

**Evaluation of Static Design Resistance for Deep Foundations, FB-DEEP**  
(BDV31 977-05)

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**Researchers:** Lin Huang, Thai Nguyen, John Schwartz

**Grip**

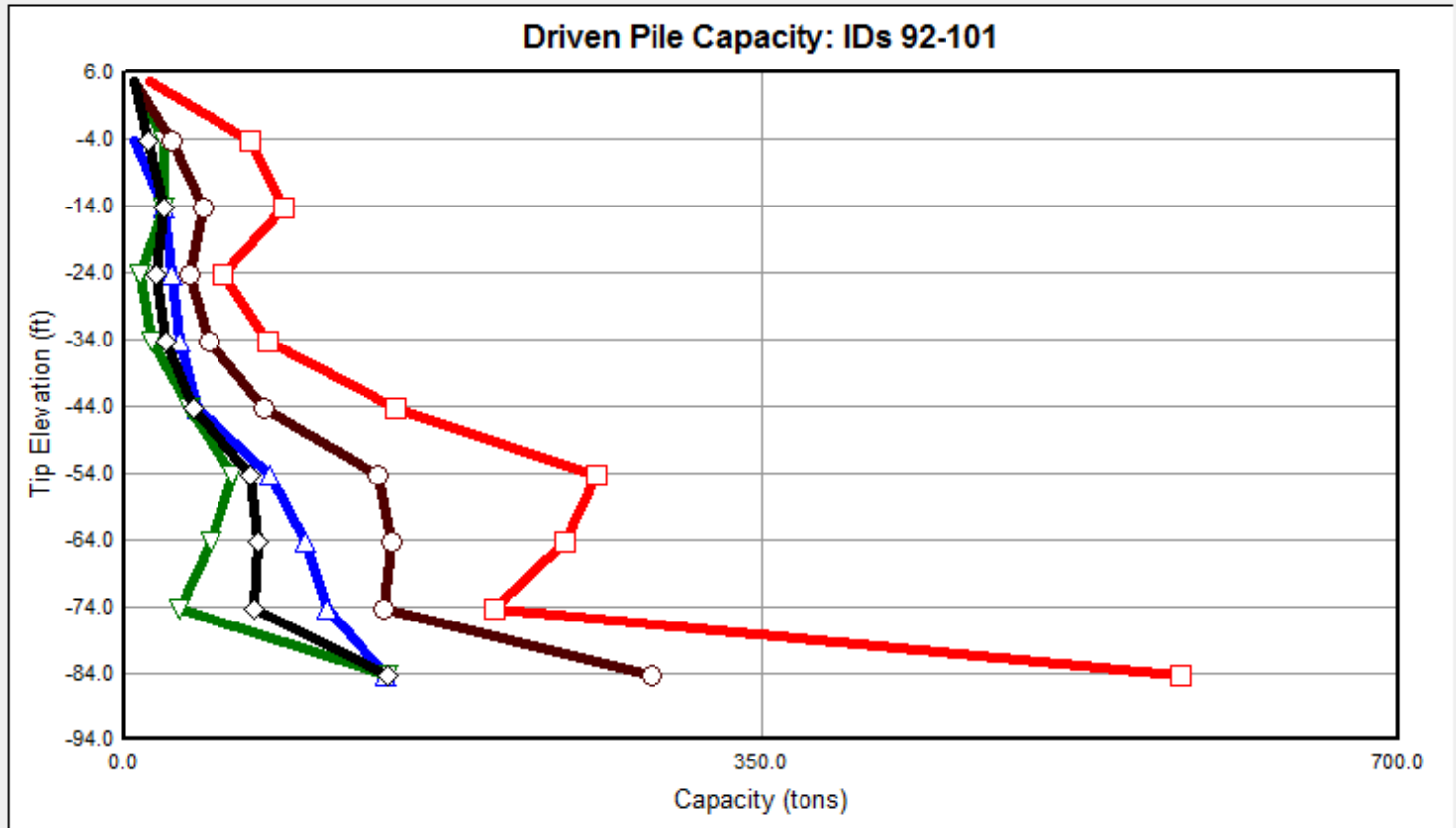
August 21, 2015

- FB-DEEP Software Predicts Nominal Side ( $R_s$ ), Tip ( $R_T$ ) and Total ( $R_N = R_s + R_T$ ) Resistance for Driven (steel H, Prestressed Concrete, and Steel Pipe) Piles and Drilled Shafts based on In situ data(SPT, CPT - piles) and laboratory (rock strength - drilled shafts); Used In FB-MultiPier for Substructure Pier Analysis and Design
- FB-DEEP also identifies LRFD Design Resistances ( $\Phi R_N$ ) for piles and shafts based on database of mean biases [measured nominal resistance (e.g. Davisson, FHWA) divided predicted resistance], and Coefficient of Variations (CV) of biases.

# FB-DEEP PCP Prediction

Job Name: South Bear

State Job (Project) #: 409040



## Curves

- Ultimate Side Friction
- Mobilized End Bearing
- Ultimate Pile Capacity
- Estimated Davisson Capacity
- Allowable Pile Capacity

\*The 'Save to File' button saves the currently selected Curves to a text file.

## Driven Pile Data

Boring Number: B-5  
 Ground Surface Elevation: 15.72 (ft)  
 Section: Square  
 Width: 24.00 (in)

## Project Data

File: Pile\_Example1  
 Date: Aug 03, 2015  
 Engineer: Ahmed

## Analysis Data

Analysis Type: SPT

Customize

Update Plot

Close

Print Graph

Print Window

Save To File

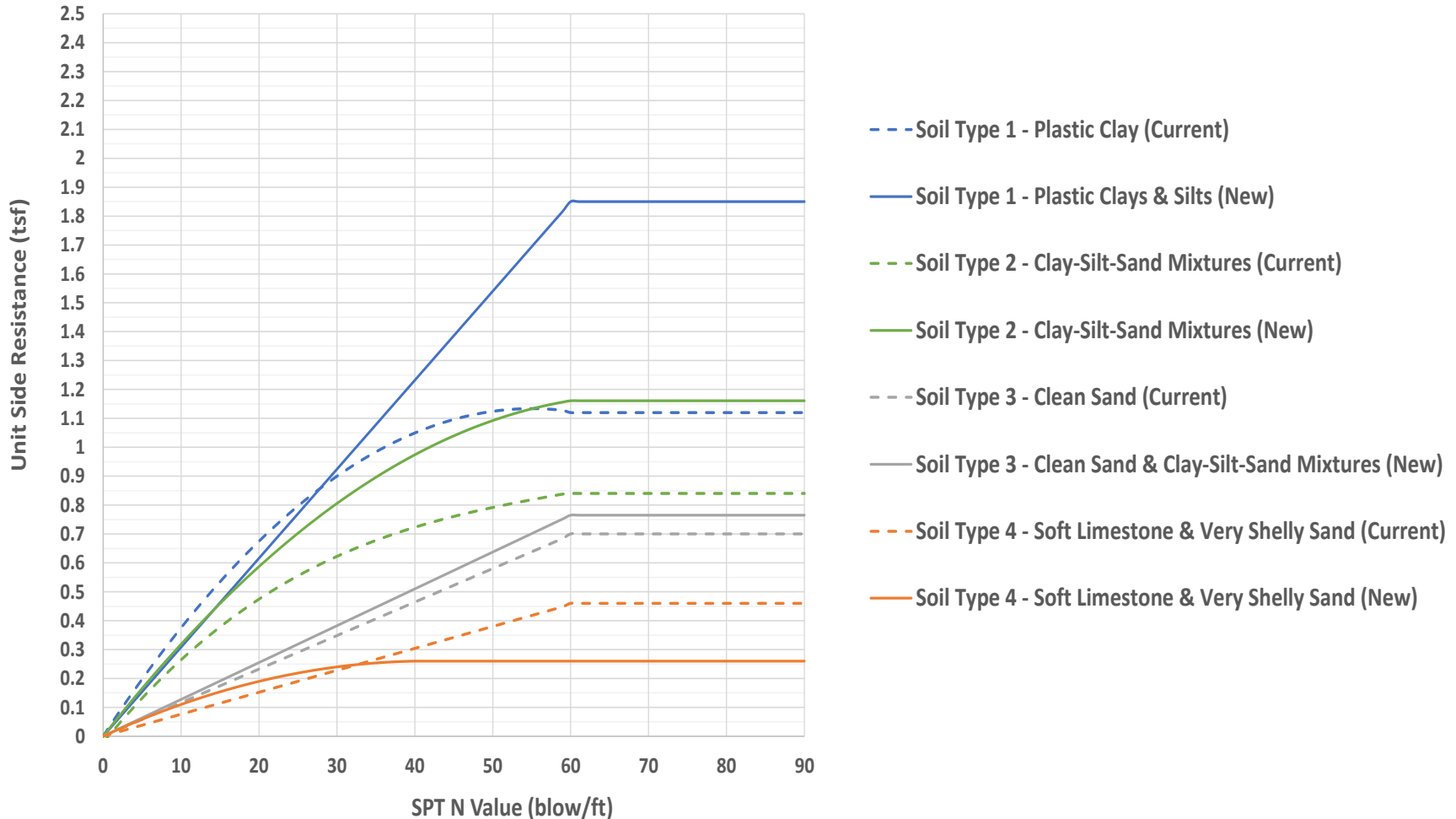
- For H piles, re-evaluate predicted side and tip resistances for piles driven through multiple layers of sand, clay and limestone;
- Evaluate side resistance for **permanent** cased drilled shafts in Limestone (FB-DEEP currently neglects);
- For prestressed concrete piles (PCP) re-evaluate side and tip resistance for piles driven into weathered (FHWA IGM – Intermediate Geotechnical Material) versus competent limestone (FB-DEEP currently treats both same);

## Sites with H Piles Evaluated in Florida:

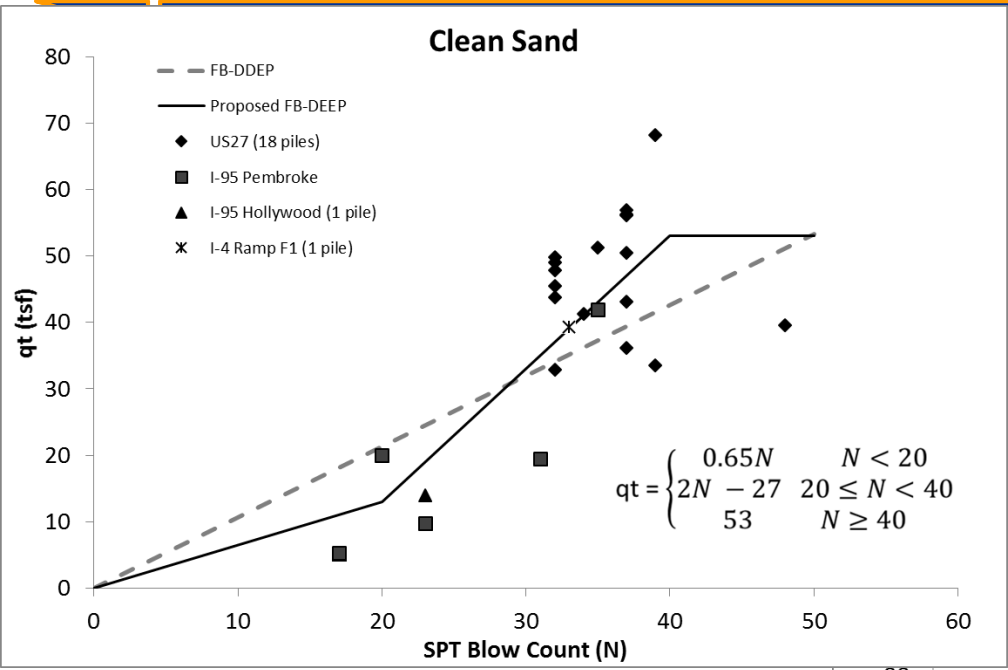
Site Information		Insitu Information		Pile Information			
Project Number (Financial)	Project Site	# of Soil Borings	Predominant Soil Type	Dimensions (in)	Length (ft)	# of Piles with CAPWAP	# of BOR CAPWAP Analyses
208466-2-52-01	SR 51 from Taylor County Line to Dixie County Line	66	Sand & Rock	14 x 89	60 - 120	3	1
221754-1-52-01	CR 146 over Aucilla River	9	Sand, Clay & Rock	14 x 117	150 - 220	5	0
422796-1-52-01 & 422796-2-52-01	Widening I 95 (SR 9) over Hallandale Beach Boulevard Bridge	5	Sand & Rock	18 x 135	90 - 116	8	5
	Widening I 95 (SR 9) over Hollywood Boulevard (SR 820)	3	Sand & Rock	18 x 135	90 - 115	11	3
	Widening I 95 (SR 9) over Stirling Road (SR 848)	3	Sand & Rock	18 x 135	110 - 168	5	4
	Widening I 95 (SR 9) over Pembroke Road Bridge	3	Sand & Rock	19 x 135	85	9	6
403984-1-52-01	Eller Drive Overpass (SR 862)	29	Sand & Rock	14 x 73	90 - 140	3	0
242484-2-52-01	I-4 (SR 408)/SR 408 interchange (Widening at Church Street Viaduct; Phase 1)	29	Sand & Clay	14 x 89 & 12 x 53	90 - 140	37	5
	I-4 (SR 408)/SR 408 interchange (Widening over Robinson Street; Phase 2)	1	Sand	14 x 89	100 - 150	14	1
	I-4 (SR 408)/SR 408 interchange (Widening over South Street; Phase 3)	2	Sand & Clay	12 x 53	150	3	0
	Ramp E (Phase 4)	3	Sand & Clay	14 x 89	150	3	0
	Ramp F2 (Phase 5)	5	Sand	14 x 89	105 - 135	3	0
	Ramps D & D1 (Phase 6)	20	Sand & Clay	12 x 53	90 - 115	18	1
	Anderson Street Overpass & Ramp F1 (Phase 7)	7	Sand & Clay	14 x 89	---	4	1
	Ramp C (Phase 8)	12	Sand	14 x 89	---	12	0
238429-3-52-01	US 27 (SR 50) Interchange at SR 50	7	Sand	14 x 73	99 - 120	33	18
<b>Total # of Soil Borings</b>		<b>204</b>		<b>Total # of CAPWAP Analyses</b>		<b>171</b>	<b>45</b>

# 6 Analysis of Side Friction for H Piles in FB-DEEP

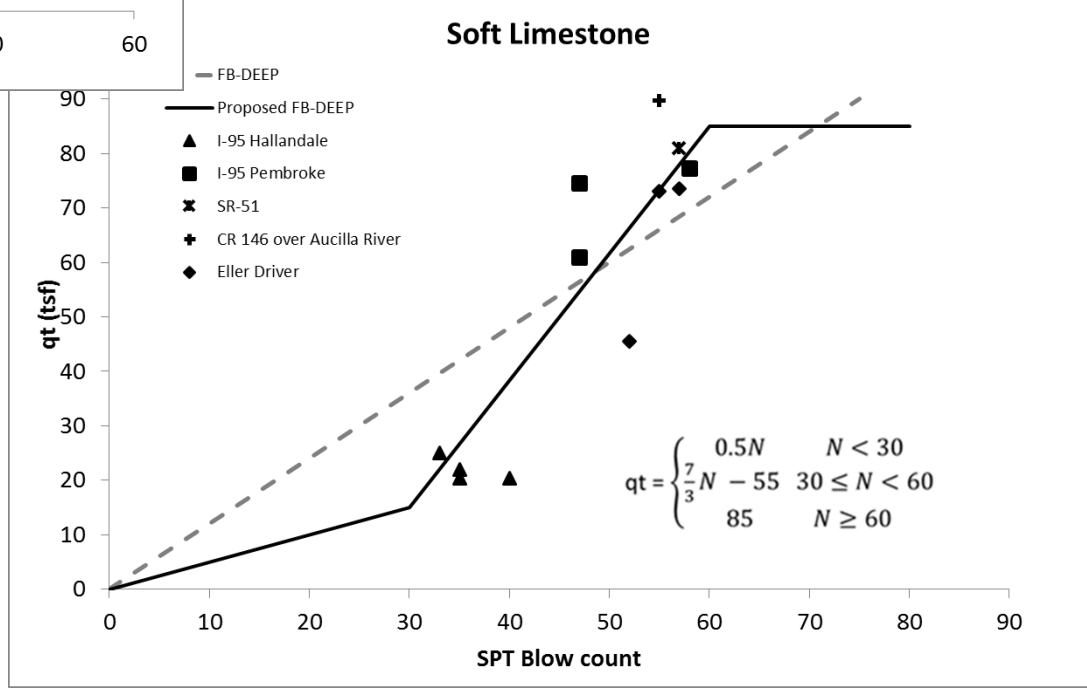
## Ultimate Unit Side Resistance: Current FB-Deep vs. New Curves



# Analysis of Tip Resistance for H Piles in FB-DEEP



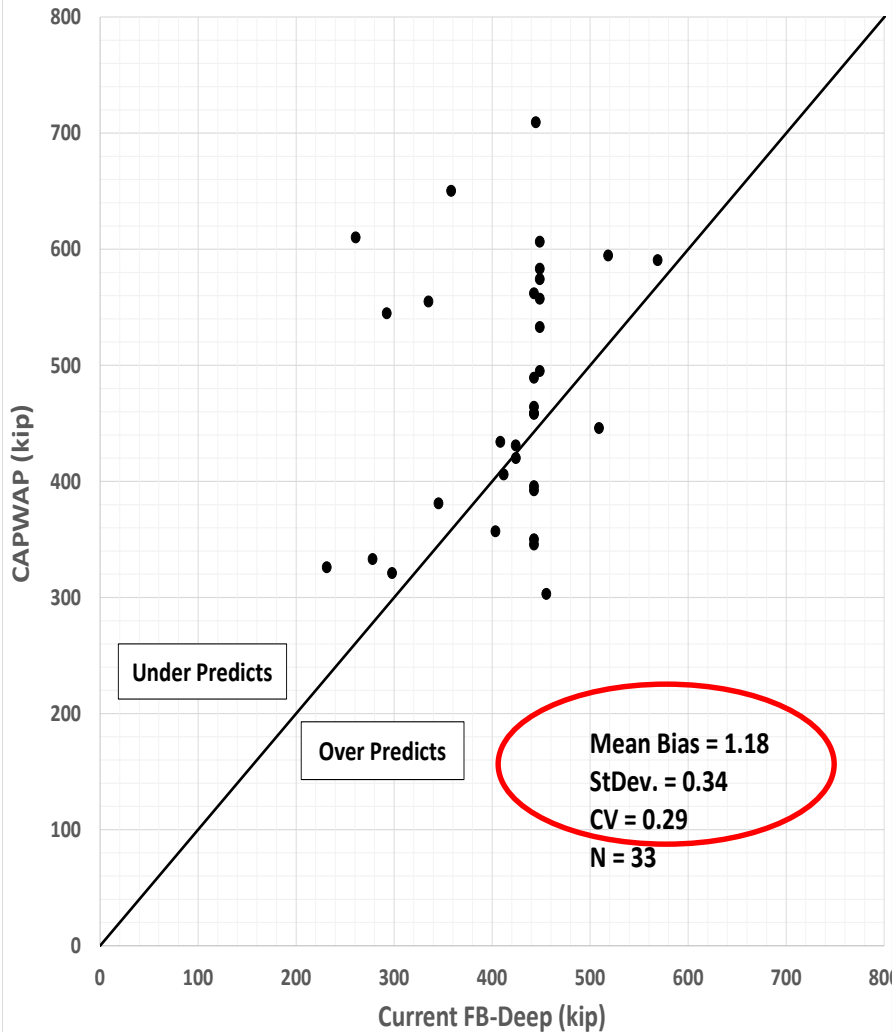
Average 8B Below the Pile Tip



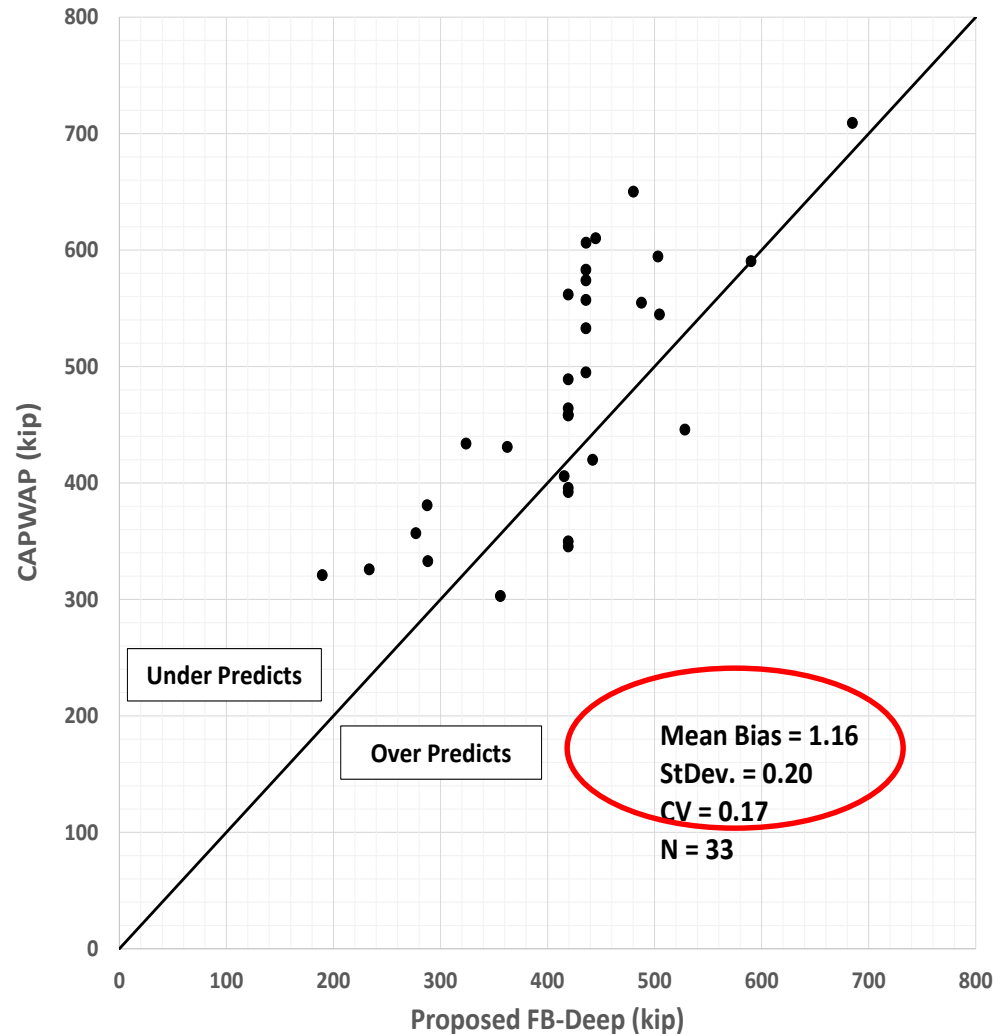
# Predicted & Measured H Pile Response for FB-DEEP

8

• Total Capacity: Current FB-Deep vs. CAPWAP



• Total Capacity: Proposed FB-Deep vs. CAPWAP





# H Piles Plug Conditions

- Difficulties in Matching Results with Measured Data
  1. Soil Borings



# H Piles Plug Conditions

- Difficulties in Matching Estimates with Measured Data
  1. Soil Borings



# H Piles Plug Conditions

- Difficulties in Matching Estimates with Measured Data
  1. Soil Borings



**Contractor built a dirt road to get to the site**

# H Piles Plug Conditions

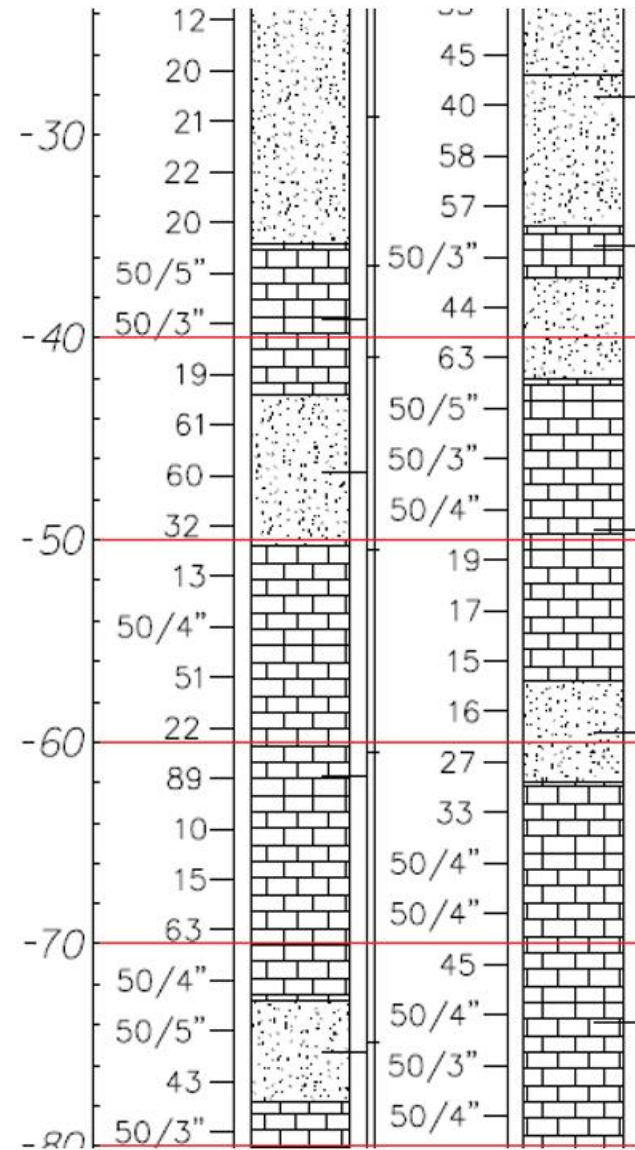
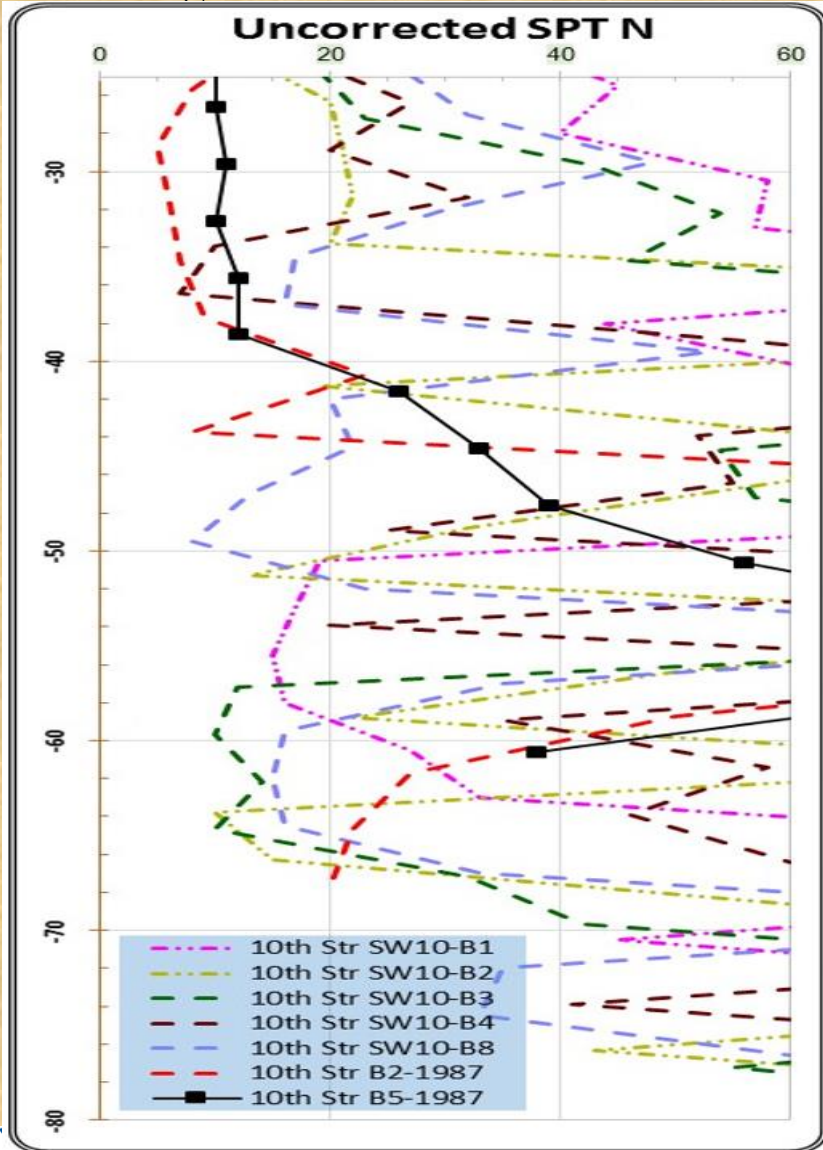
- Difficulties in Matching Estimates with Measured Data
  2. Soil Gaps (between the H Pile Flanges) have not been recorded

3. Long term capacities are rarely evaluated (7-day RESTRIKE or longer)
4. Static Load Tests not common



# H Piles Plug Conditions – Case Studies

1) Project in Progress HP 14x89 with 4.2-k Ram D19-42 Hammer

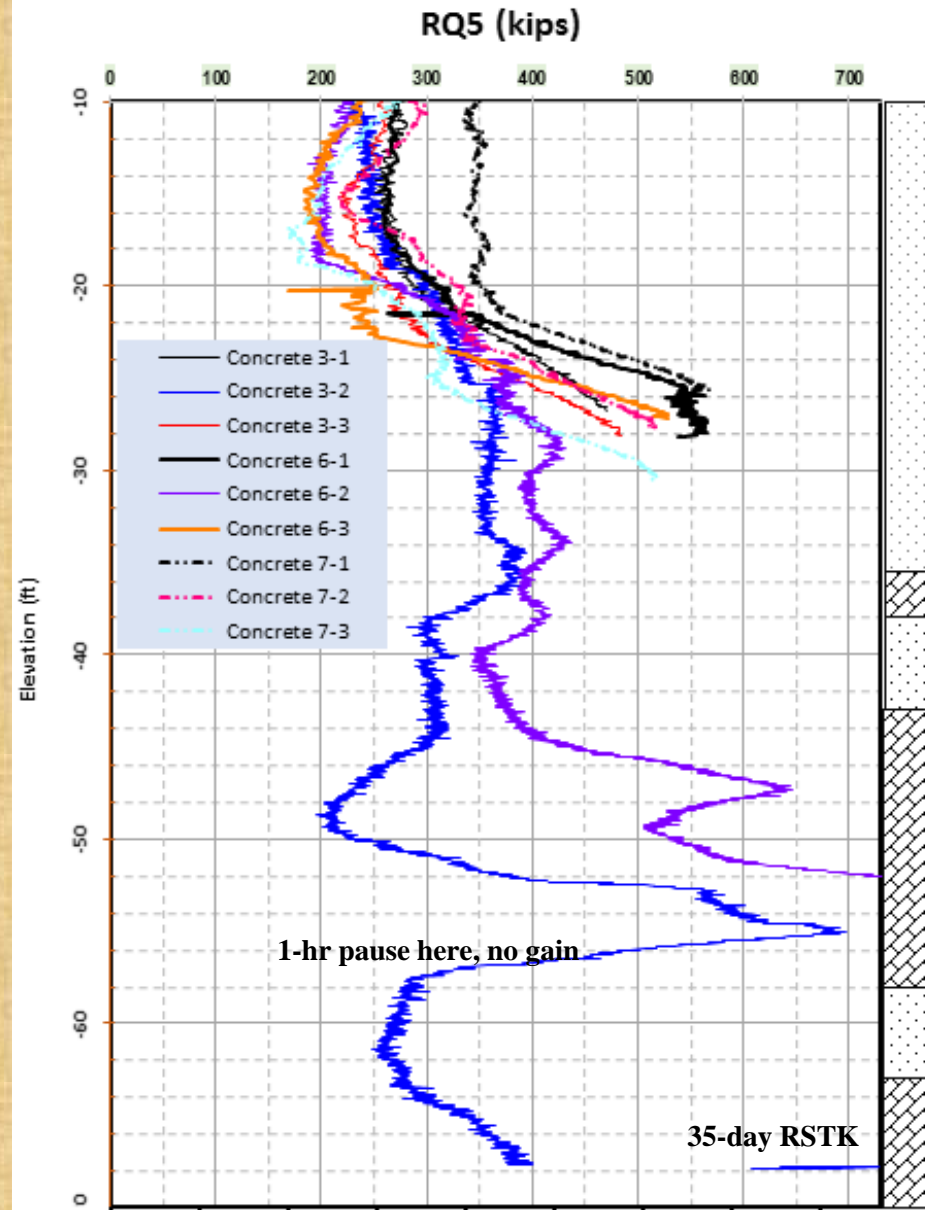


Variability in Soil Profiles

# H Piles Plug Conditions – Case Studies

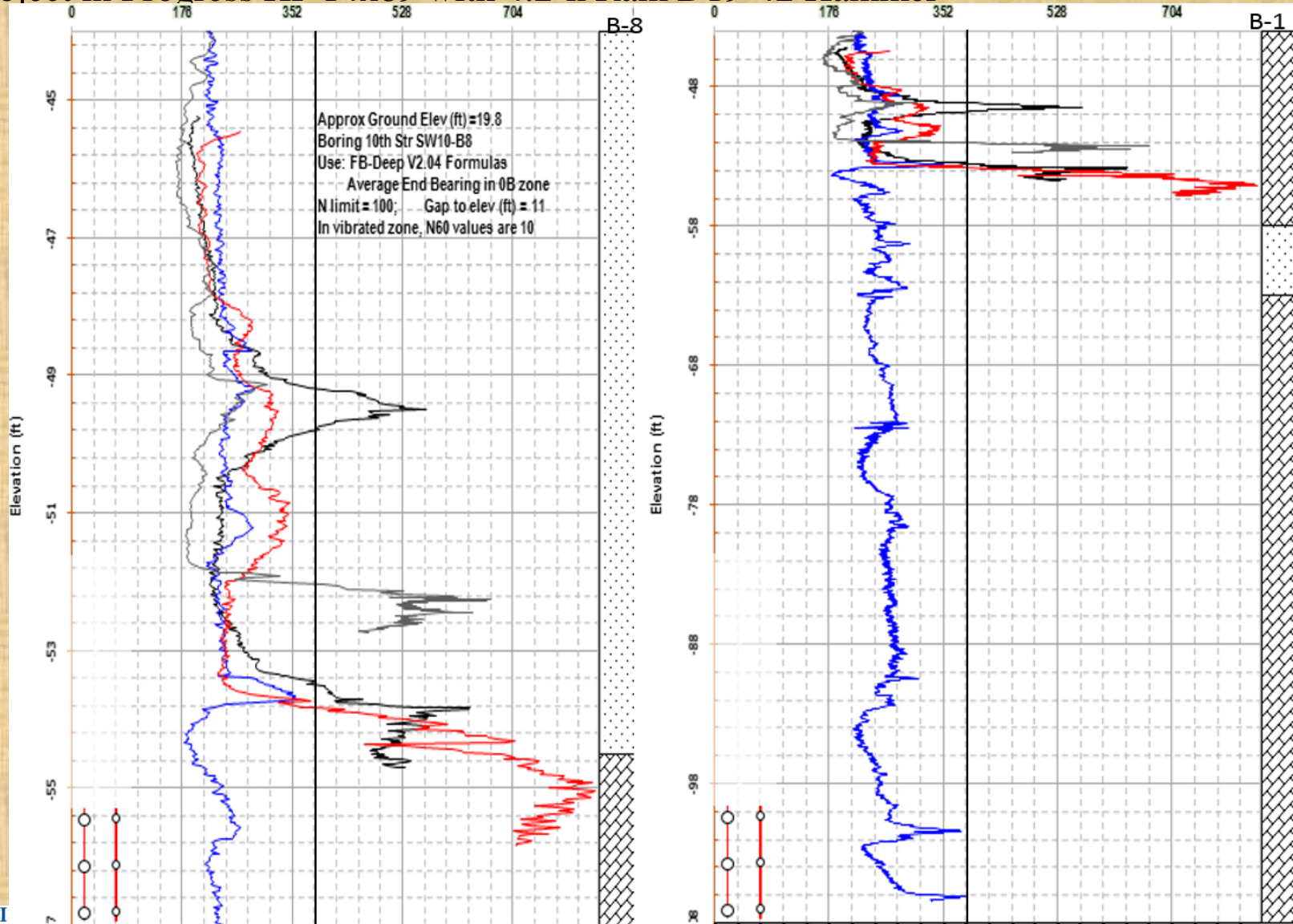
1) Project in Progress HP 14x89 with 4.2-k Ram D19-42 Hammer

Variability in PDA results  
(Concrete Piles at the  
same site)



# H Piles Plug Conditions – Case Studies

## 1) Project in Progress HP 14x89 with 4.2-k Ram D19-42 Hammer

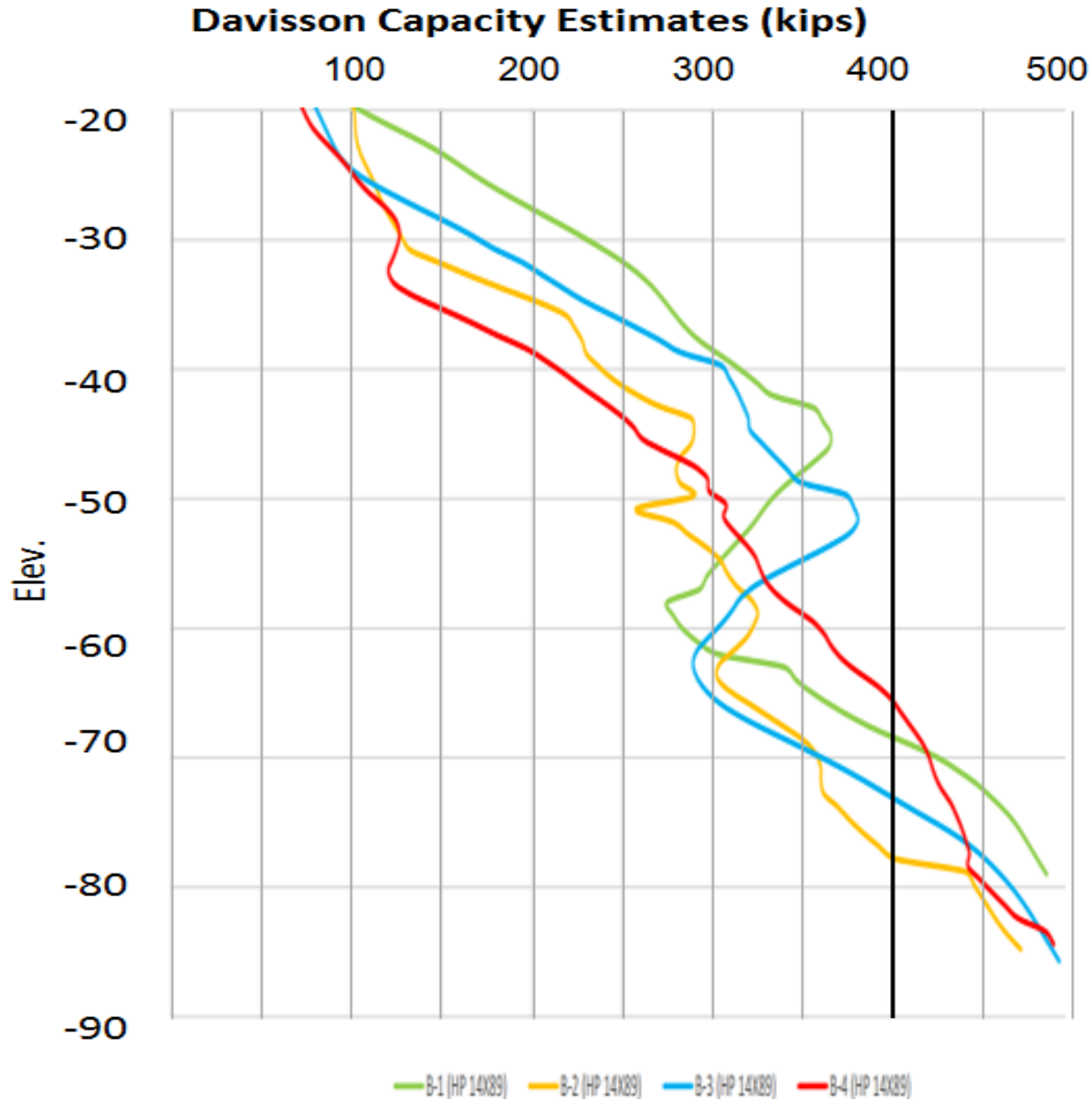


Variability in PDA results

# H Piles Plug Conditions – Case Studies

1) Project in Progress HP 14x89 with 4.2-k Ram D19-42 Hammer

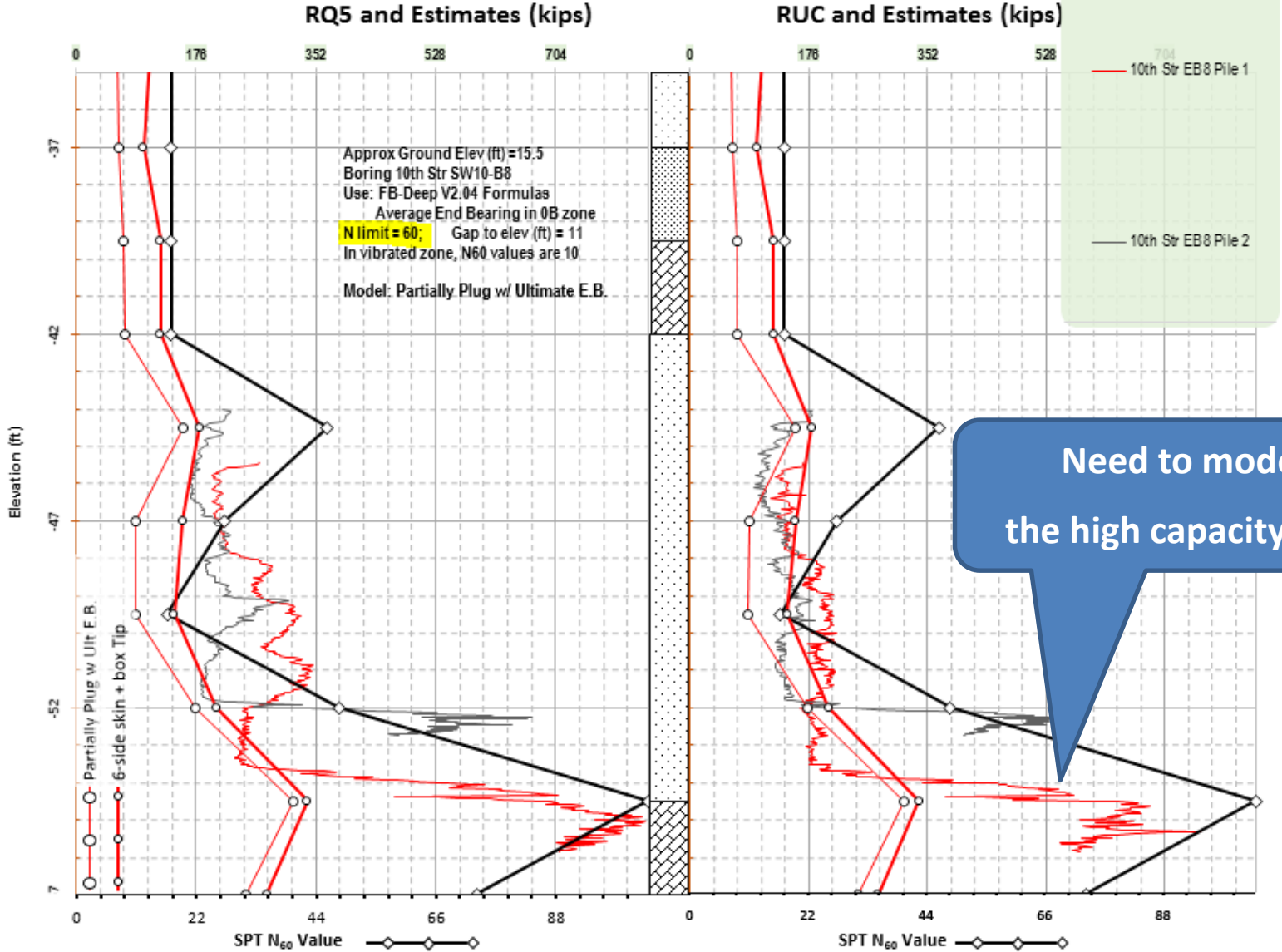
However, due to the averaging (8B+3.5B) and critical depth correction, all current FB-Deep curves looks quite similar, with all of them expecting 400 kips (required) at around elev. -70 ft. No curve is showing 500 to 700 kips at elev. – 50 to -56 ft.





# H Piles Plug Conditions – Case Studies

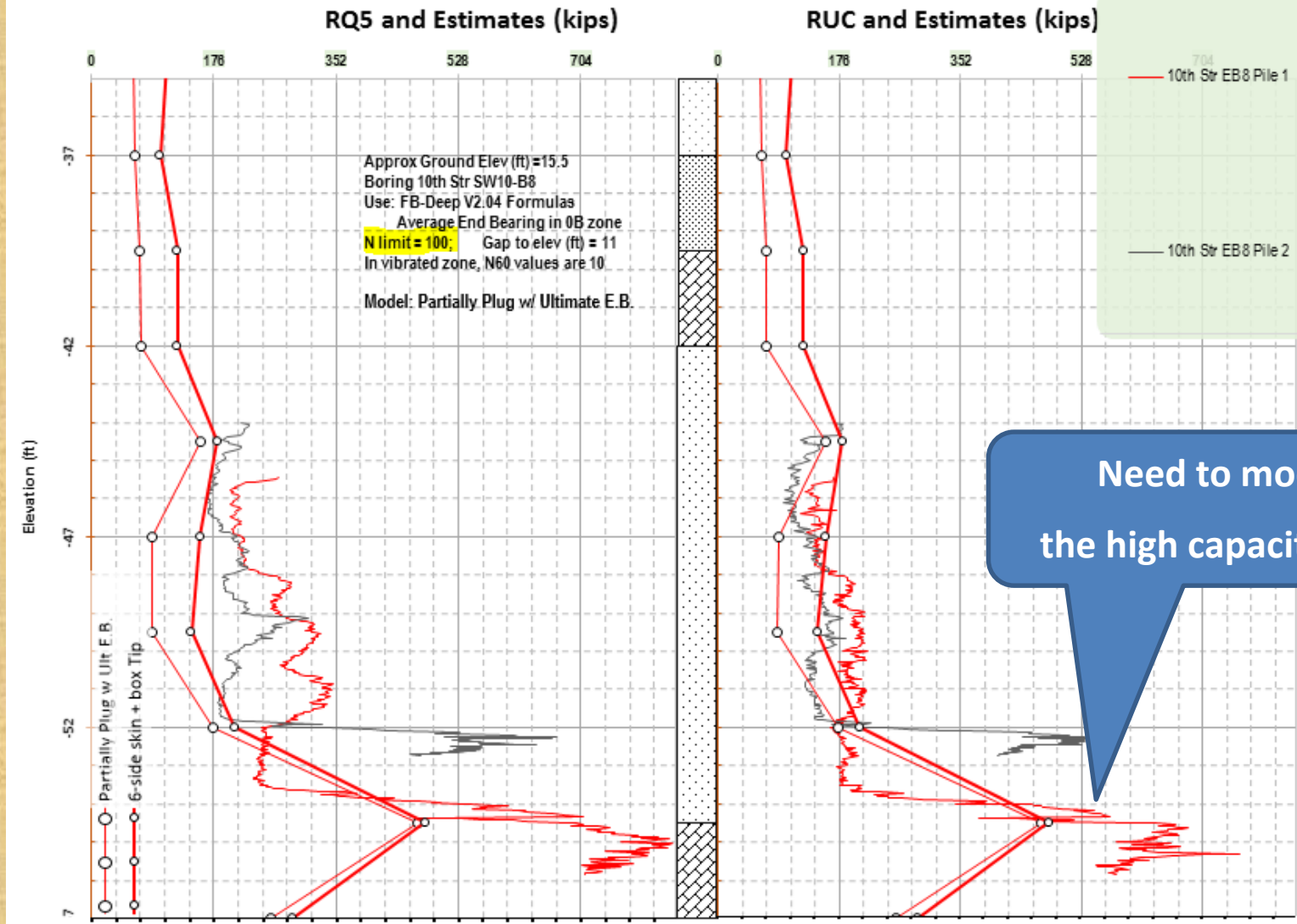
1) Project in Progress HP 14x89 with 4.2-k Ram D19-42 Hammer



Research boring done within 3-ft of Pile

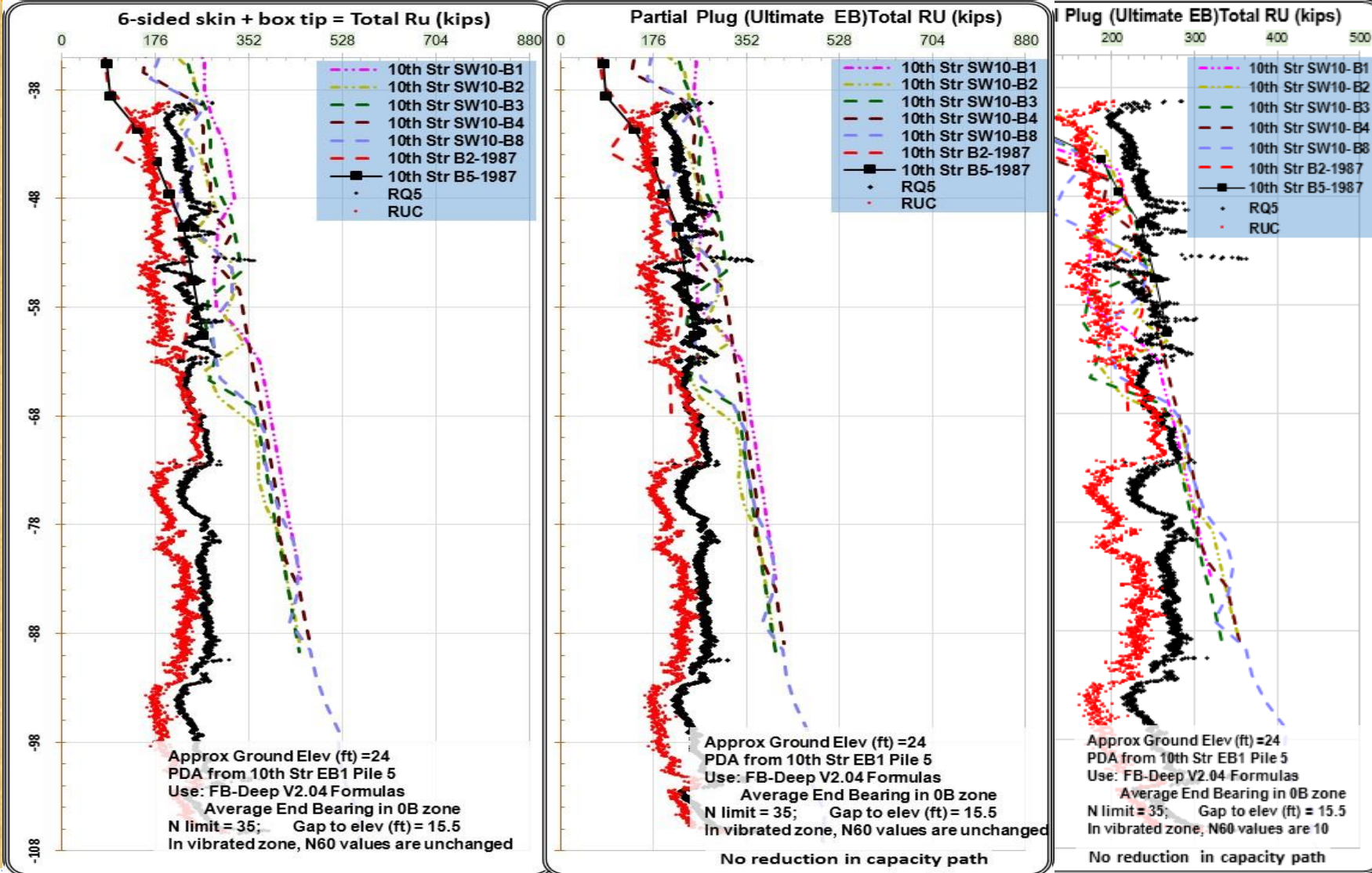
# H Piles Plug Conditions – Case Studies

## 1) Project in Progress HP 14x89 with 4.2-k Ram D19-42 Hammer



# H Piles Plug Conditions – Case Studies

## 1) Project in Progress HP 14x89 with 4.2-k Ram D19-42 Hammer

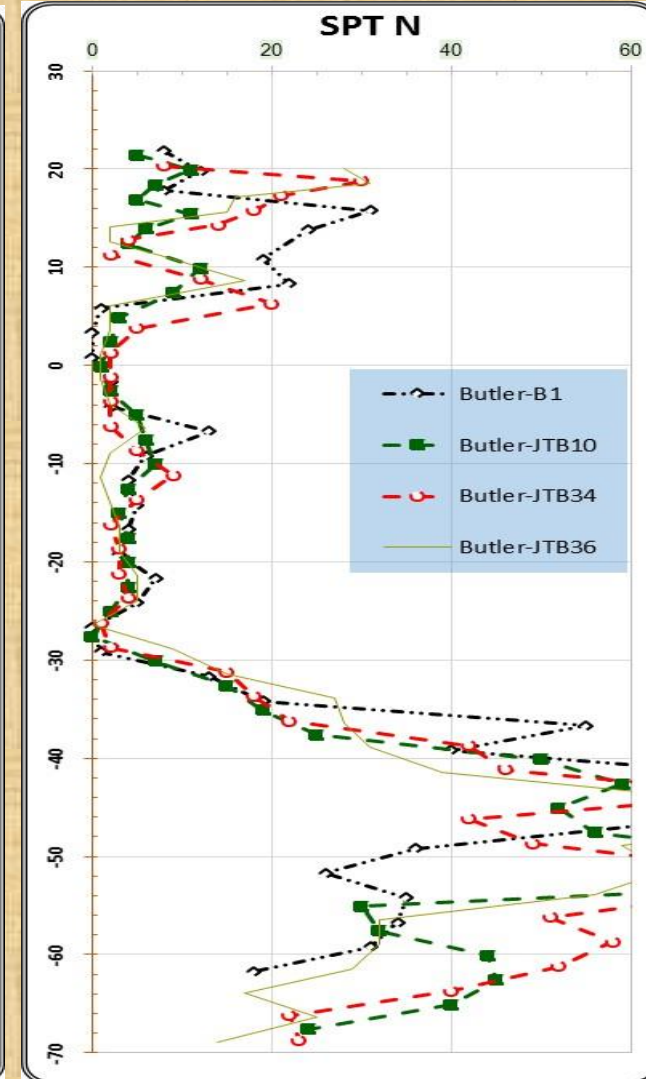
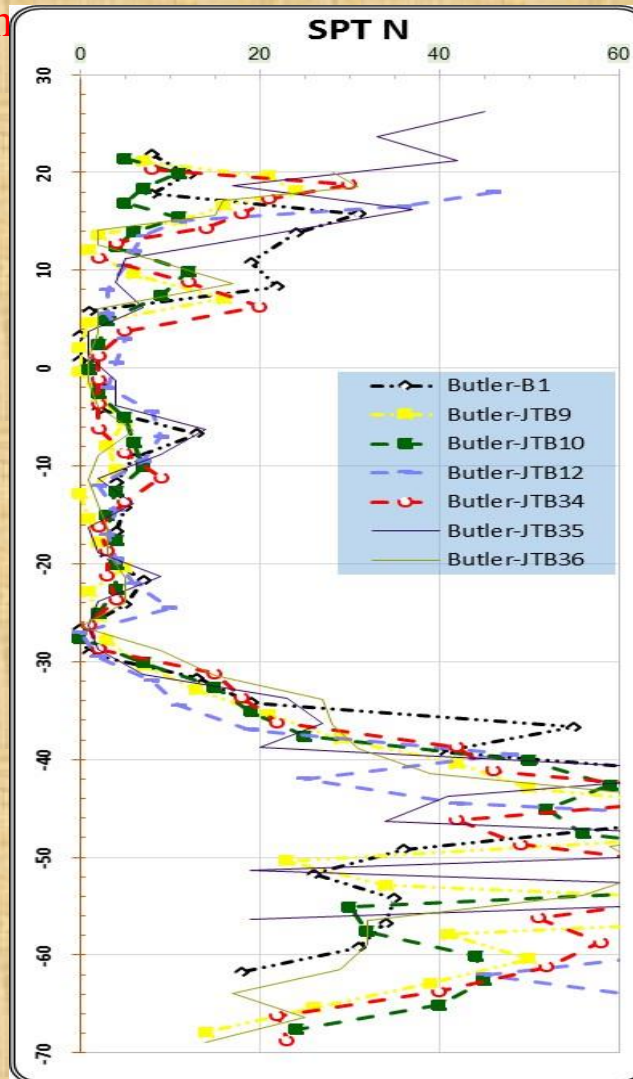


Bent 1, Pile 5 experienced no hard limestone.

N limited to lower values to reflect the thin limestone shelves; Vibrated Zone also has great influence

# H Piles Plug Conditions – Case Studies

2) I-95 over Butler Blvd (Jacksonville) HP 14x89 with 6.6-k Ram D30-42 Hammer  
Site is quite uniform

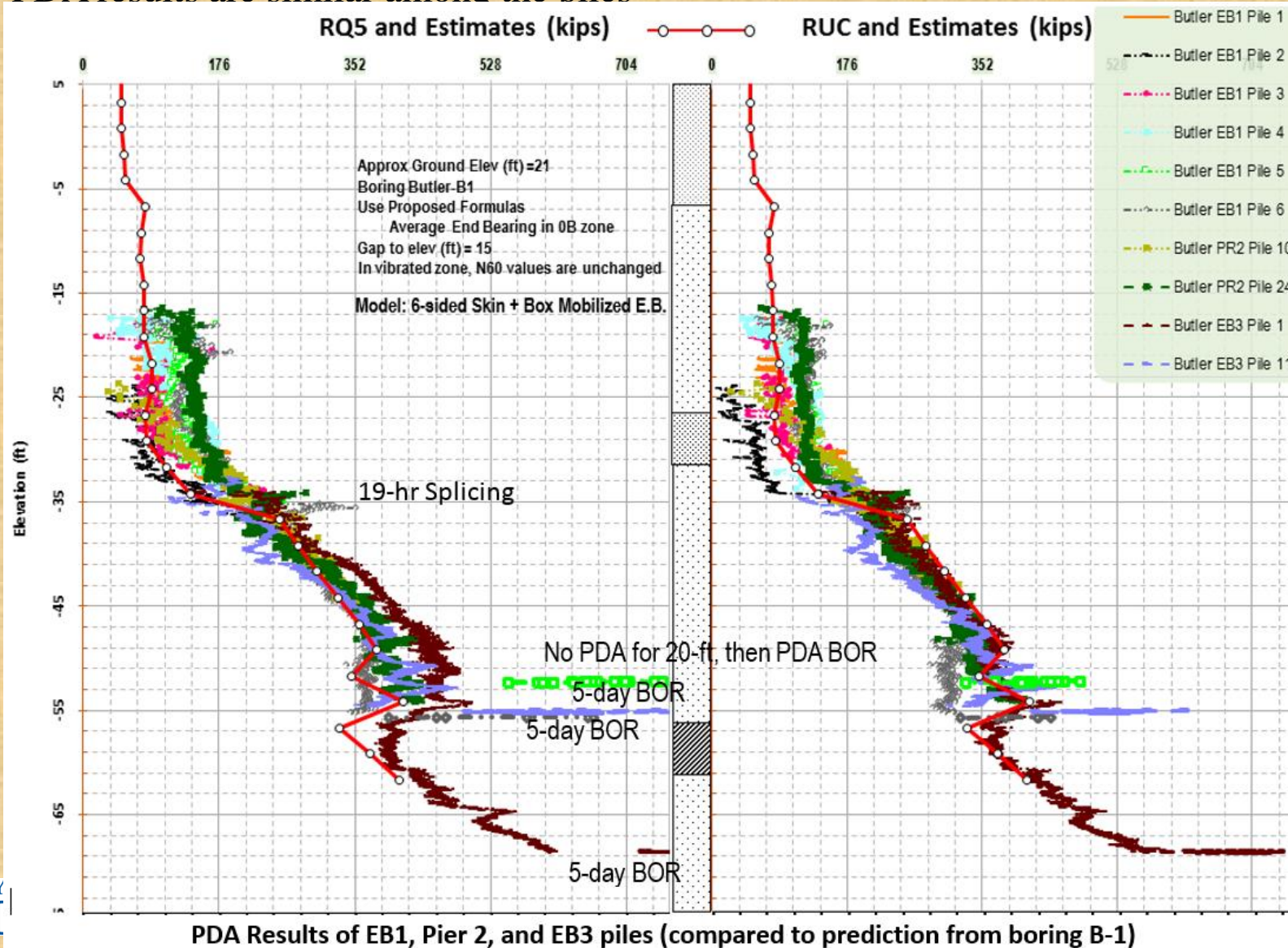


2 furthest borings are approx 200-ft apart

Borings closest to EB1  
piles (within 100-ft)

# H Piles Plug Conditions – Case Studies

- 2) I-95 over Butler Blvd (Jacksonville) HP 14x89 with 6.6-k Ram D30-42 Hammer
- PDA results are similar among the piles



# H Piles Plug Conditions – Case Studies

## 2) I-95 over Butler Blvd (Jacksonville) HP 14x89 with 6.6-k Ram D30-42 Hammer

Ultimate skin friction in layers

above bearing layer = 25.58(tons)

Average SPT in Bearing layer

above tip = 46.24(blow/ft)

Ultimate skin friction in

bearing layer = **30.77(tons)**

Corrected Ultimate skin friction

in bearing layer = **18.08(tons)**

Total Skin Friction = 43.66(tons)

End bearing capacity

ELEVATION SPT Blows UNIT E. B.

(ft)	(Blows/ft)	(tsf)	
-34.41	26.57	28.34	<-- 8B above tip
-36.70	60.00	64.00	
-39.20	49.60	52.91	
-41.70	60.00	64.00	
-44.20	60.00	64.00	<-- Pile tip elevation
-46.70	78.12	64.00	
-48.48	54.22	52.30	<-- 3.5B below tip

Average unit end bearing above pile tip= 56.99(tsf)

Average unit end bearing below pile tip= 61.56(tsf)

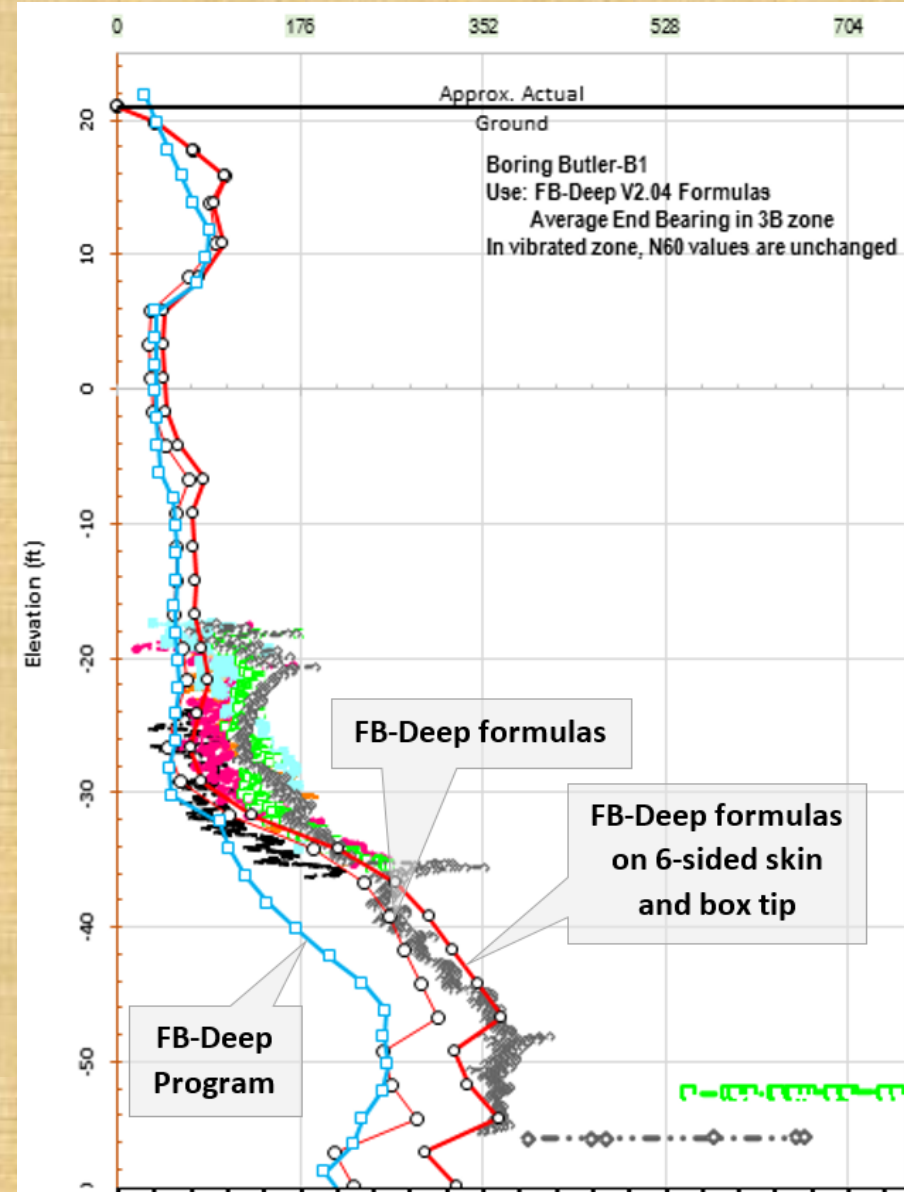
Average unit end bearing of pile tip =59.28(tsf)

Critical depth of embedment in bearing layer = 14.69(ft)

Actual depth of embedment = 12.50(ft)

Maximum mobilized end bearing capacity = **83.63(tons)**

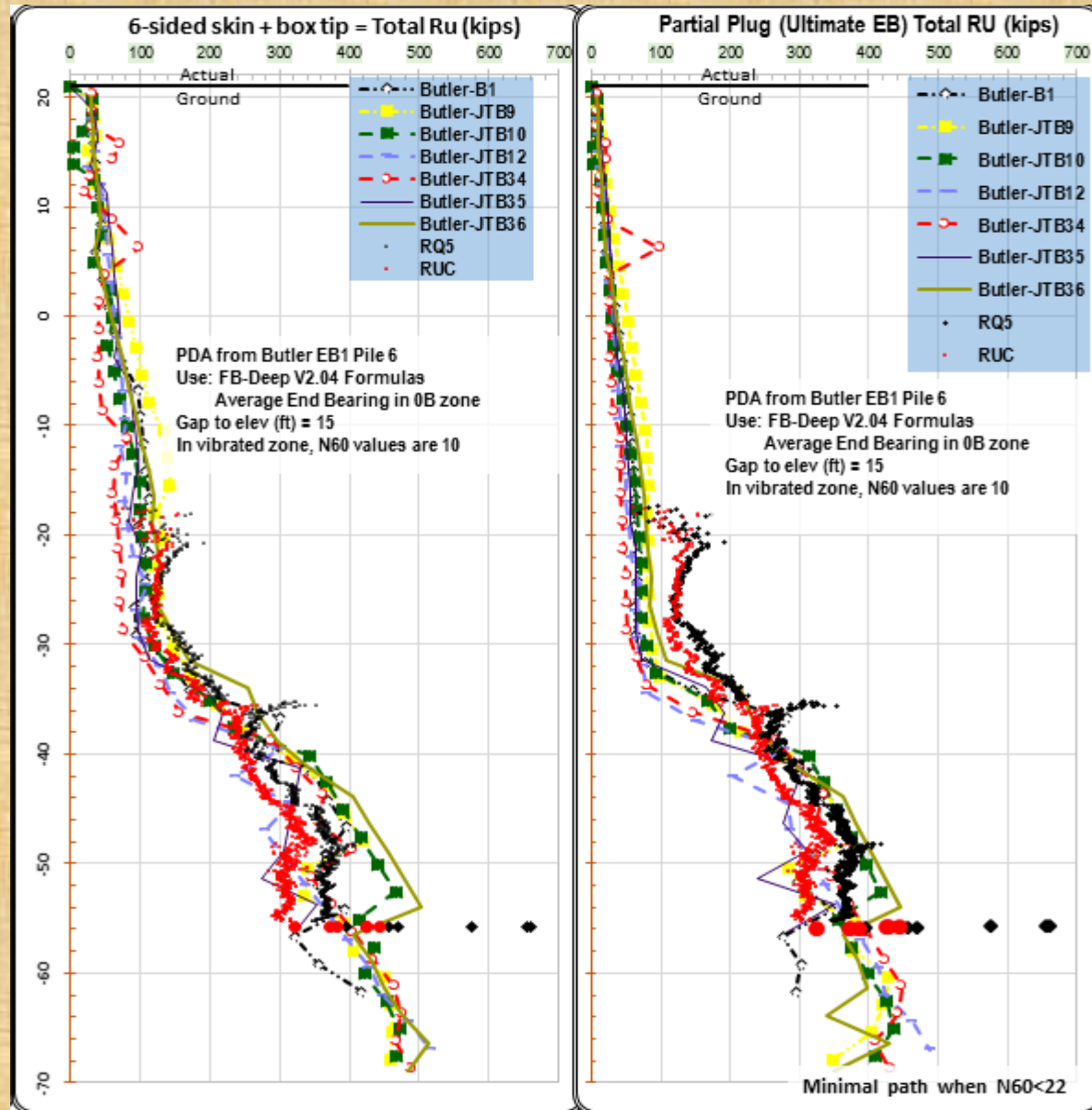
Corrected mobilized end bearing capacity = **74.68(tons)**



# H Piles Plug Conditions – Case Studies

## 2) I-95 over Butler Blvd (Jacksonville) HP 14x89 with 6.6-k Ram D30-42 Hammer

Predictions of 7 borings  
within 200-ft agree well with  
the PDA results from EB1,  
Pile 6



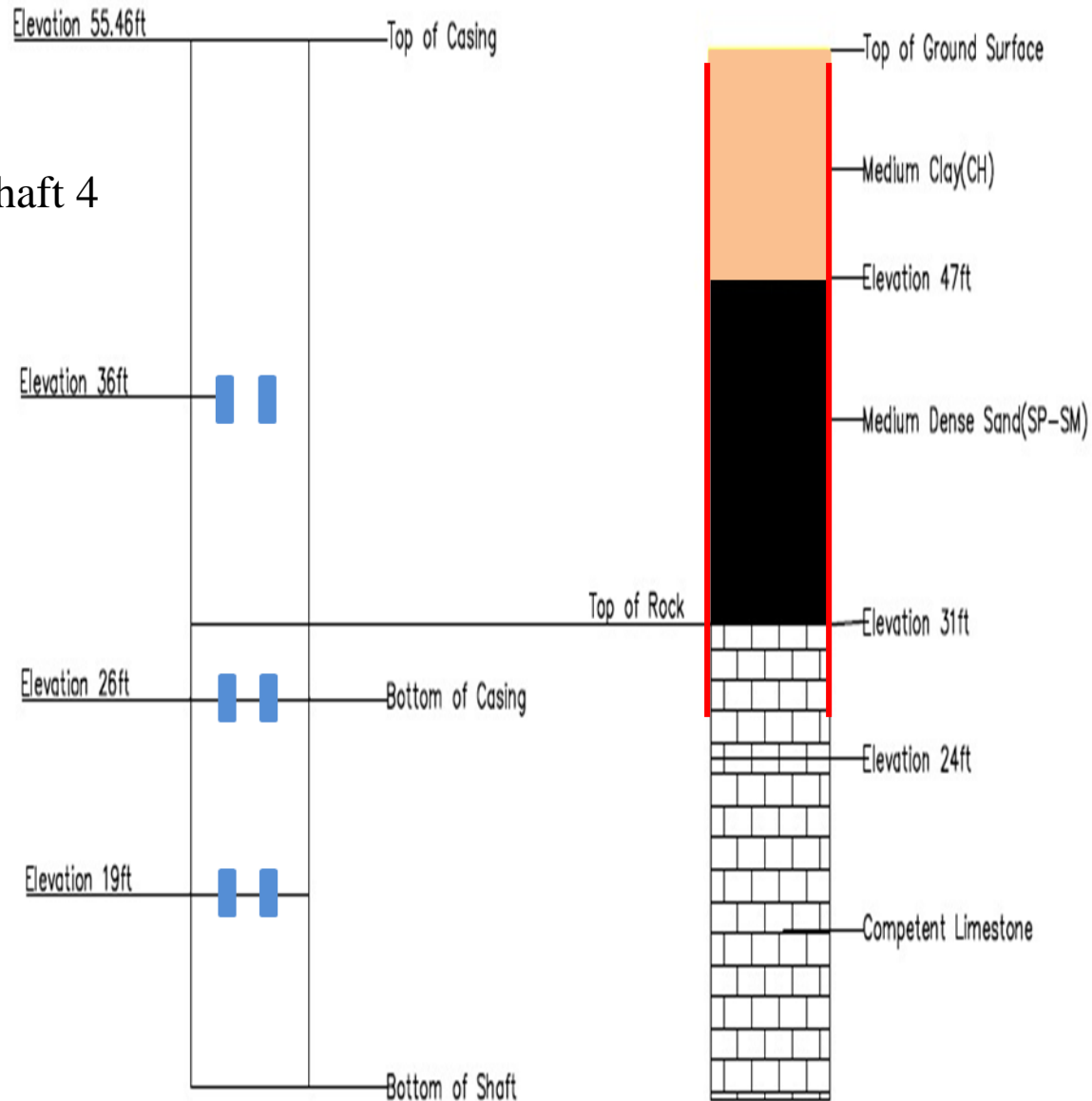
- 1) Let Engineers decide Upper Limit of SPT-N (not default to  $N=60$ ). E.g. Limit of 60, 80, or 100
- 2) If the limestone shelves are thin, let Engineers select Upper Limit of says  $N = 30$  or 35
- 3) Resistance should be included when  $N < 5$ . To be still conservative, this lower limit can be  $N < 2$  or  $N < 3$ . However, it is best for the Engineers to select this Lower Limit as well
- 4) Gap should be included in the analyses
- 5) In the Vibrated Depth, let the Engineers decide to overwrite the SPT-N values (e.g.  $N=10$ )
- 6) Average  $8B+3.5B$  zone and Critical Depth correction maybe suitable for other soil types, but may not be suitable for H piles due to its shape.
- 7) Current formulas (including recently proposed formulas) will need to be further evaluated to best fit the results at other analyzed sites.
- 8) It appears that the following 2 models best reflect the PDA EOD results:
  - (i) “6-sided Side Resistance” plus “Box Mobilized End Bearing”
  - (ii) “Partially Plugged Side Resistance” plus “Partially Plugged Ultimate End Bearing”
- 9) All other models produce much lower capacity predictions (compared to PDA EOD results)
- 10) For BOR (long term) capacity, let the Engineers enter the setup factors for each layer. FB-Deep will then have 2 curves: EOD and Longterm. Example: Sand (Soil 3) –  $A_0 = 1$  to 1.2  
Silt (Soil 2) –  $A_0 = 1$  to 1.5  
Limestone (Soil 4) –  $A_0 = 1$  to 2  
Clay (Soil 1) –  $A_0 = 1.2$  to 2



# Side Friction of Cased Drilled Shafts in Limestone

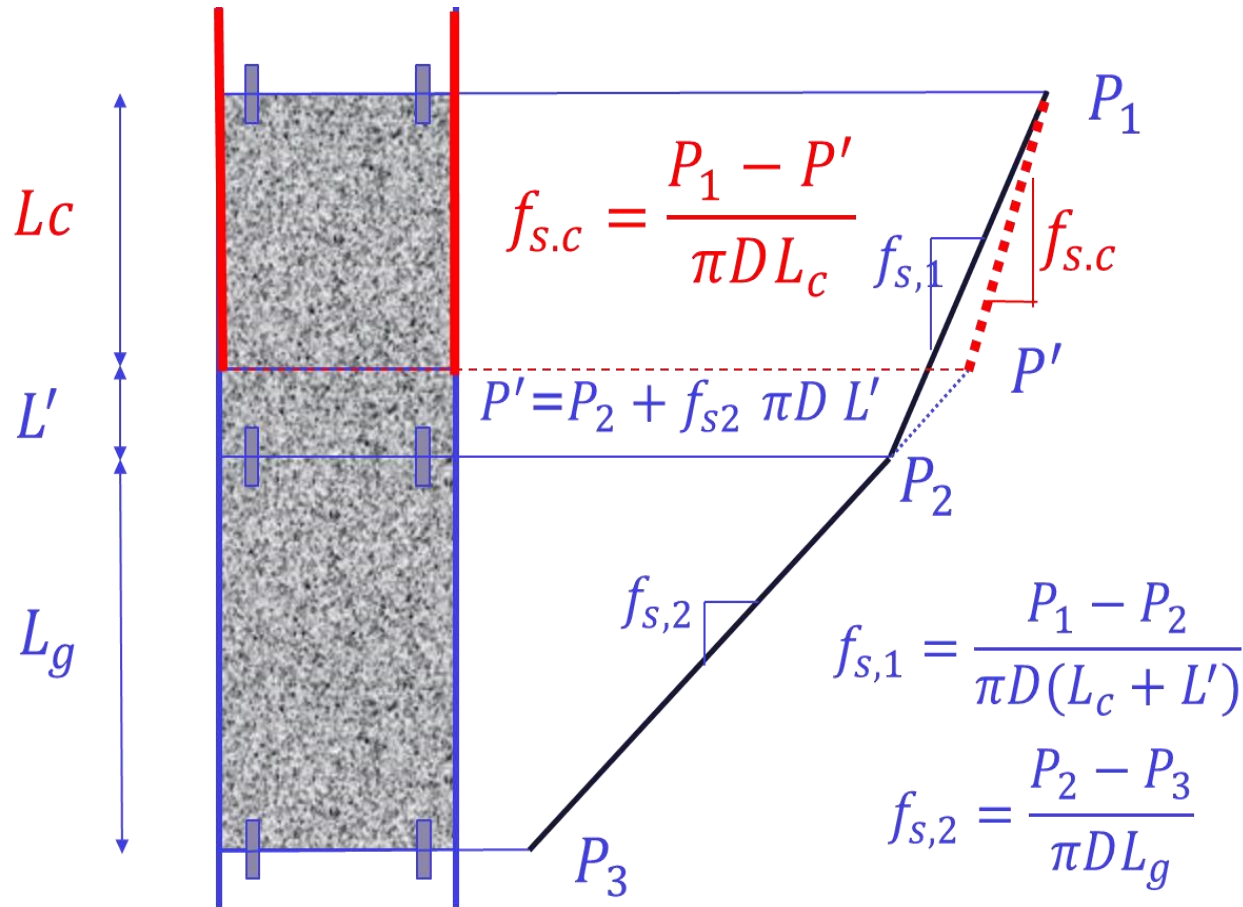
25

Victory Bridge Pier 52 Shaft 4



# Side Friction of Cased Drilled Shafts in Limestone

Casing Ends Between Instrumentation

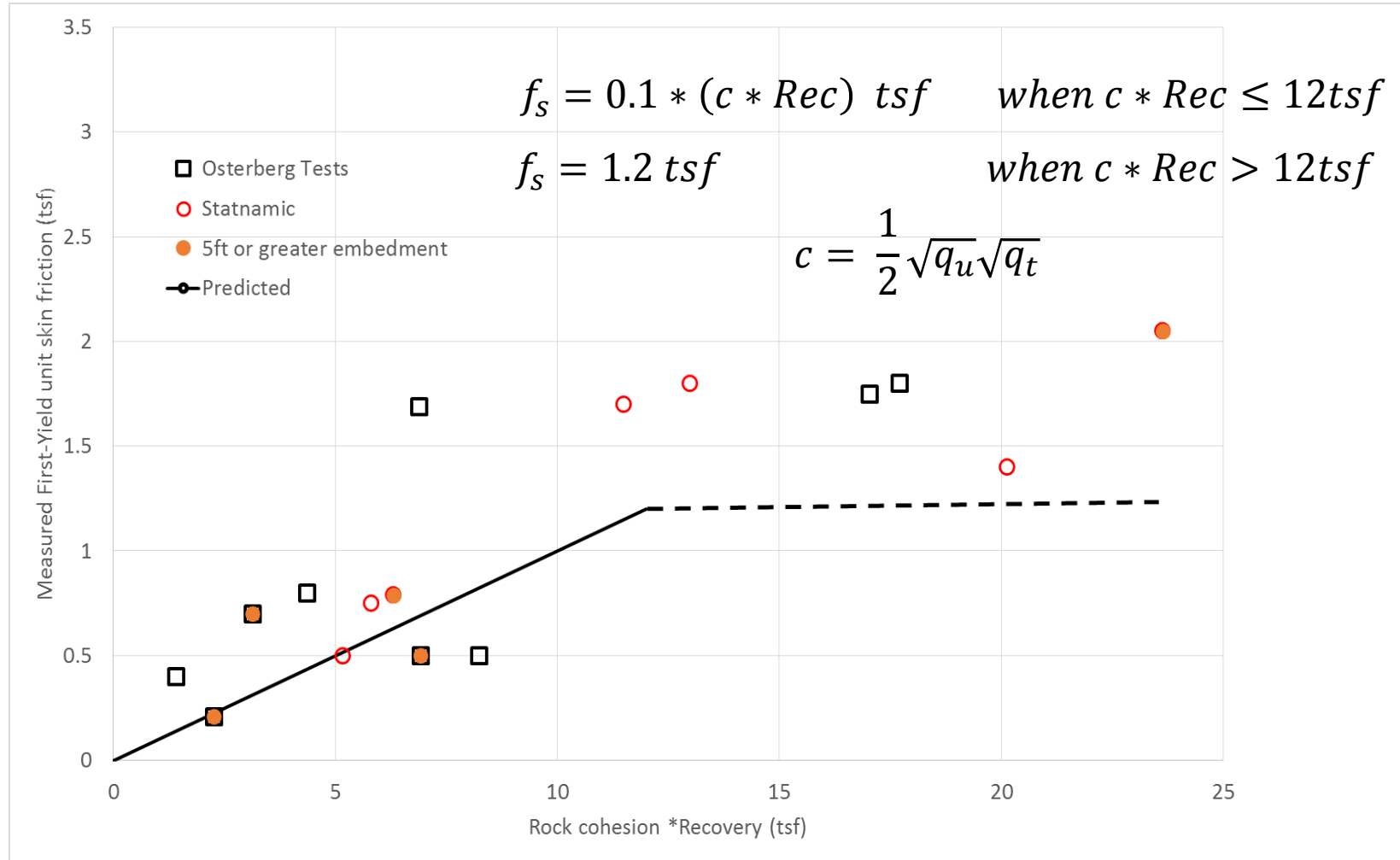


# 7 Sites, 16 Cased Drilled Shafts in Limestone

Project Site	Load Test Shaft	Load Test Method	Embedment Depth in Limestone (ft)	Diameter (ft)	Unit Skin Friction & Displacement in Cased Zone					
					First-Yield		Peak		Residual	
					f <sub>sy</sub> (tsf)	Disp (in.)	f <sub>sp</sub> (tsf)	Disp (in.)	f <sub>sR</sub> (tsf)	Disp (in.)
Gandy Bridge	Pier 26 Shaft 2	O-cell	2.5	4	0.5	0.030	1.1	0.321	0.5	0.536
	Pier 52 Shaft 3	Statnamic	1	4	1.7	0.340	2.8	0.488	2.4	0.488
	Pier 91 Shaft 4	O-cell	2.5	4	1.69	0.850	1.7	0.850	1.69	1.200
	Pier 26 Shaft 1	Statnamic	1	4	1.4	0.030	2.5	0.150	2.3	0.588
Victory Bridge	Bent 3 Shaft 2	O-cell	2.03	4	1.8	0.080	3.6	0.835	2.6	1.480
	Bent 3 Shaft 1	O-cell	1	4	1.75	0.090	3.4	1.549	2.7	1.965
	Test Shaft #5	Statnamic	5	4	2.05	0.030	2.9	0.472	2.9	0.472
Hillsborough Avenue	Pier 4 Shaft 4-1	O-cell	5	4	0.7	0.080	0.8	0.260	0.65	0.499
	Pier 4 Shaft 4-2	O-cell	3.7	4	0.8	0.170	1.17	0.498	1.17	0.498
	Pier 5 Shaft 10	Statnamic	10.33	4	0.79	0.220	1.06	0.465	1.06	0.465
Lee Roy Selmon	Test Shaft #3	Statnamic	4.4	4	1.8	0.400	2.4	1.290	2.4	1.290
17 <sup>th</sup> Street	LTSO-1	O-cell	9.2	4	0.5	0.020	0.91	0.071	0.91	0.071
	LTSO-2	O-cell	18.5	4	0.21	0.040	0.23	0.057	0.23	0.057
Apalachicola River	Pier 59, TS#8	O-cell	3	9	0.4	0.100	0.82	0.574	0.82	0.574
Jewfish Creek	Test Shaft #1	Statnamic	2	4	0.5	0.022	1.5	0.215	1.5	0.215
	Test Shaft #2	Statnamic	2.5	4	0.75	0.037	1.05	0.072	0.75	0.264

# Side Friction of Cased Drilled Shafts in Limestone

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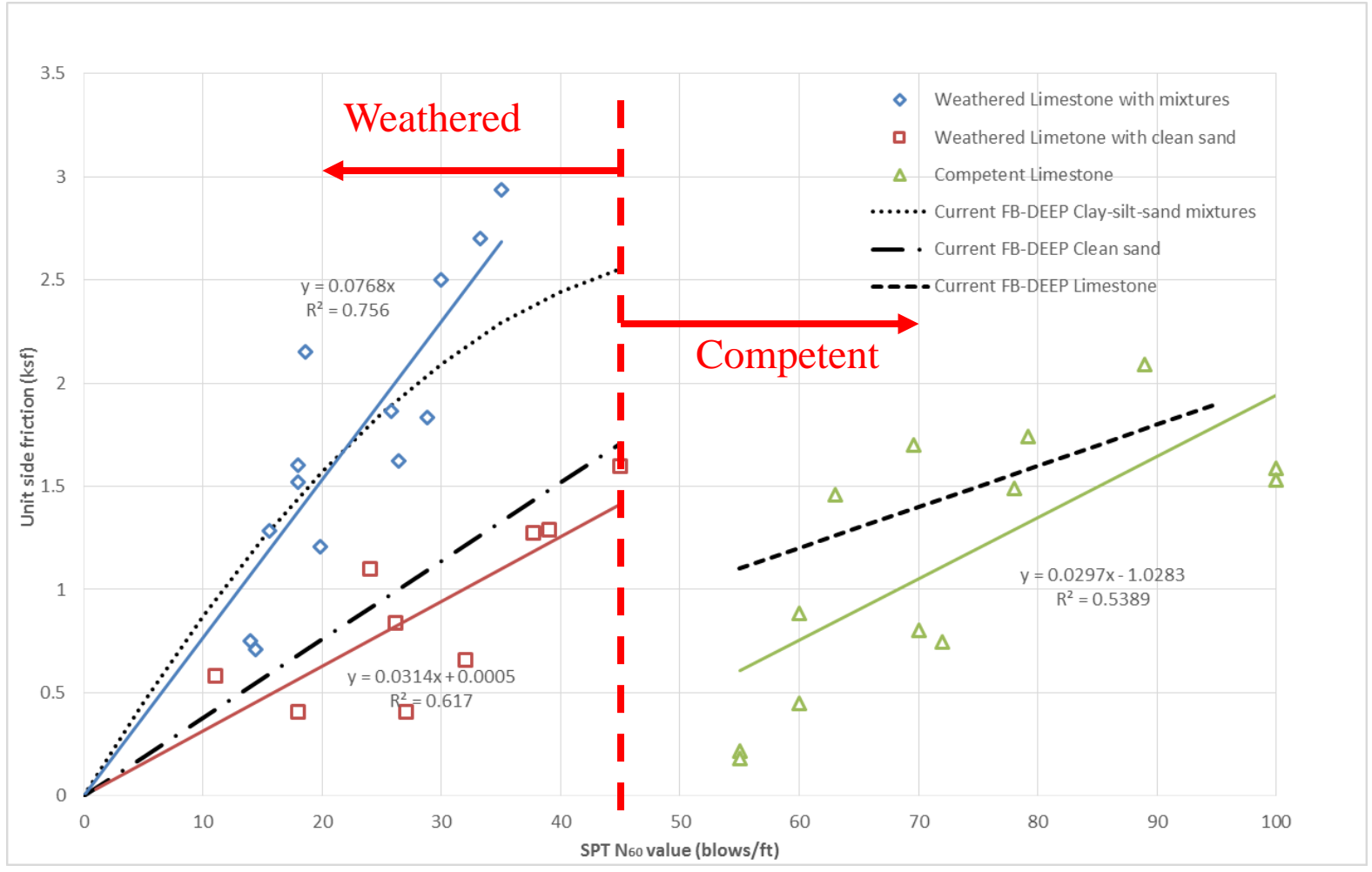


Sites with Prestressed Concrete Piles Evaluated in Florida:

Site Information		Insitu Information		Pile Information		
Project Number (Financial)	Project Site	# of Soil Borings	Predominant Soil Type	Dimensions (in)	Length (ft)	# of Piles with CAPWAP
242484-2-52-01	I-4/SR 408	58	Sand	18 & 24	90 - 107	112
210448-2-52-01	San Sebastian Bridge	11	Sand & Clay	24	38 - 111	111
211449-1-52-01	CR 229 over South Prong of St. Mary's River	2	Sand & Clay	18	47 - 90	14
209293-2-52-01, 209294-1-52-01, 209294-9-52-01	SR 98	121	Sand & Rock	24	45 - 119	183
208166-1-52-01	Plantation Oaks Boulevard over SR 23	50	Sand & Rock	18	55 - 100	11
208466-2-52-01	SR 51	6	Clay & Rock	24	73 - 99	5
420809-3-52-01	I-595	234	Sand & Rock	18 & 24	30 - 115	170
213304-3-52-01	I-95 Overland Bridge Replacement	133	Sand & Rock	24	22 - 66	5
406813-6-52-01	CR 245 over Olustee Creek	10	Sand & Rock	24	61 - 69	7
210687-3-52-01	SR 200 North of Callahan	11	Clay & Rock	24	36 - 66	25
429551-1-52-01	SR 200 South of Callahan	31	Sand & Rock	24	46 - 111	33
422796-1-52-01 & 422796-2-52-01	I-95 over Snake Creek	5	Sand & Rock	18	55 - 80	8
		<b>Total # of Soil Borings:672</b>		<b>Total # of Piles with CAPWAP Data: 684</b>		
				<b>Total # of Piles with Limestone Bearing Layer: 264</b>		
				<b>Total # of BOR CAPWAP Analyses on Piles with Limestone Bearing Layer: 65</b>		

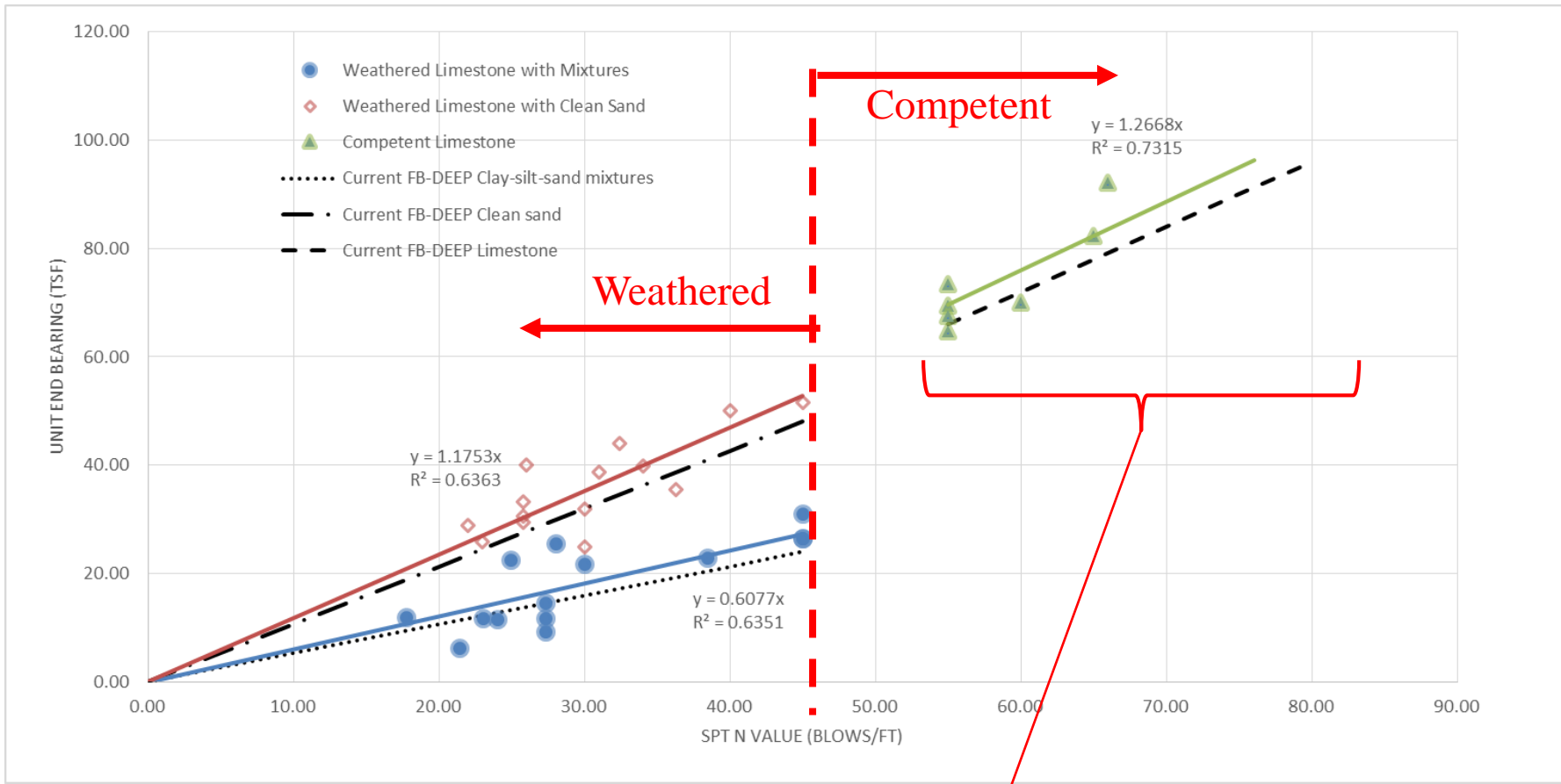
# Analysis of PCP in weathered & Competent Limestone

## Unit Side Friction:



# Analysis of PCP in weathered & Competent Limestone

## Unit End Bearing (Average N – 8B below):



Currently Adding Palmetto Expressway, District 6 (19 Bridges PCP in Limestone)



**Thank You**