying 10% to 50%
- Results were inconsistent, although experimentation underway to address these issues.

# Consolidation: Untreated Soil



# Consolidation, Untreated Soil

| Property                 | 0% OC  |        |        | 10% OC |        |        | 30% OC |        |        | 50% OC |        |        |
|--------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
|                          | Test 1 | Test 2 | Test 3 | Test 1 | Test 2 | Test 3 | Test 1 | Test 2 | Test 3 | Test 1 | Test 2 | Test 3 |
| C <sub>c</sub>           | 0.025  | 0.040  | 0.037  | 0.095  | 0.062  | 0.066  | 0.41   | 0.334  | 0.326  | 0.679  | 0.659  | 0.738  |
| C <sub>r</sub>           | 0.007  | 0.017  | 0.017  | 0.014  | 0.013  | 0.011  | 0.042  | 0.036  | 0.018  | 0.059  | 0.0523 | 0.089  |
| e <sub>o</sub>           | 0.614  | 0.667  | 0.678  | 0.66   | 0.57   | 0.60   | 1.33   | 1.53   | 1.34   | 2.52   | 2.58   | 2.62   |
| w <sub>initial</sub> (%) | 9.2    | 9.7    | 10.05  | 24.7   | 30.5   | 31.3   | 67.8   | 67     | 68.9   | 88.9   | 87.8   | 89.3   |
| γ <sub>w</sub> (pcf)     | 111.49 | 109.69 | 108.07 | 97.9   | 108.6  | 106.9  | 84.0   | 78.1   | 84.2   | 57.2   | 56.0   | 56.1   |
| γ <sub>d</sub> (pcf)     | 102.10 | 99.99  | 98.20  | 78.5   | 83.3   | 81.4   | 50.1   | 46.8   | 49.9   | 30.3   | 29.8   | 29.6   |
| G <sub>s</sub>           | 2.64   |        |        | 2.09   |        |        | 1.87   |        |        | 1.71   |        |        |
| pH                       | 7      |        |        | 5      |        |        | 5      |        |        | 5      |        |        |

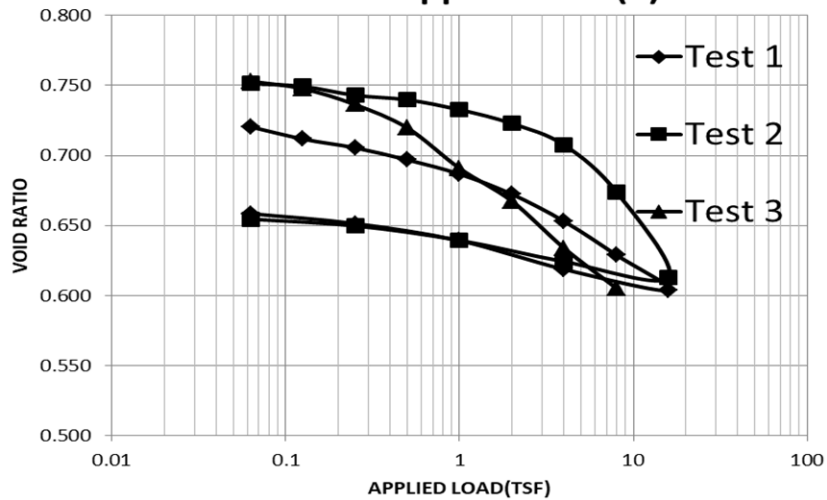
# Consolidation: Summary of Results, Untreated 50/70 Ottawa Sand

| Properties                           | Current Research (2017) | Simpson (2014) | Feng and Montoya (2014) | Lin et al. (2015) |
|--------------------------------------|-------------------------|----------------|-------------------------|-------------------|
| G <sub>s</sub>                       | 2.64                    | 2.65           | 2.65                    | 2.65              |
| D <sub>10</sub>                      | 0.21                    | 0.25           | N/A                     | 0.26              |
| D <sub>30</sub>                      | 0.25                    | 0.26           | N/A                     | 0.31              |
| D <sub>50</sub>                      | 0.27                    | 0.26           | 0.22                    | 0.44              |
| D <sub>60</sub>                      | 0.28                    | 0.27           | N/A                     | 0.37              |
| C <sub>U</sub>                       | 1.33                    | 1.07           | 1.40                    | 1.43              |
| C <sub>C</sub>                       | 1.06                    | 1.02           | 0.90                    | 1.01              |
| C <sub>C</sub> (Compression Index)   | 0.025, 0.025 (Test 1)   | 0.05           | 0.06                    | 0.024             |
|                                      | 0.040, 0.040 (Test 2)   |                |                         |                   |
|                                      | 0.037, 0.039 (Test 3)   |                |                         |                   |
| C <sub>R</sub> (Recompression Index) | 0.007, 0.007 (Test 1)   | 0.005          | 0.04                    | 0.0010            |
|                                      | 0.017, 0.017 (Test 2)   |                |                         |                   |
|                                      | 0.017, 0.015 (Test 3)   |                |                         |                   |
| Initial Void Ratio                   | 0.614 (Test 1)          | 0.66           | 0.75                    | 0.73              |
|                                      | 0.667 (Test 2)          |                |                         |                   |
|                                      | 0.678 (Test 3)          |                |                         |                   |



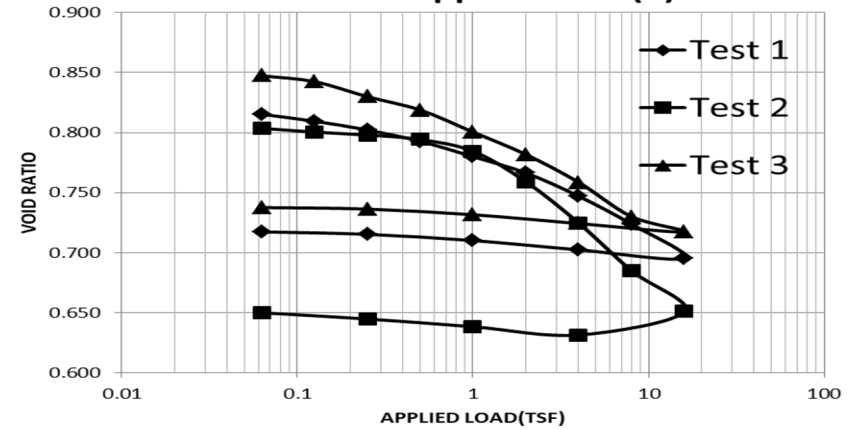
# Consolidation: Treated Sand

**J13-0**  
Void ratio vs. Applied Load(1)



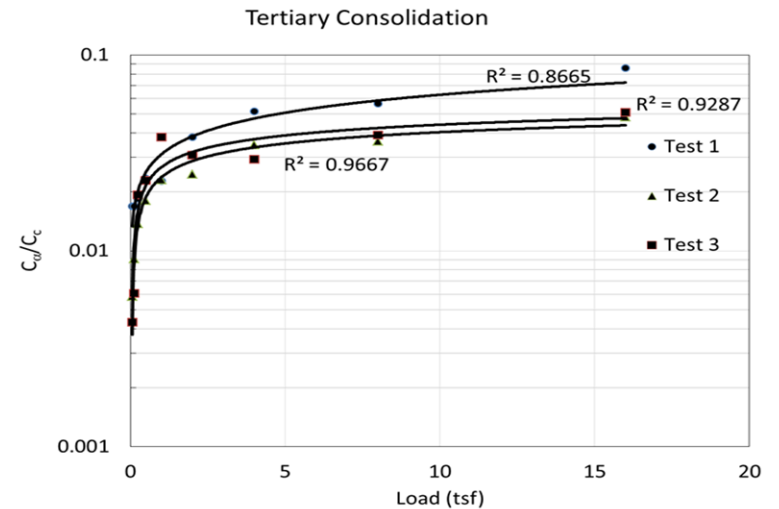
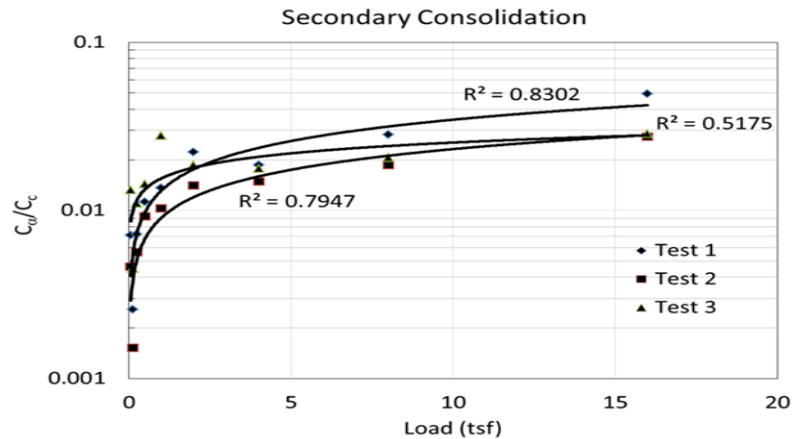
| J13-0                        | Test 1 | Test 2 | Test 3 |
|------------------------------|--------|--------|--------|
| $C_C$                        | 0.077  | 0.156  | 0.103  |
| $C_R$                        | 0.022  | 0.022  | 0.020  |
| Initial Void Ratio           | 0.72   | 0.75   | 0.75   |
| pH                           | 7      | 7      | 7      |
| Initial moisture content (%) | 0.45   | 0.45   | 0.44   |
| Wet density (pcf)            | 96.2   | 95.0   | 94.2   |
| Dry density (pcf)            | 95.7   | 94.5   | 93.7   |

**J14-2**  
Void ratio vs. Applied Load(1)



| J14-2                        | Test 1 | Test 2 | Test 3 |
|------------------------------|--------|--------|--------|
| $C_C$ (1)                    | 0.071  | 0.123  | 0.086  |
| $C_R$ (1)                    | 0.012  | 0.012  | 0.125  |
| $C_C$ (2)                    | 0.066  | 0.116  | 0.080  |
| $C_R$ (2)                    | 0.013  | 0.011  | 0.012  |
| Initial Void Ratio           | 0.79   | 0.81   | 0.85   |
| pH                           | 5      | 5      | 5      |
| Initial moisture content (%) | 0.75   | 0.75   | 0.75   |
| Wet density (pcf)            | 92.6   | 91.2   | 89.1   |
| Dry density (pcf)            | 91.9   | 91.2   | 89.1   |

# Secondary and Tertiary Compression: 10% Organic Content



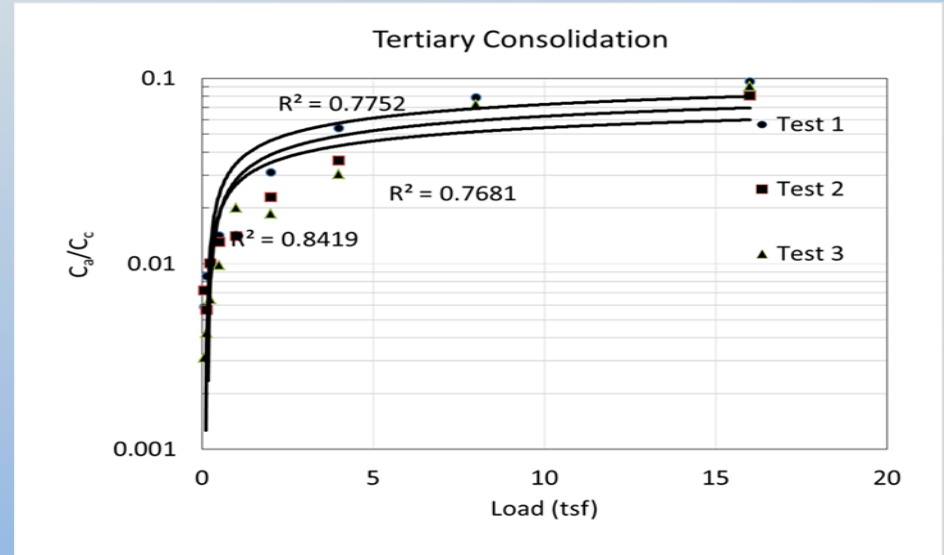
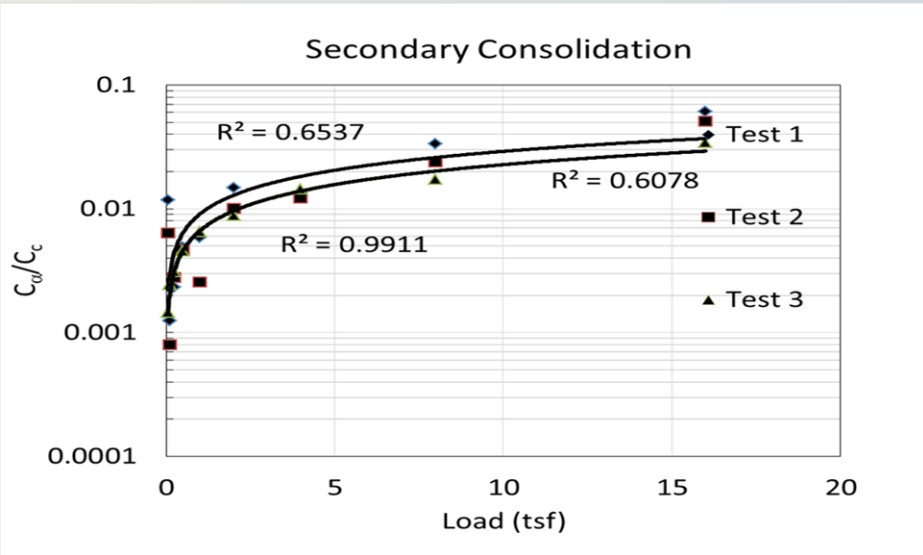
Averages – Secondary Consolidation

|             | Test 1  | Test 2  | Test 3  |
|-------------|---------|---------|---------|
| $C_a$       | 0.0014  | 0.00069 | 0.0011  |
| $C_{ae}$    | 0.00082 | 0.00044 | 0.00071 |
| $C_a/C_c$   | 0.018   | 0.011   | 0.017   |
| $C_{ae}/OC$ | 0.0081  | 0.0044  | 0.0071  |

Averages – Tertiary Consolidation

|             | Test 1 | Test 2  | Test 3 |
|-------------|--------|---------|--------|
| $C_a$       | 0.0028 | 0.0013  | 0.0016 |
| $C_{ae}$    | 0.0017 | 0.00093 | 0.0011 |
| $C_a/C_c$   | 0.037  | 0.025   | 0.027  |
| $C_{ae}/OC$ | 0.017  | 0.0092  | 0.011  |

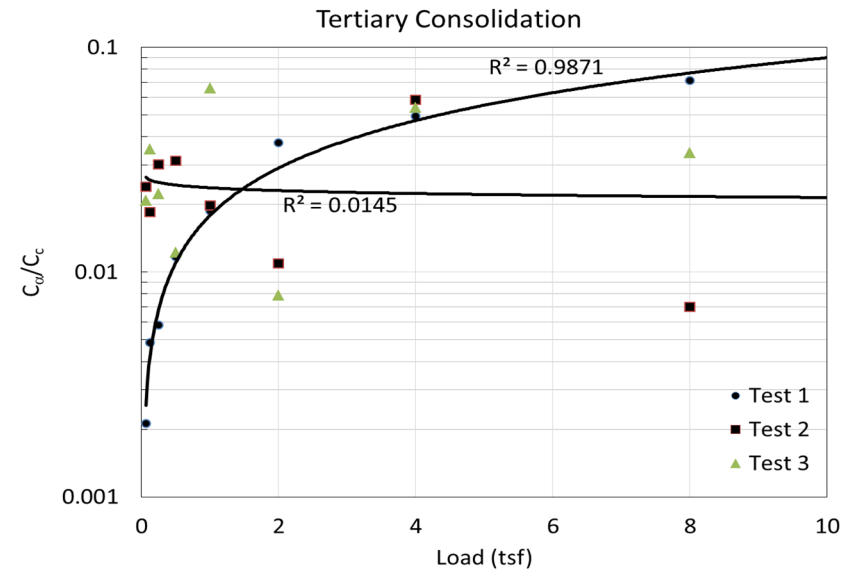
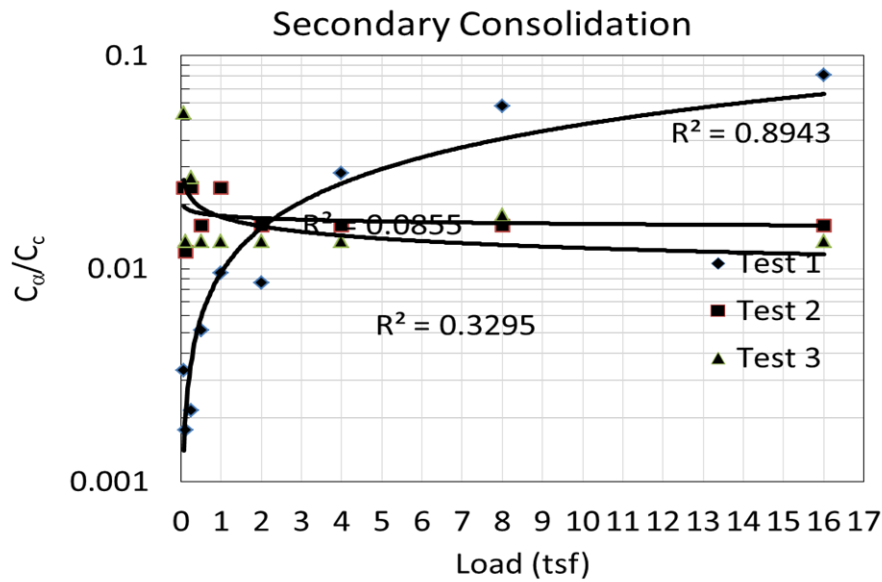
# Secondary and Tertiary Compression: 30% Organic Content



| Averages – Secondary Consolidation |        |        |        |
|------------------------------------|--------|--------|--------|
|                                    | Test 1 | Test 2 | Test 3 |
| $C_a$                              | 0.0058 | 0.0049 | 0.0036 |
| $C_{ae}$                           | 0.0025 | 0.0019 | 0.0015 |
| $C_a/C_c$                          | 0.017  | 0.013  | 0.010  |
| $C_{ae}/OC$                        | 0.0083 | 0.0064 | 0.0051 |

| Averages – Tertiary Consolidation |        |        |        |
|-----------------------------------|--------|--------|--------|
|                                   | Test 1 | Test 2 | Test 3 |
| $C_a$                             | 0.012  | 0.0091 | 0.0098 |
| $C_{ae}$                          | 0.0052 | 0.0036 | 0.0042 |
| $C_a/C_c$                         | 0.035  | 0.024  | 0.028  |
| $C_{ae}/OC$                       | 0.017  | 0.012  | 0.014  |

# Secondary and Tertiary Compression: 50% Organic Content



**Averages – Secondary Consolidation**

|             | Test 1 | Test 2 | Test 3 |
|-------------|--------|--------|--------|
| $C_a$       | 0.015  | 0.011  | 0.013  |
| $C_{ae}$    | 0.0042 | 0.0032 | 0.0036 |
| $C_a/C_c$   | 0.022  | 0.018  | 0.020  |
| $C_{ae}/OC$ | 0.0080 | 0.0063 | 0.0071 |

**Averages – Tertiary Consolidation**

|             | Test 1 | Test 2 | Test 3 |
|-------------|--------|--------|--------|
| $C_a$       | 0.023  | 0.015  | 0.016  |
| $C_{ae}$    | 0.0066 | 0.0042 | 0.0053 |
| $C_a/C_c$   | 0.034  | 0.025  | 0.029  |
| $C_{ae}/OC$ | 0.013  | 0.0084 | 0.011  |

# UNF New Treatment Options

- UNF Treatment Cells

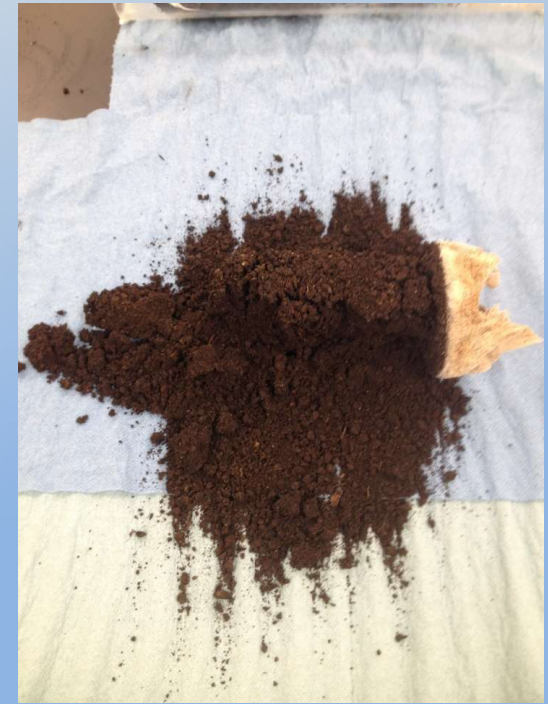


- Were using two strains purchased from ATCC & USDA
- New approaches
  - Strains distributed by USDA Strain
  - New Method: Deep Soil Treatment
  - Possible enzyme treatment option

# Organics – Percolation Method



48hr Run



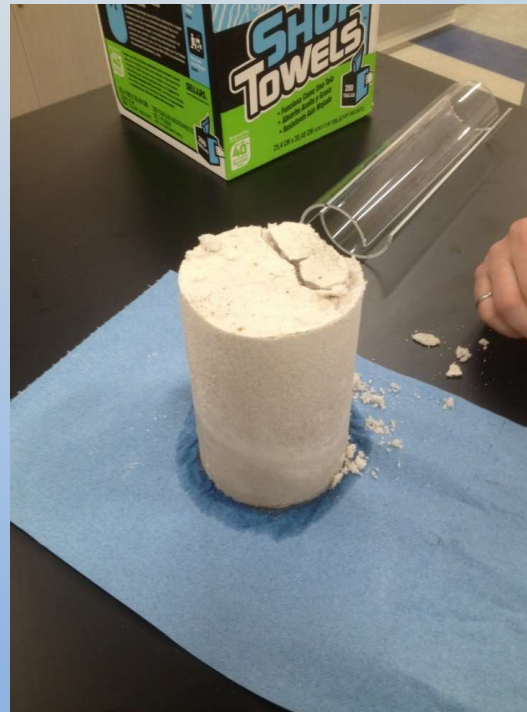
50% OC soil  
2.5M Urea 2.5M CaCl<sub>2</sub>

Post Treatment Wet

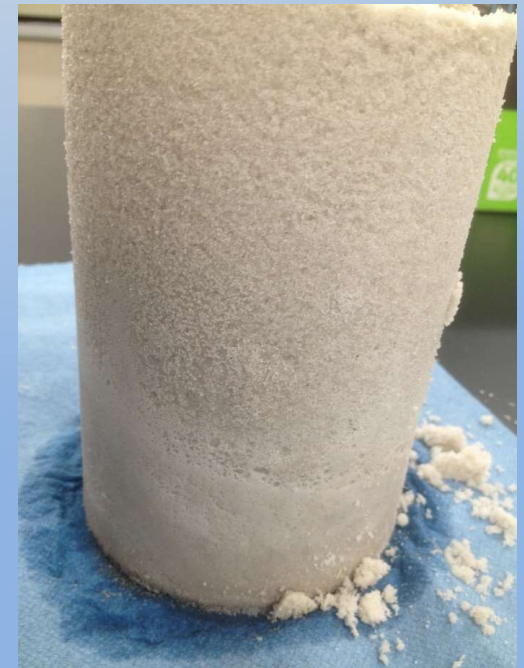
Post Treatment Dry



# Deep Soil Treatment - New Approach



Ottawa Sand – 1.0M Urea, 0.25M  $\text{CaCl}_2$



24hr Run

# Organics – Deep Soil Treatment Approach



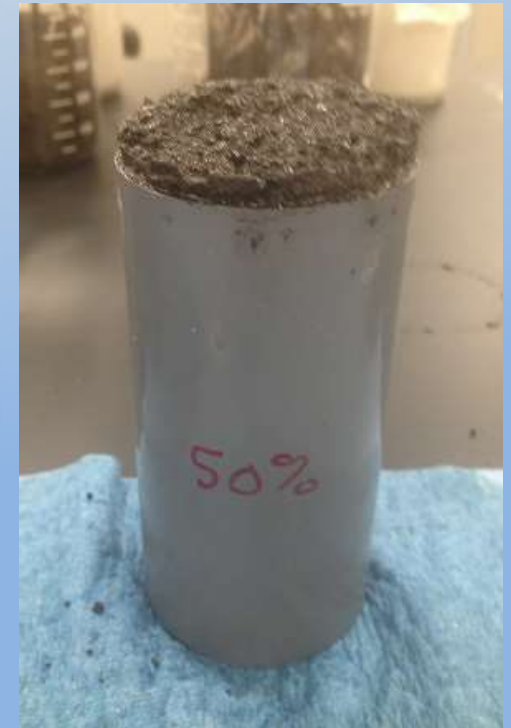
Ottawa Sand



10% OC Soil



30% OC Soil



50% OC Soil



# Organics – Deep Soil Treatment Approach



# Organics – Deep Soil Treatment Approach



Ottawa Sand

10% OC Soil

30% OC Soil

50% OC Soil

# Organics – Deep Soil Treatment Approach



Post Treatment Percolation Method

# Organics – Deep Soil Treatment Approach



10% OC Soil

30% OC Soil

50% OC Soil

# Organics – Future Direction(s)

- Explain why sporesarcina likes silica more than OC.
  - SEM to look for calcification points and particle bridging
  - Surface area effects to cause a morphological change in the bacteria to induce calcite formation. Use of Surfactants to modify the soil surface tension.
  - CT progressive scans of calcite precipitation in situ.
  - Compression chamber to prevent CO<sub>2</sub> escape thus possibly increasing homogeneity and calcite yield.
  - Enzyme treatment of OC soils with knowledge of above without having to deal with a living organism.

# Summary

- Ottawa treatment
  - Have shown success comparative to previous studies
  - Completed DST
  - Consolidation in progress
  - Beginning triaxial soon
- Organics treatment
  - Underway
  - Preliminary results presented
- More collaborative treatment process
  - Treating at UF/UNF
  - Expanding treatment options
- Increasing productivity/success
  - Introducing more treatment options
  - Multiple treatments at a time

Thank You!

Questions?

