

Bottom Side Grouting of Drilled Shafts Prior to Tip Grouting

Civil & Coastal
Engineering

FDOT Contract No.: BDK-75-977-46

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Presentation Overview

- Previous Research
- FDOT Test Chamber
 - Shot Shaft (3' x 6')
 - Long Shaft (3' x 25')
 - Top-Down Test on Long Shaft (3' x 25')
- FDOT Test Site
 - Field Shaft (3-½' x 25')
 - Top-Down Test on Field Shaft (3-½' x 25')
 - Statnamic Test on Field Shaft (3-½' x 25')
- Predicted and Measured Capacities
 - Before Grouting
 - After Grouting

Previous Research

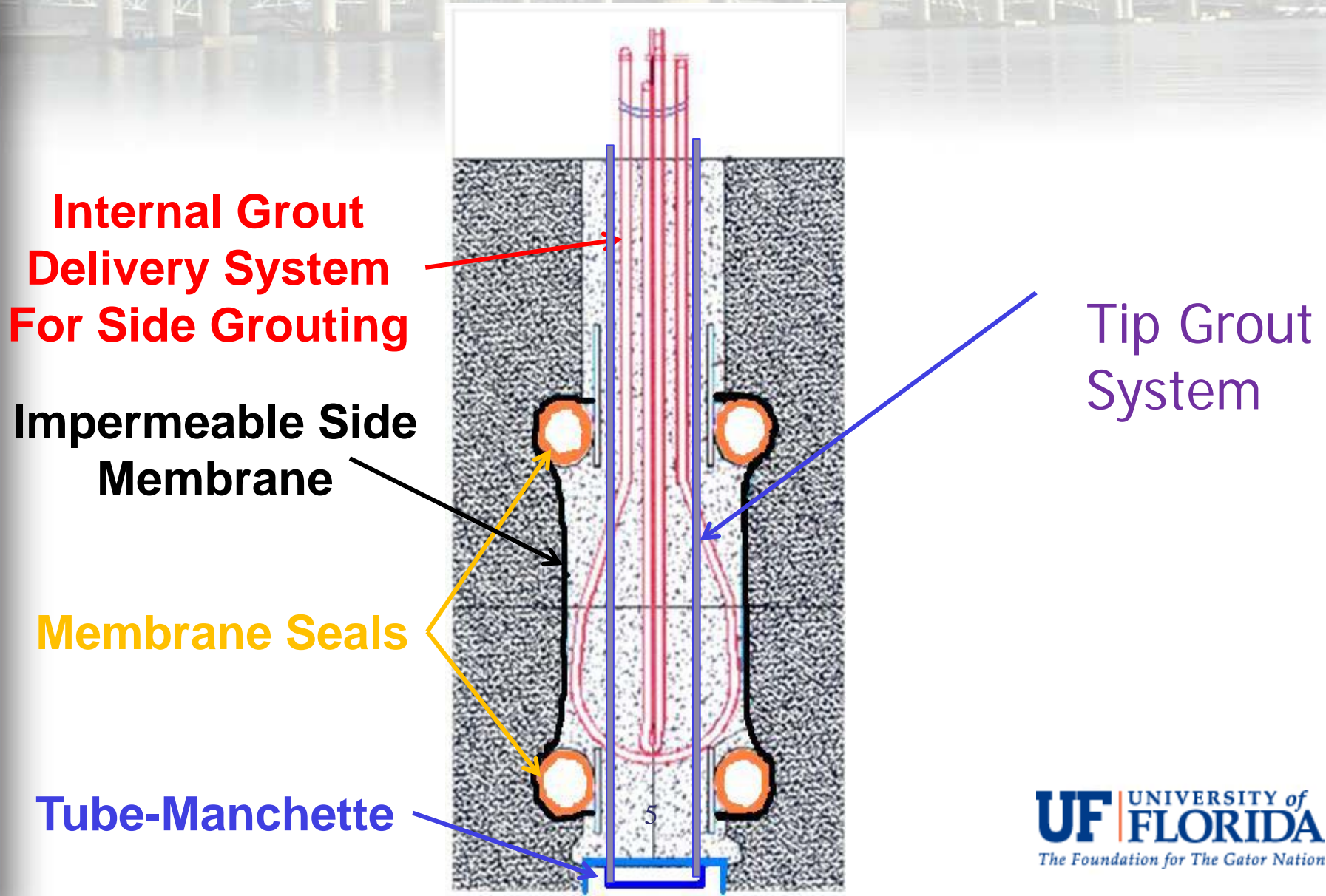
- Post Grouted Drilled Shaft Tips (Mullins, 2001 & 2004)
 - No Side Grouting Prior to Tip Grouting
 - Grout Flows along Path of Least Resistance during Tip Grouting
 - No Cavity Expansion during Tip Grouting
 - Did Not Significantly Improve Soil Conditions around Shaft
 - No Significant Increase in Tip Capacity of Drilled Shaft
- End Bearing Prediction of Post-Grouted Drilled Shaft (No Side Grouting)
 - Mullins, 2006 Method for Tip Grouted Shaft (GP_{max} , GPI, & TCM)
 - Thiyyakkandi (2013) Estimates Tip Area and Tip Pressure – mobilized tip resistance vs. displacement

Previous Research

- Prestressed Concrete Pile Installation – Utilizing Jetting and Pressure Grouting (McVay, 2009)
 - No Side Membrane Initially (Side Grout Ports Only)
 - Grout Followed Path of Least Resistance during Tip Grouting
 - Tested Flexible and Semi-Rigid Membranes
 - Improved Contact Area between Grout and Foundation Element
- Piles Group Efficiencies of Grout-Tipped Drilled Shafts and Jet-Grouted Piles (McVay, 2010)
 - Multiple Grouting Phases using Different Color Grout (Dyed Grout)
 - Identified Grout Flow during Subsequent Tip Grouting Phases
 - Developed FEM Model and Design Approach for Side Grouted Foundations (K_g Method)

FDOT Test Chamber

Design of Side Grouting System



FDOT Test Chamber

Short Shaft (3' x 6') – Fabrication

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Short Shaft (3' x 6') – Construction

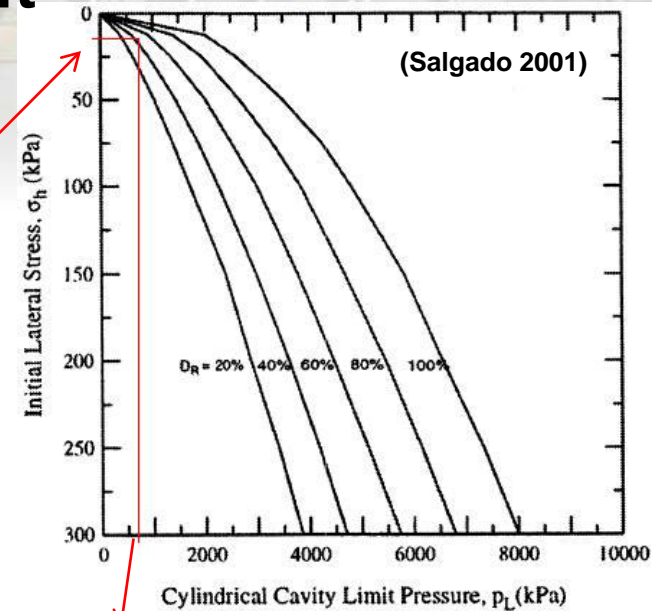
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Short Shaft (3' x 6') – Side Grout

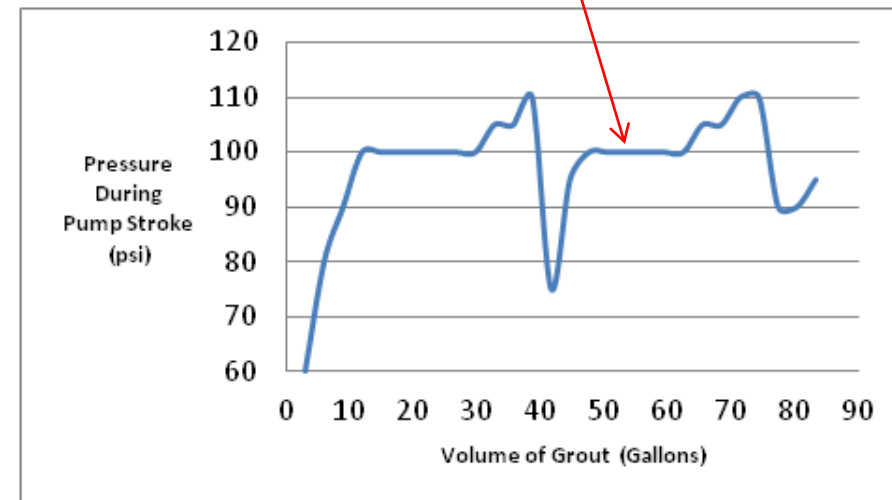
Average Depth of Side Grout Zone = 5'
Initial Lateral Stress, $\sigma_h = \sigma_v * K_0 \approx 1.9 \text{ psi}$
or 13 kPa



700 kPa \approx 102 psi



No Upward Grout Flow

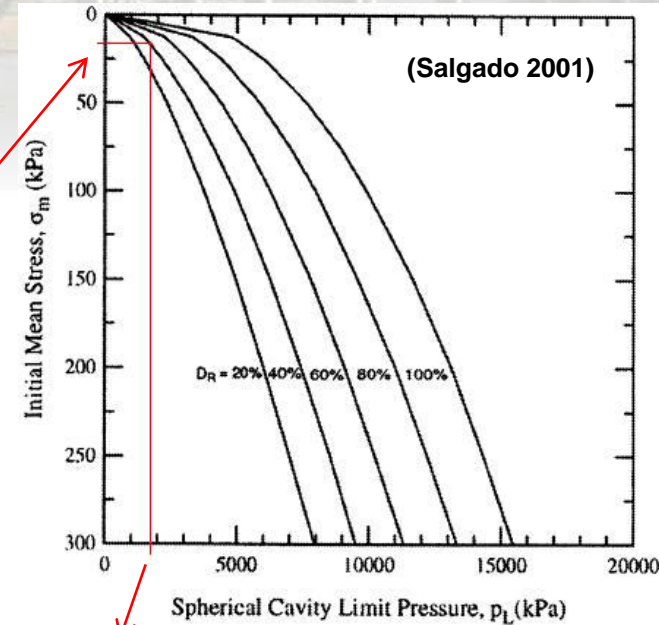


FDOT Test Chamber

Short Shaft (3' x 6') – Tip Grout

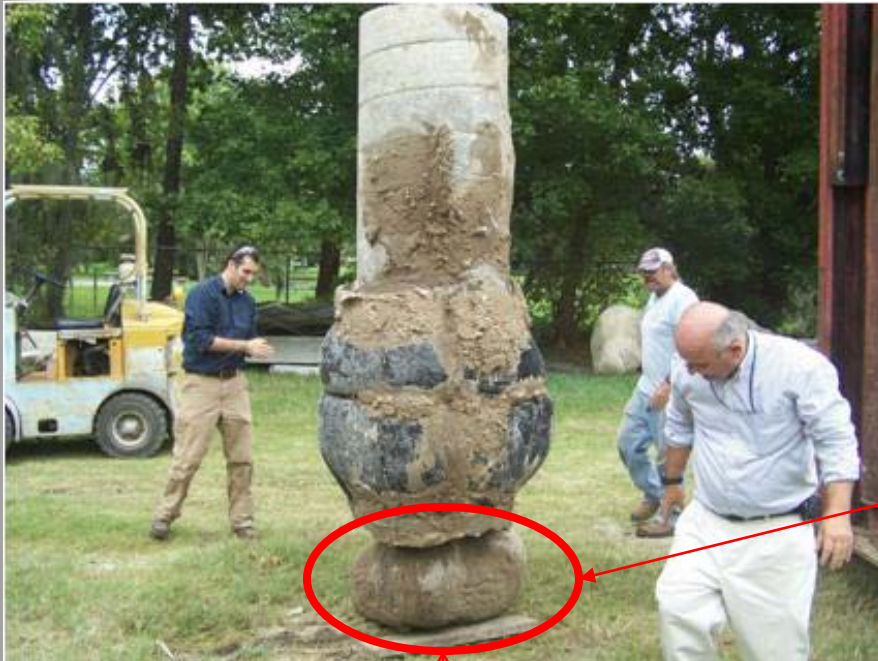
Depth of Tip Grout Zone = 6'

$$\text{Initial Mean Stress, } \sigma_m = \frac{(2 \cdot \sigma_h) + \sigma_v}{3} \approx 3 \text{ psi or } 20 \text{ kPa}$$



1800 kPa \approx 261 psi (Max)

Shaft moved up



Cavity Expansion!

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Long Shaft (3' x 25') – Shaft Casing

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Long Shaft (3' x 25') – Shaft Casing



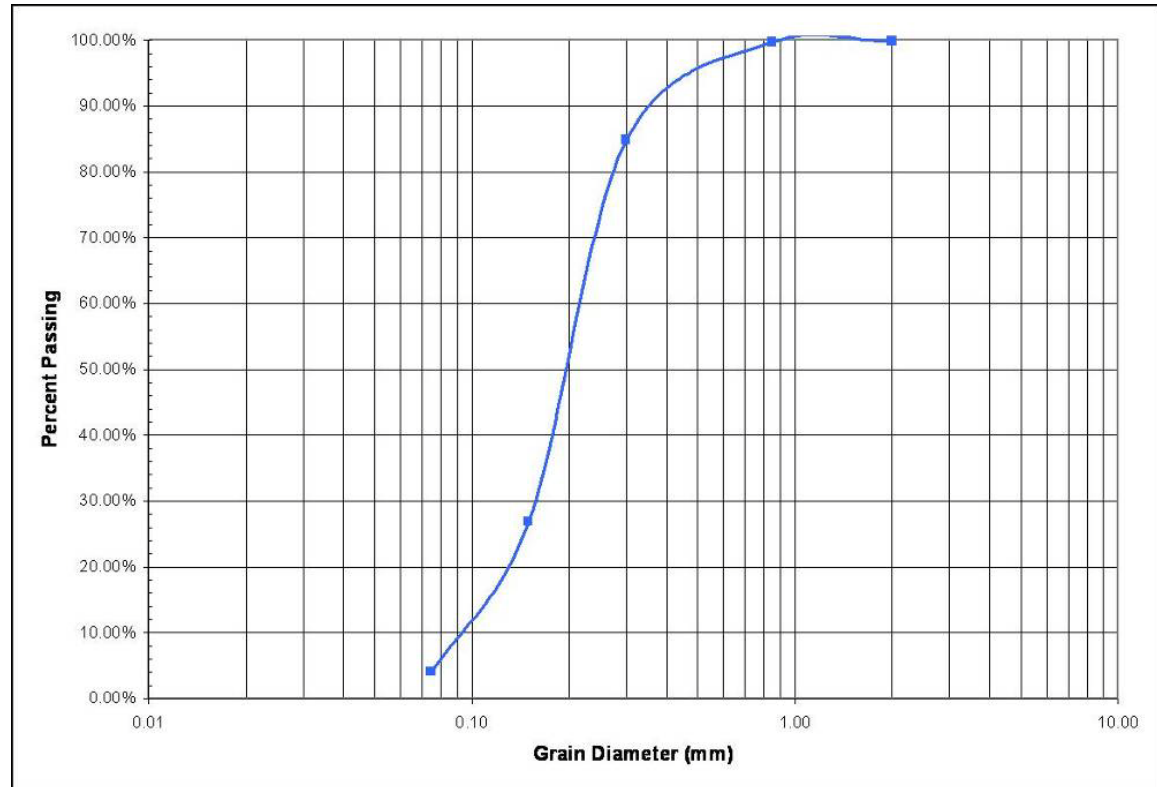
FDOT Test Chamber

Long Shaft (3' x 25') – Soil Placement

**Test Soil: A-2-4
(Silty Sand – from
FDOT Borrow Pit
in Lake City, FL)**

**18 Inch Soil Lifts
8% Moisture Content
50% Relative Density
 $\gamma \approx 110 \text{ lb/ft}^3$ & $\Phi' \approx 33^\circ$**

**SPT Blow Counts:
3 – 5 at 8 ft Depth
15 – 20 at 25 ft Depth**



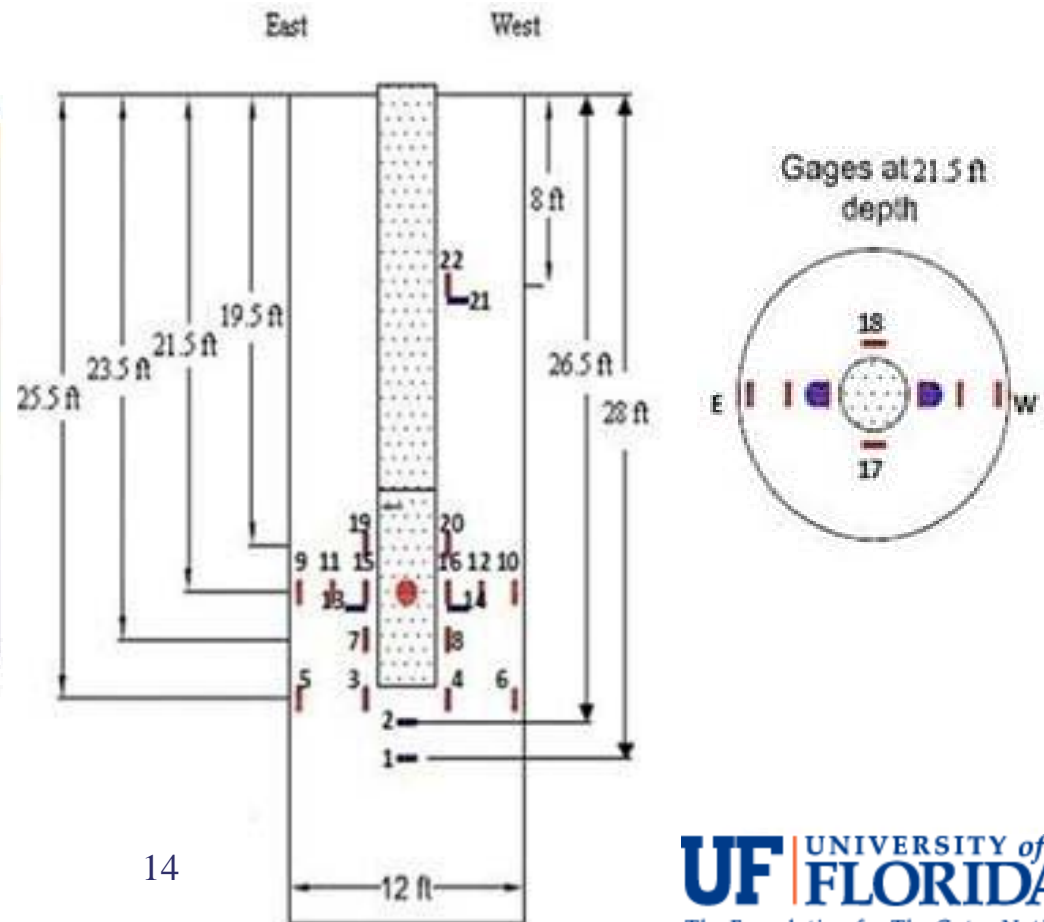
FDOT Test Chamber

Long Shaft (3' x 25') – Soil Placement



FDOT Test Chamber

Long Shaft (3' x 25') – Pressure Cell Placement



FDOT Test Chamber

Long Shaft (3' x 25') – Fabrication

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Long Shaft (3' x 25') – Construction

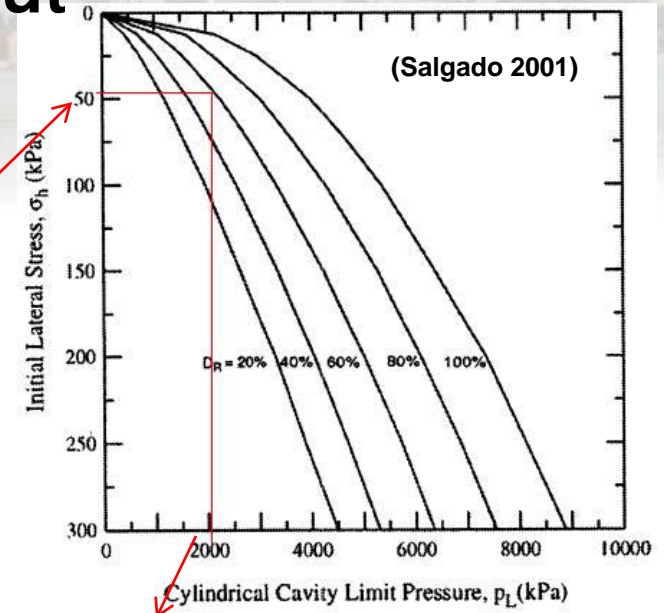
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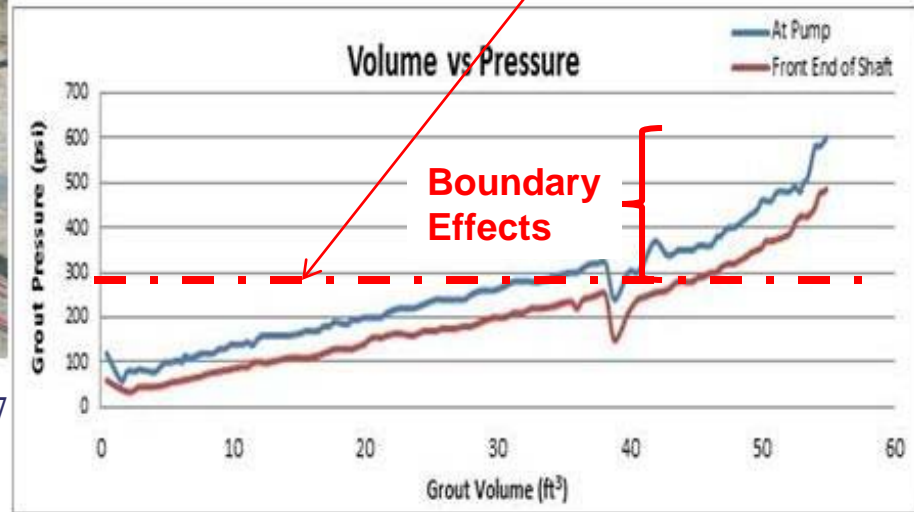
FDOT Test Chamber

Long Shaft (3' x 25') – Side Grout

Average Depth of Side Grout Zone = 20'
 Initial Lateral Stress, $\sigma_h \approx 7$ psi
 or 48 kPa



2050 kPa \approx 297 psi

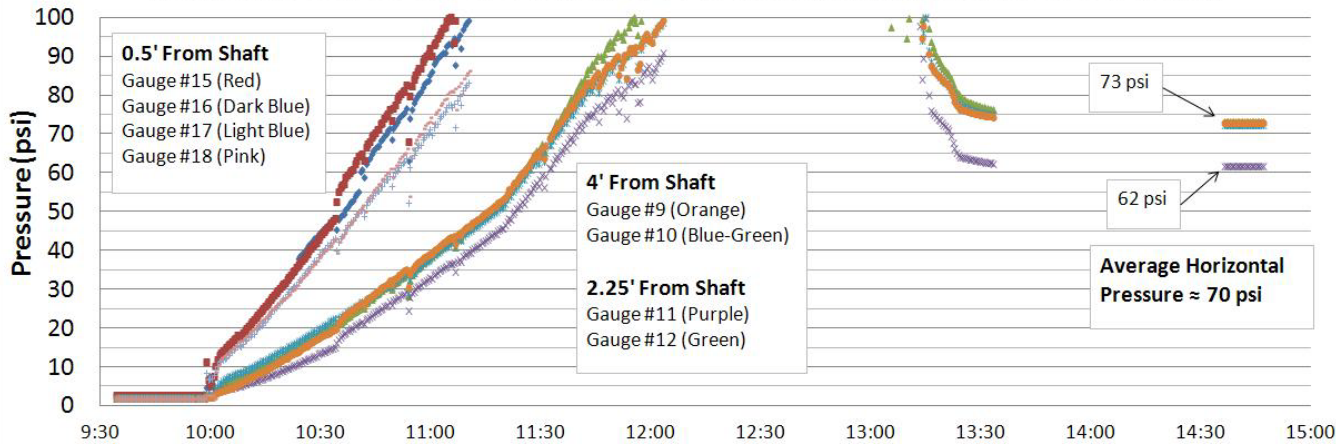


No Upward Grout Flow

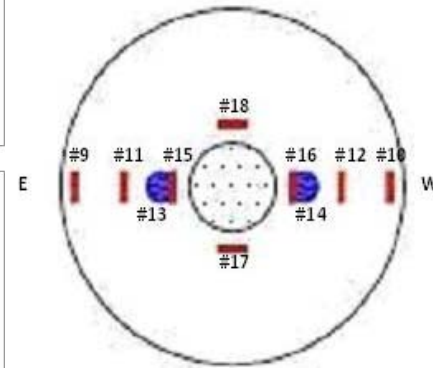
FDOT Test Chamber

Long Shaft (3' x 25') – Side Grout

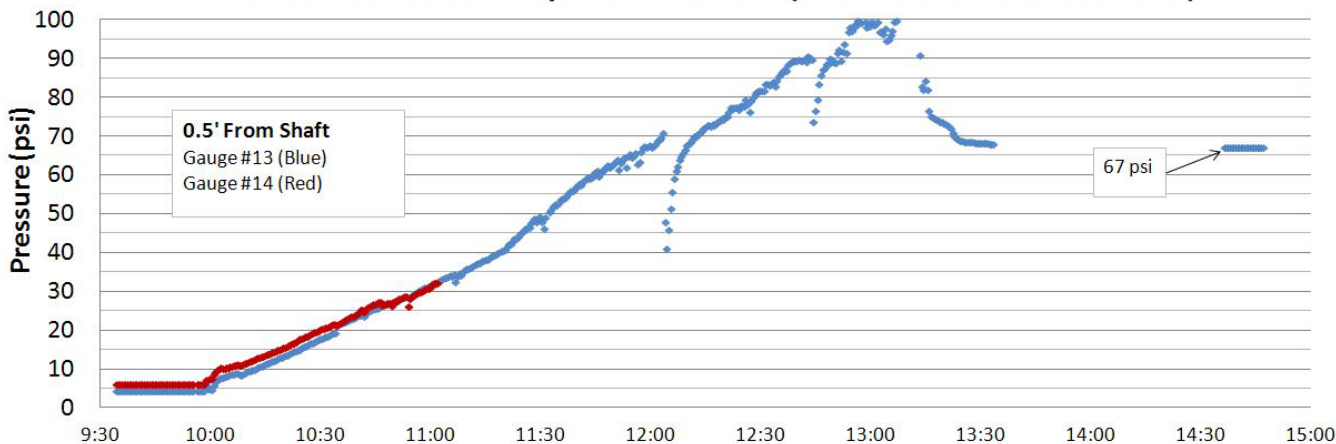
Horizontal Soil Stress at a Depth of 21.5 Feet (Middle of Side Grout Zone)



Pressure Cells at
Depth of 21.5'
(Middle of Side
Grouted Zone)



Vertical Soil Stress at a Depth of 21.5 Feet (Middle of Side Grout Zone)

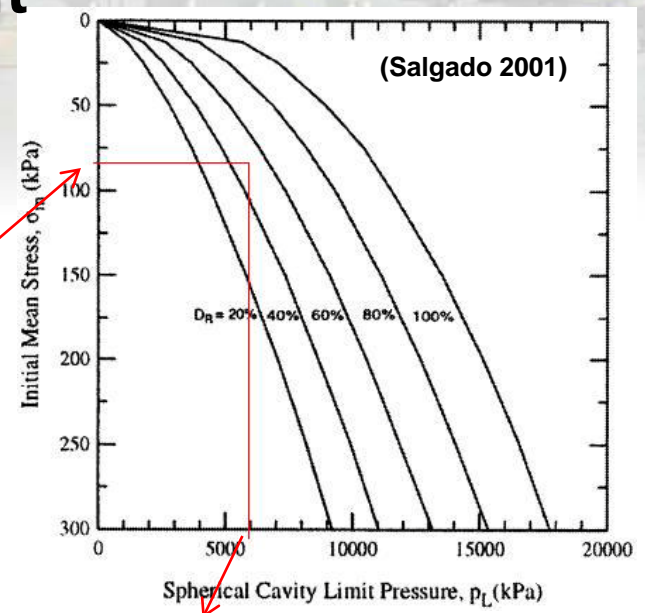


FDOT Test Chamber

Long Shaft (3' x 25') – Tip Grout

Depth of Tip Grout Zone = 25'
 Initial Mean Stress, $\sigma_m = \frac{(2 \cdot \sigma_h) + \sigma_v}{3}$

≈ 12 psi
 or 83 kPa

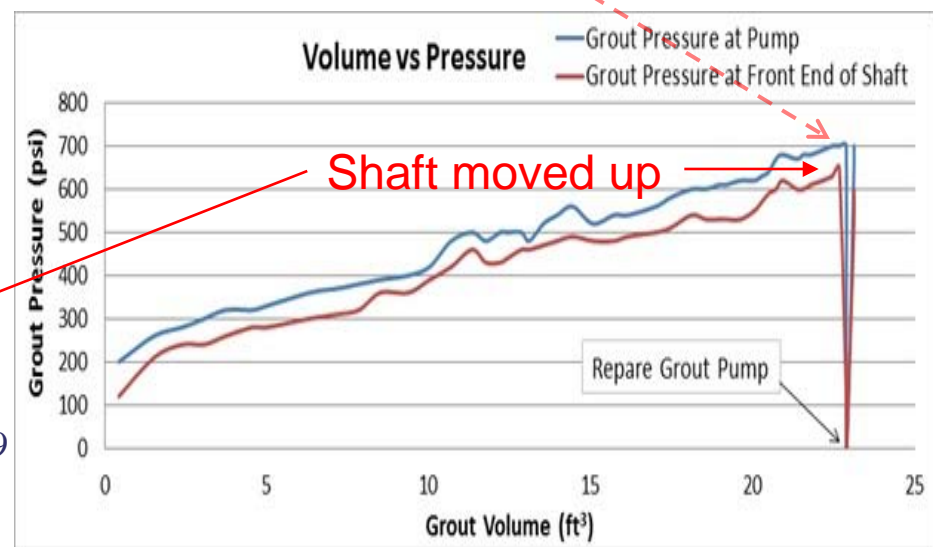


5900 kPa ≈ 856 psi (Max)



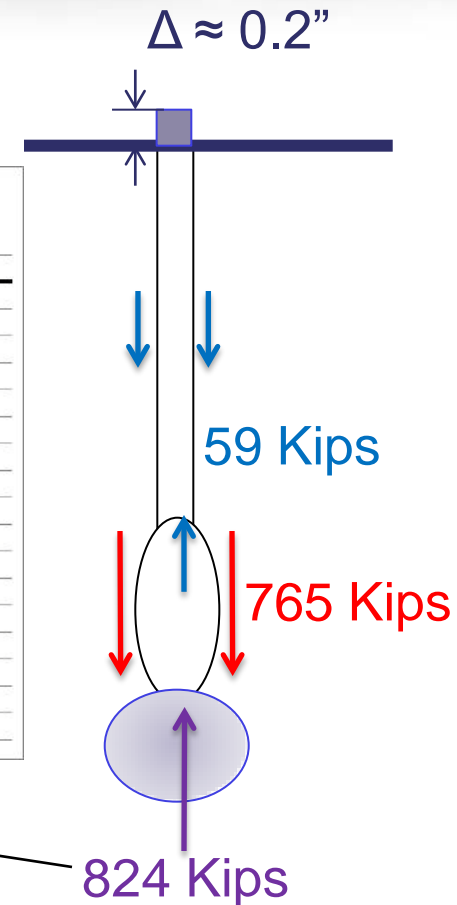
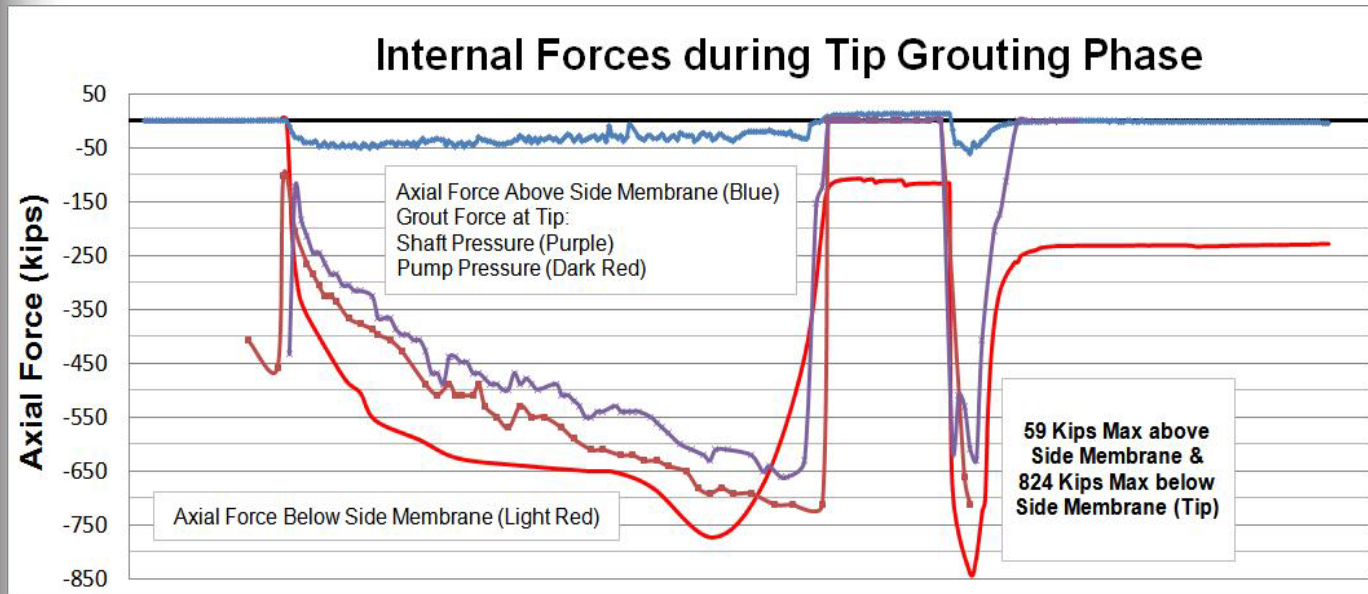
0.4" Upward Shaft Movement
 (0.2" Differential Movement with Soil)

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FDOT Test Chamber

Long Shaft (3' x 25') – Tip Grout



Shaft Capacity $\geq 2 \times$ Skin = 1648 Kips

(650 psi Grout Pressure
& 1267 in² Tip Area)

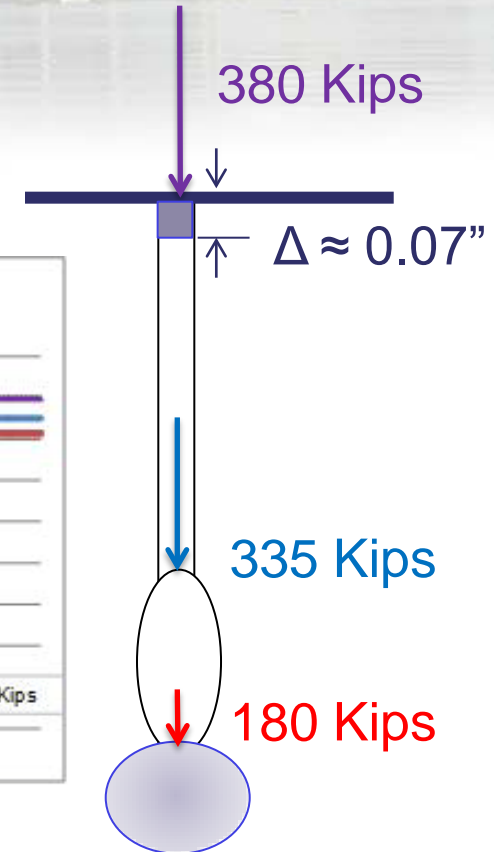
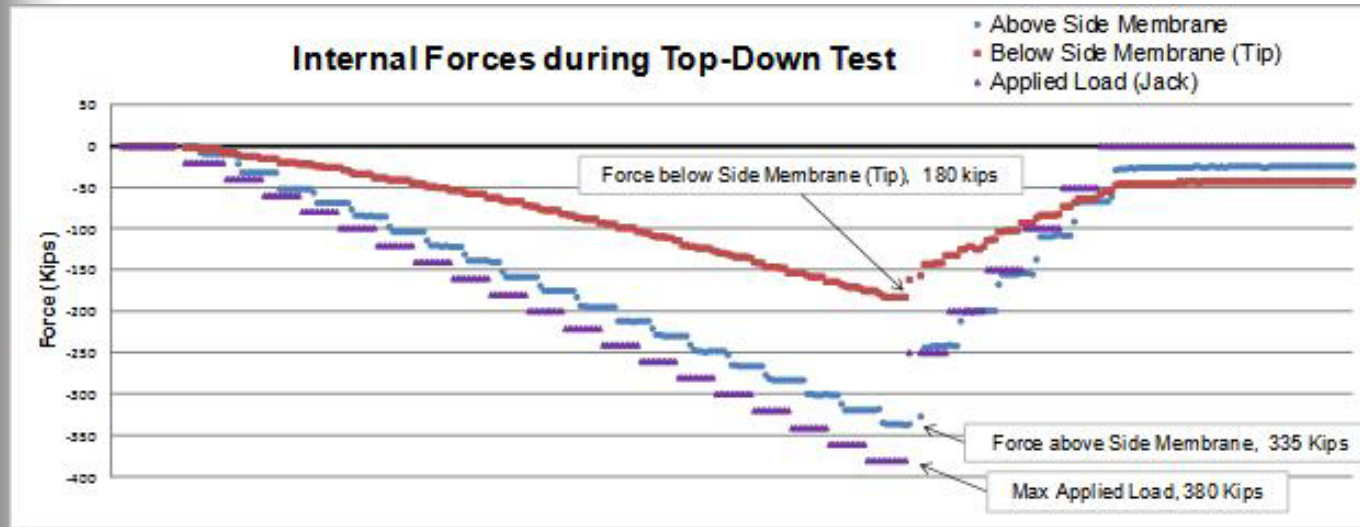
FDOT Test Chamber

Long Shaft (3' x 25') – Top-Down Test



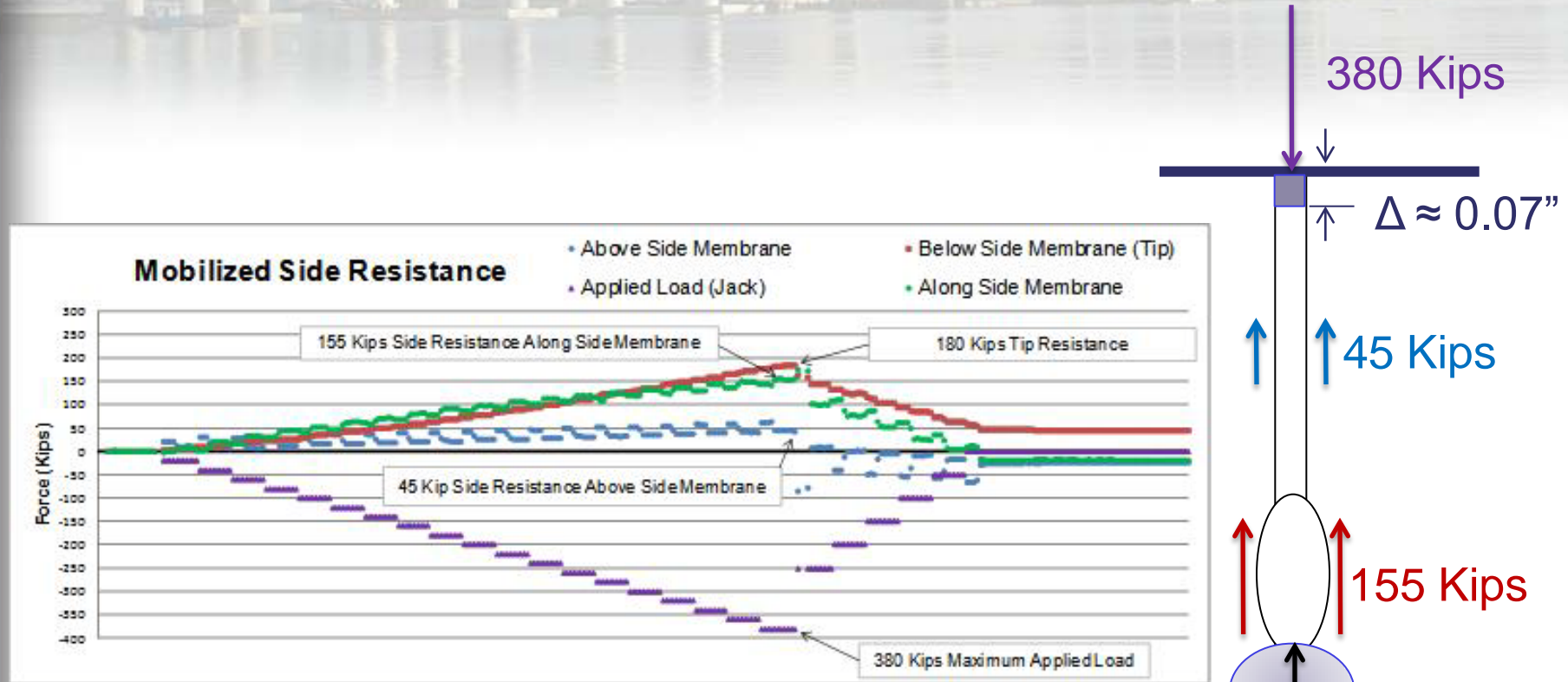
FDOT Test Chamber

Long Shaft (3' x 25') – Top-Down Test



FDOT Test Chamber

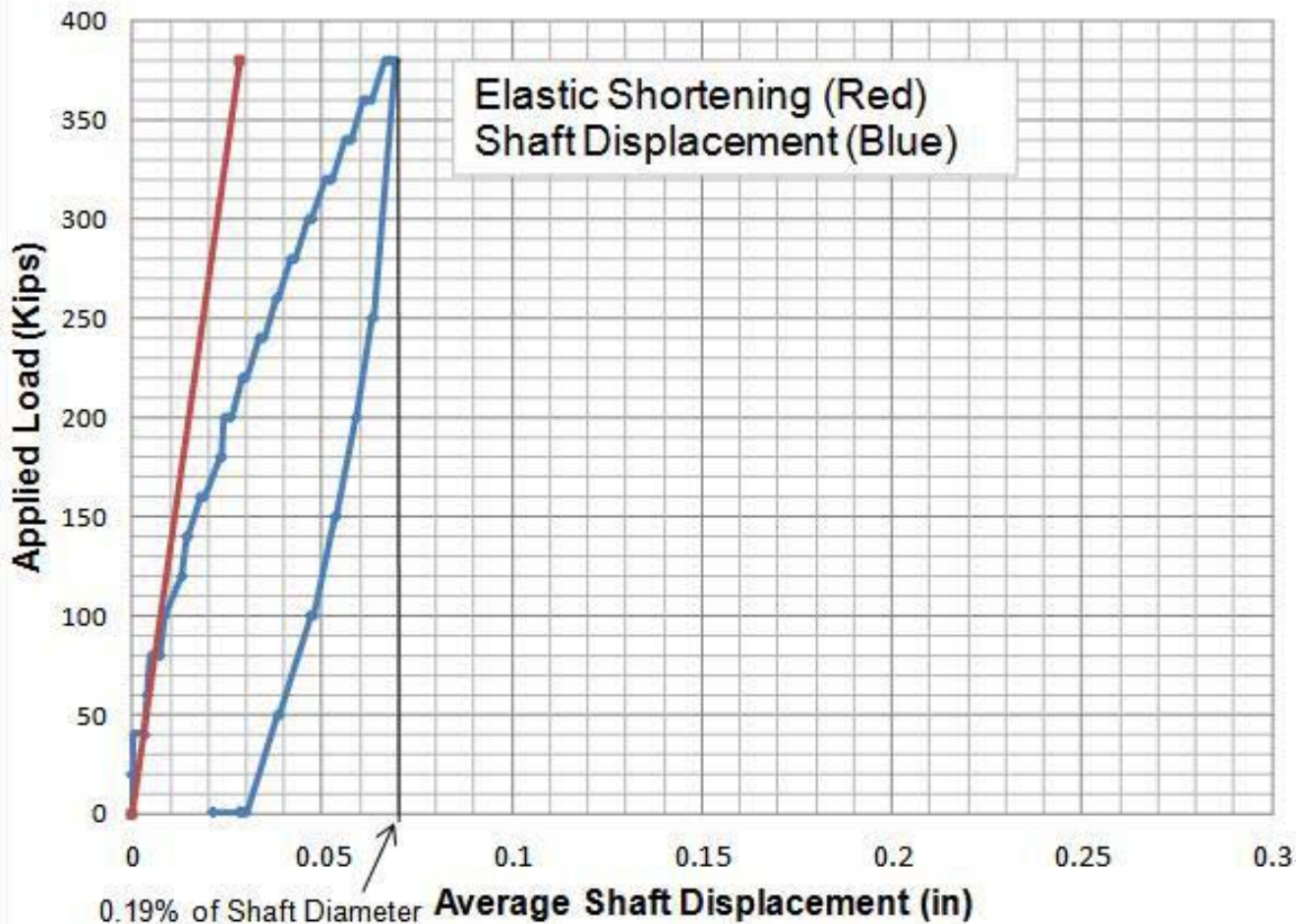
Long Shaft (3' x 25') – Top-Down Test



**40% of Applied
Load Carried by
Side Grouted
Zone!!!**

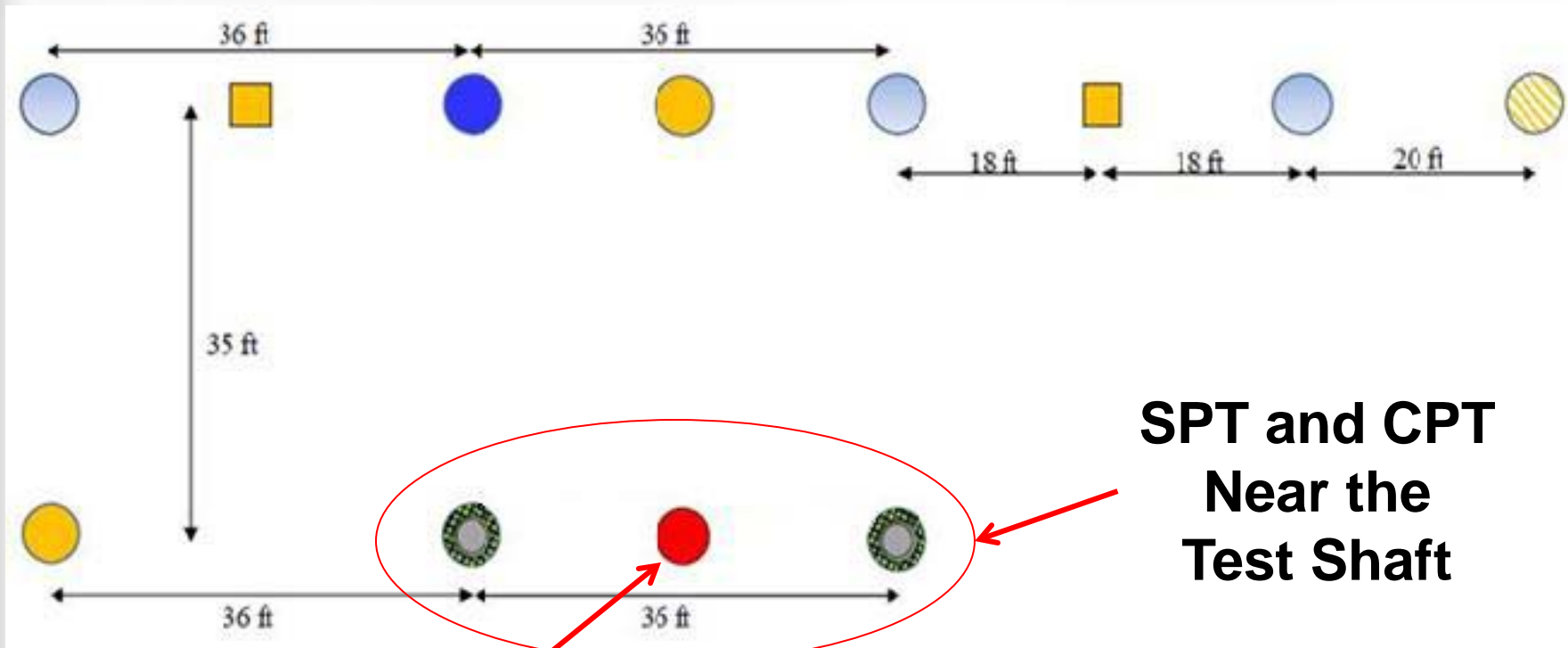
FDOT Test Chamber

Long Shaft (3' x 25') – Top-Down Test



FDOT Test Site

Field Shaft (3-1/2' x 25') – Site Layout

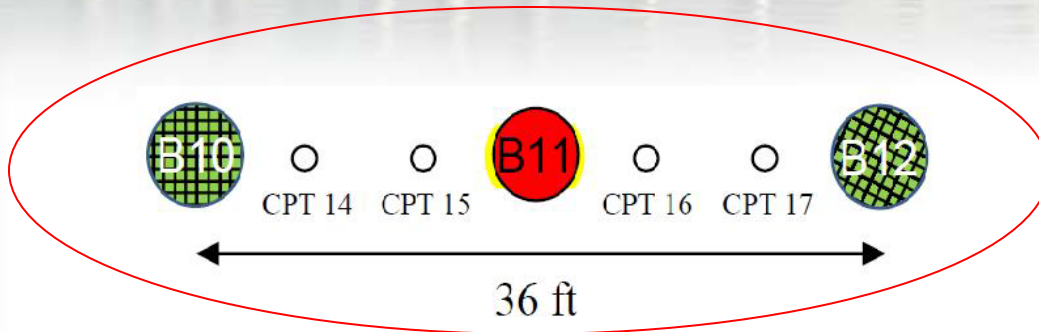


**SPT and CPT
Near the
Test Shaft**

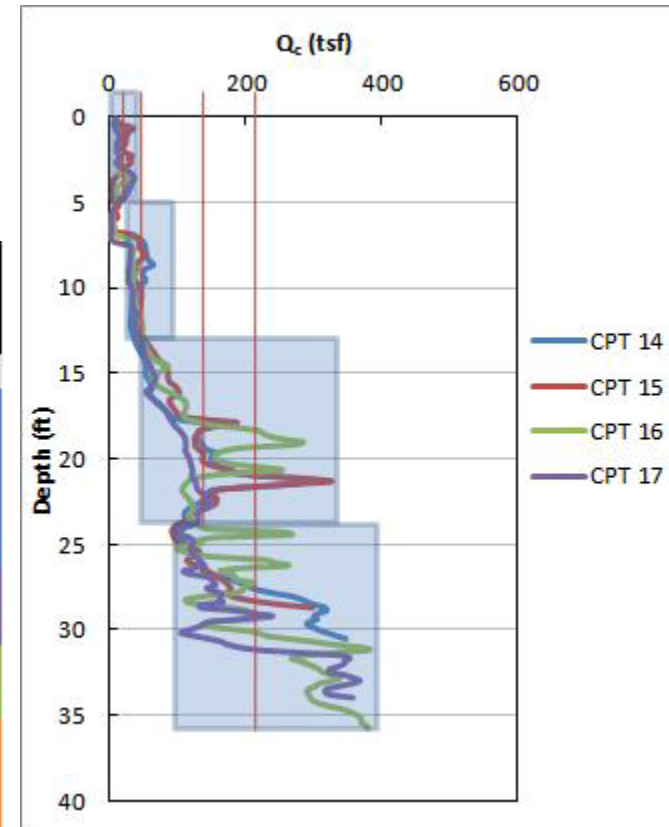
**Side and Tip
Grouted Drilled
Shaft**

FDOT Test Site

Field Shaft (3-½' x 25') – Soil Layers

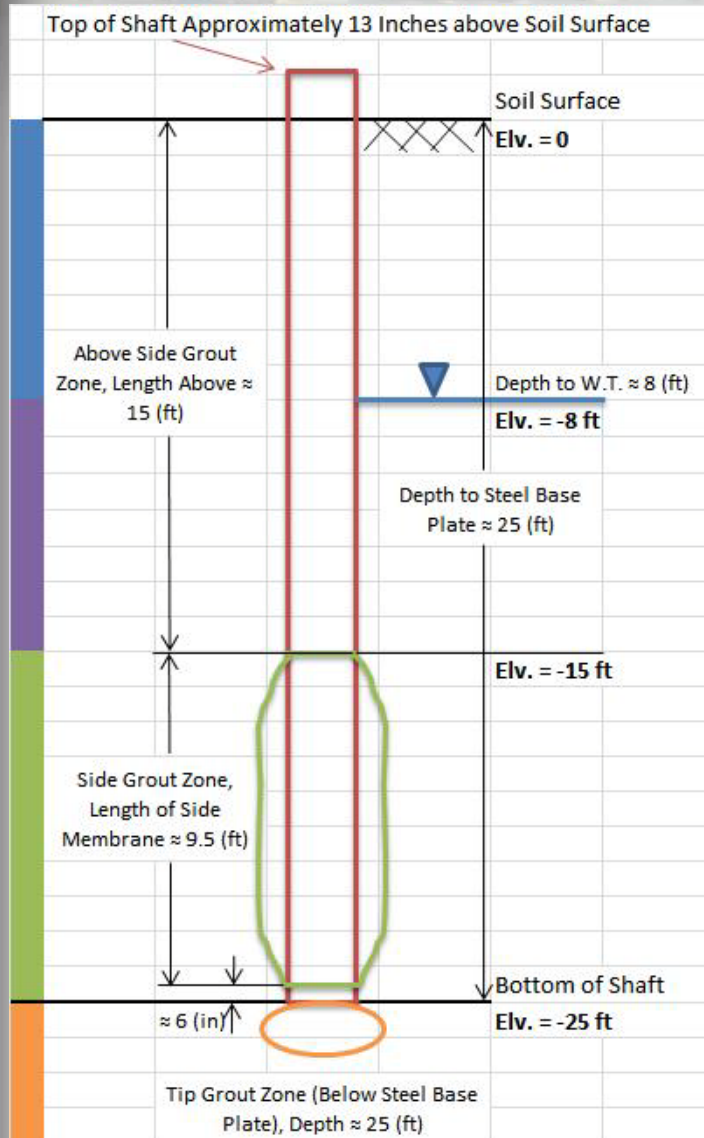


SAMPLE NUMBER	SAMPLE DEPTH (ft)	AASHTO CLASS	UNIFIED CLASS	SPT N-Value	Avg SPT N-Value	Soil Layers
B11						
1	1.0 - 2.5	A-2-6	SC	5	6.0	1
2	2.5 - 4.0	A-7-6	CH	7		
3	4.0 - 5.5	A-7-6	CH	5		
4	5.5 - 7.0	A-6	SC	6		
5	7.0 - 8.5			7		
6	8.5 - 10.0	A-3	SP-SM	6	5.5	2
7	13.5 - 15.0	A-3	SP	5		
8	18.5 - 20.0	A-3	SP-SM	19	16.0	3
9	23.5 - 25.0	A-3	SP	13		
10	28.5 - 30.0	A-3	SP	27	55.0	4
11	33.5 - 35.0	A-3	SP-SM	54		
12	38.5 - 40.0	A-3	SP	84		



FDOT Test Site

Field Shaft (3-1/2' x 25') – Soil Properties



Soil Layer (#)	Depth (ft)	Depth to Mid-Point of Soil Layer (ft)	Peak Friction Angle, ϕ_p	Ultimate Friction Angle, ϕ_u	Moist Unit Weight (lb/ft ³)
1	0 - 8	4	35	---	115
2	8 - 15	11.5	35	---	120
3	15 - 25	20	41.2	36.2	125
4	25 - 40	32.5	41.2	---	130

Soil Layer (#)	Depth (ft)	Vert. Effective Stress, σ_v' (lb/ft ²)	Vert. Effective Stress, σ_v' (lb/in ²)	(1) Lateral Earth Pressure Coef., K_0	Horiz. Effective Stress, σ_h' (lb/ft ²)	Horiz. Effective Stress, σ_h' (lb/in ²)
1	0 - 8	460	3.2	0.43	196.2	1.4
2	8 - 15	1122	7.8	0.43	478.3	3.3
3	15 - 25	1636	11.4	0.34	558.5	3.9
4	25 - 40	2456	17.1	0.34	838.3	5.8

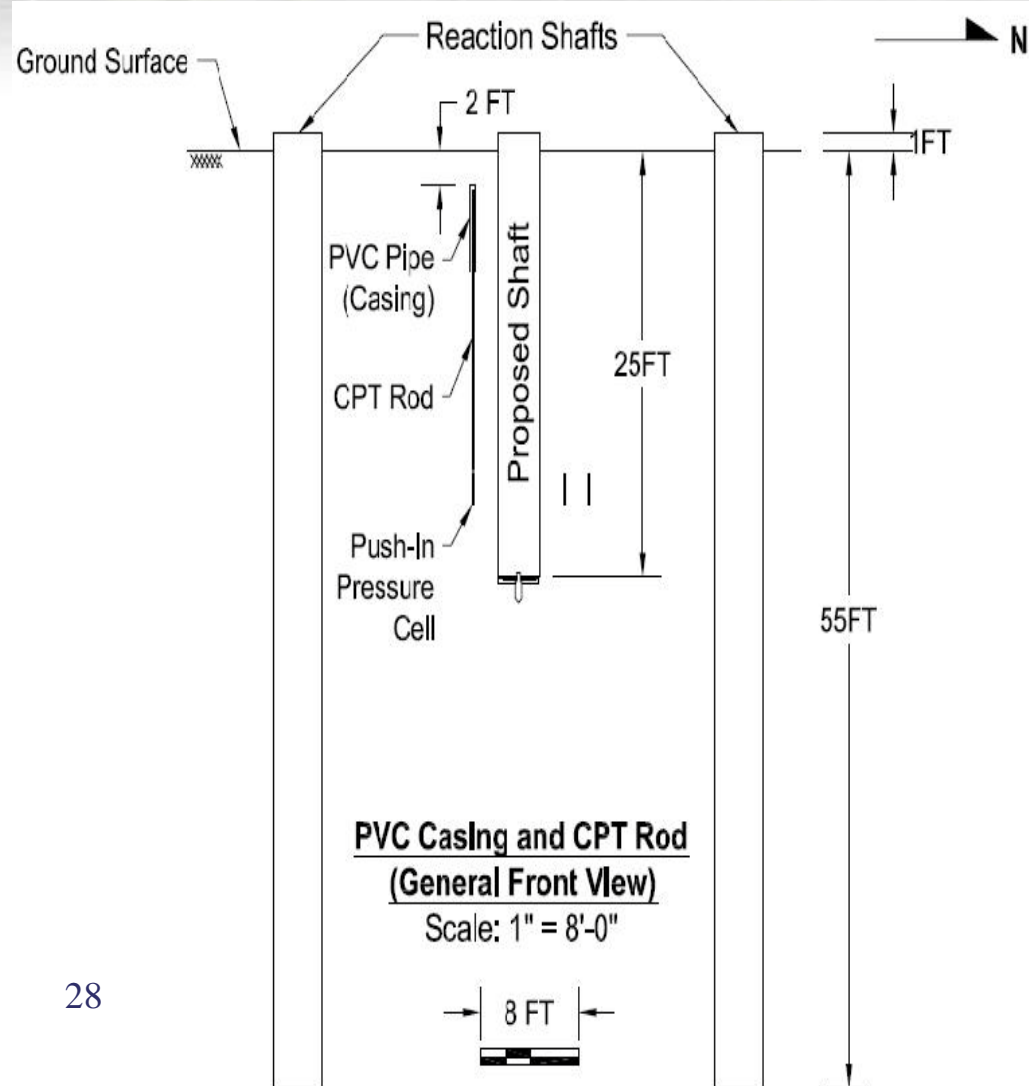
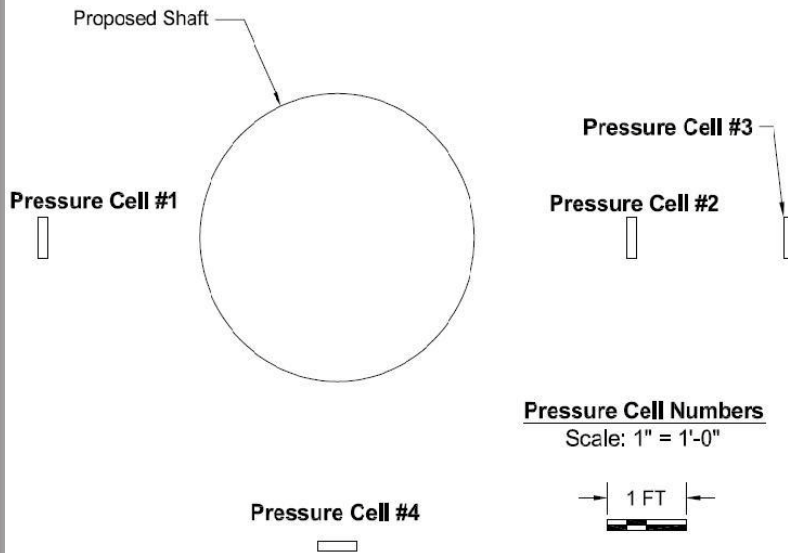
(1) Lateral Earth Pressure Coefficient (Jaky 1960), $K_0 = 1 - \sin(\phi_p)$

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Field Shaft (3-1/2' x 25') – Push-In Pressure Cells



Pressure Cell #5



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Field Shaft (3-1/2' x 25') – Fabrication



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Field Shaft (3-½' x 25') – Construction



FDOT Test Site

Field Shaft (3-½' x 25') – Grouting

Completed Shaft Construction and All Grouting in 2 Weeks!

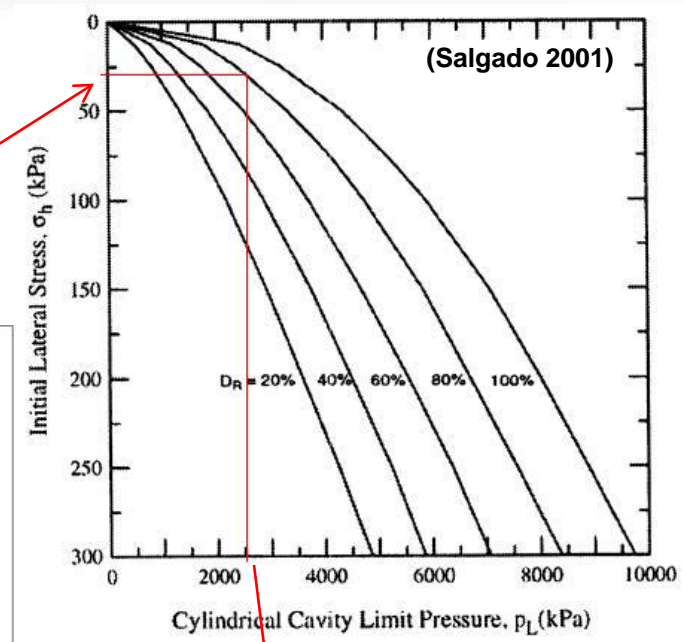
- Grout Membrane Seals (24 hr.)
- Grout Side Membrane (4 & 6 Days)
- Grout Tip (13 Days after Shaft Const.)



FDOT Test Site

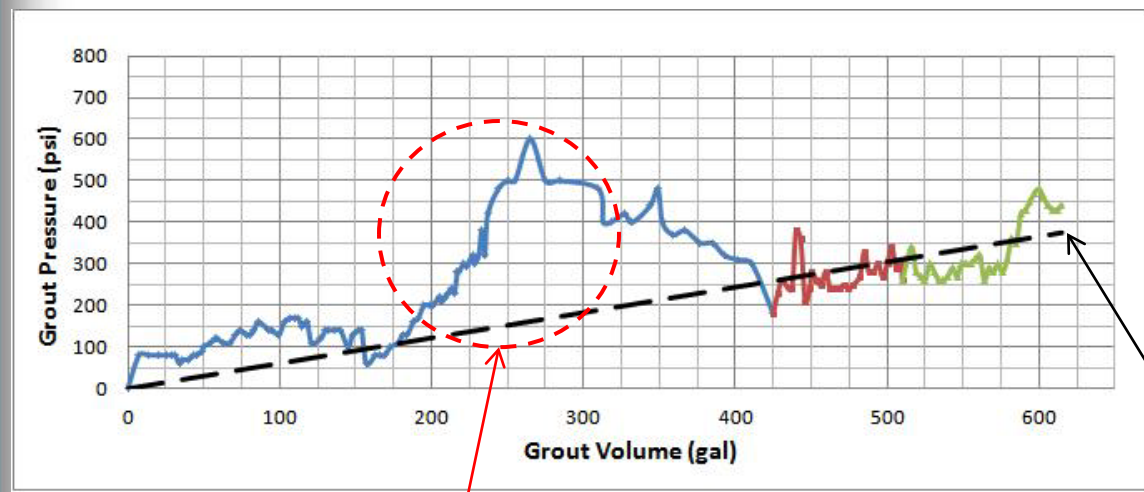
Field Shaft (3-1/2' x 25') – Side Grouting

Average Depth of Side Grout Zone = 20'
 Initial Lateral Stress, $\sigma_h \approx 3.9$ psi
 or 26.7 kPa



2500 kPa \approx 363 psi

375 psi



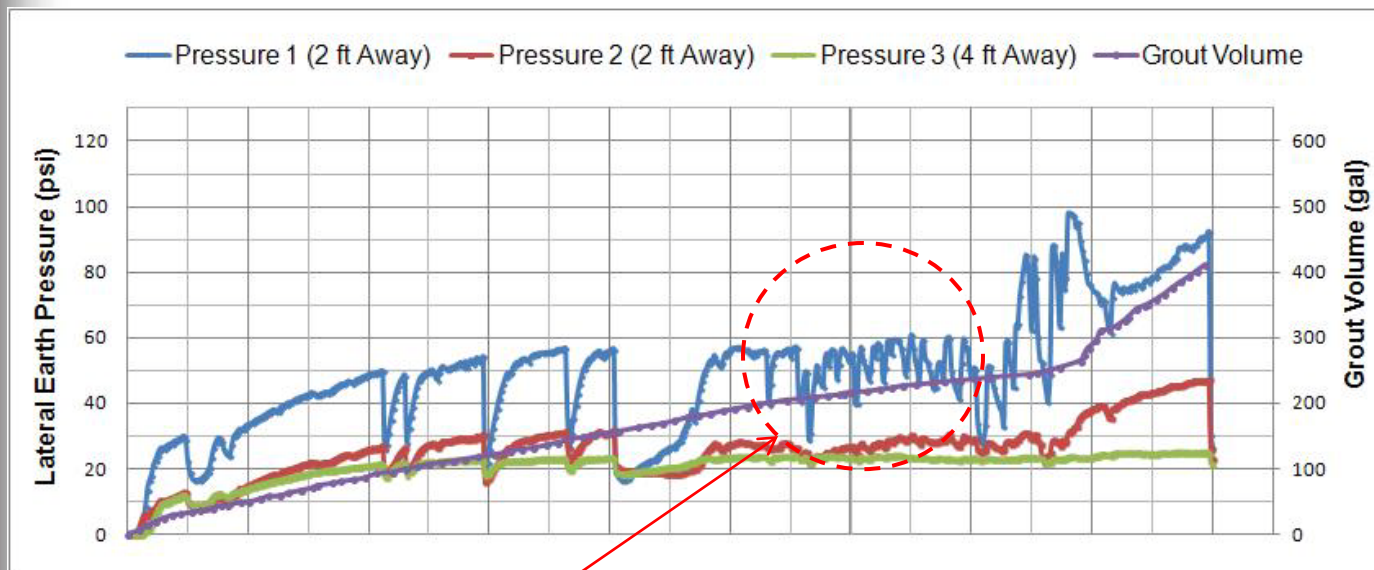
Grout Pump Recirculating back into Reservoir at the End of Stroke

FDOT Test Site

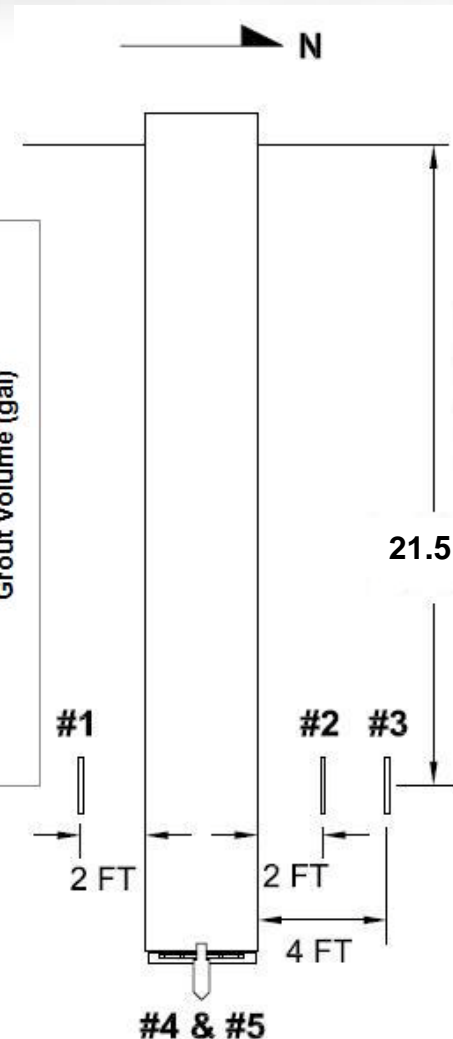
Field Shaft (3-1/2' x 25') – Side Grouting

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Push-In Pressure Cells at Depth of 21.5' (Middle of Side Grouted Zone)



**Grout Pump Recirculating
back into Reservoir at the
End of Stroke**

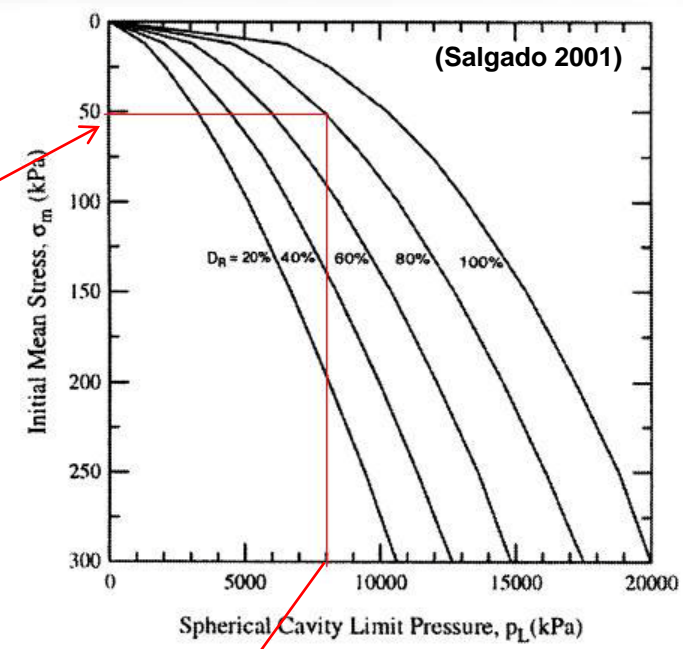
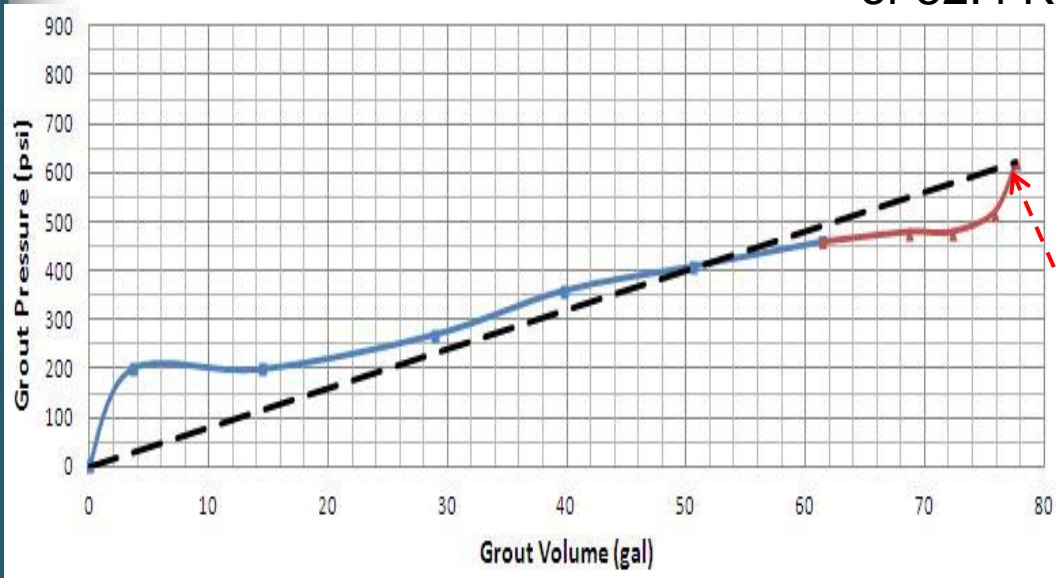


FDOT Test Site

Field Shaft (3-1/2' x 25') – Tip Grouting

Depth of Tip Grout Zone = 25'

Initial Mean Stress, $\sigma_m = \frac{(2 \cdot \sigma_h) + \sigma_v}{3} \approx 7.6 \text{ psi}$
 or 52.4 KPa



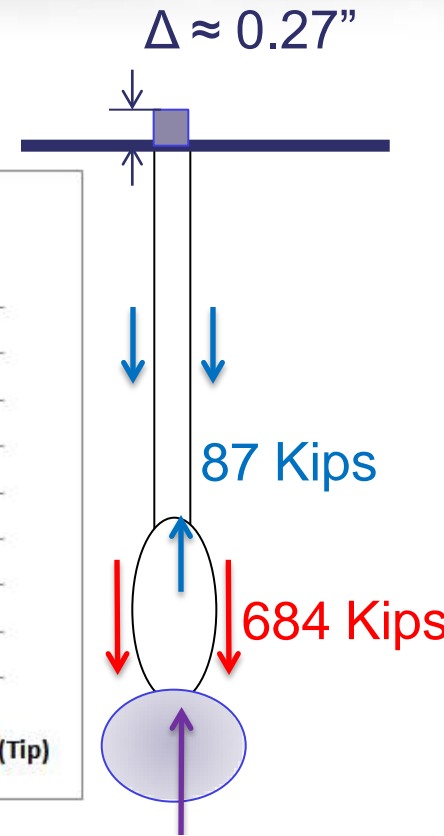
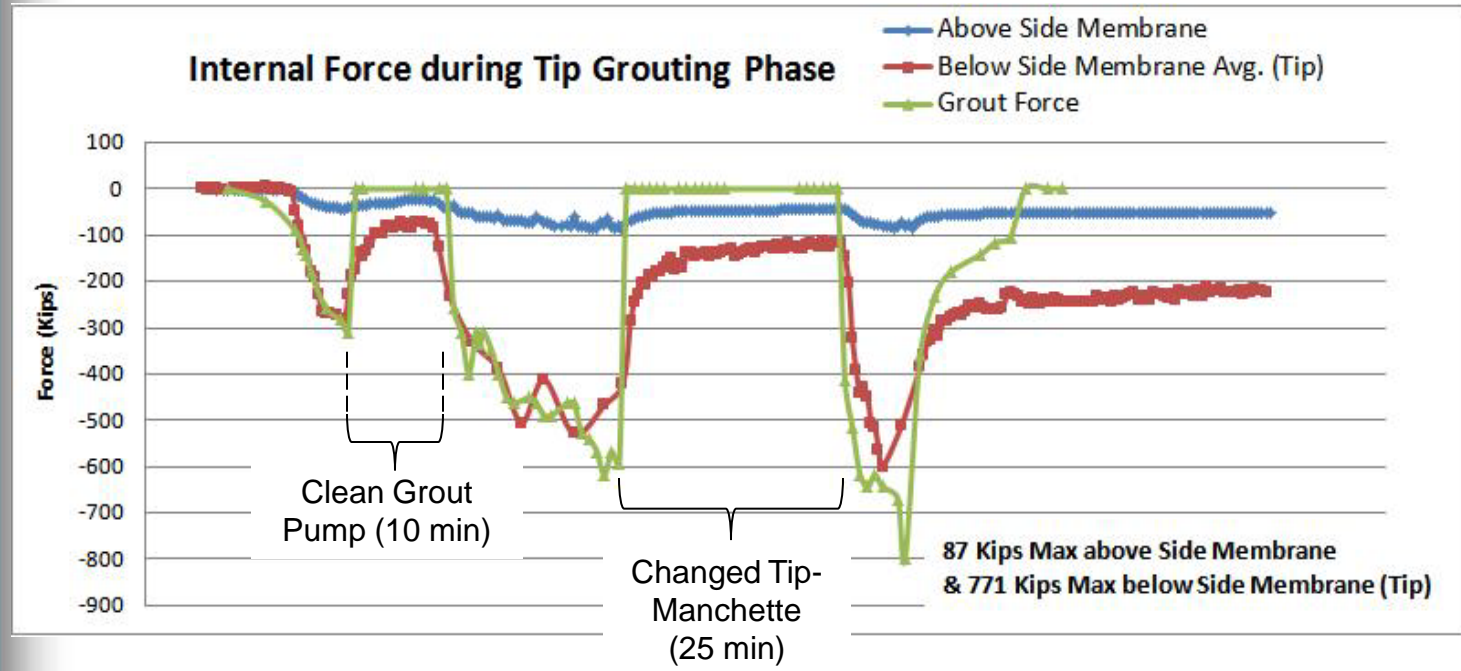
8000 kPa \approx 1160 psi (Max)

Observed: 620 psi (Max)

0.34" Upward Shaft Movement
 (0.27" Differential Movement with Soil)³⁴

FDOT Test Site

Field Shaft (3-1/2' x 25') – Tip Grouting



Shaft Capacity $\geq 2 \times$ Skin = 1542 Kips ← 771 Kips (620 psi Grout Pressure & 1243 in² Tip Area)

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Field Shaft (3-1/2' x 25') – Top-Down Test

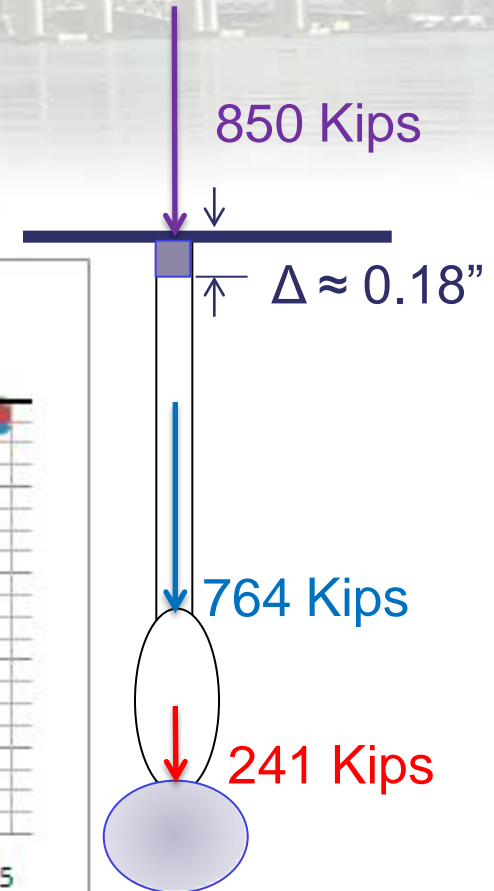
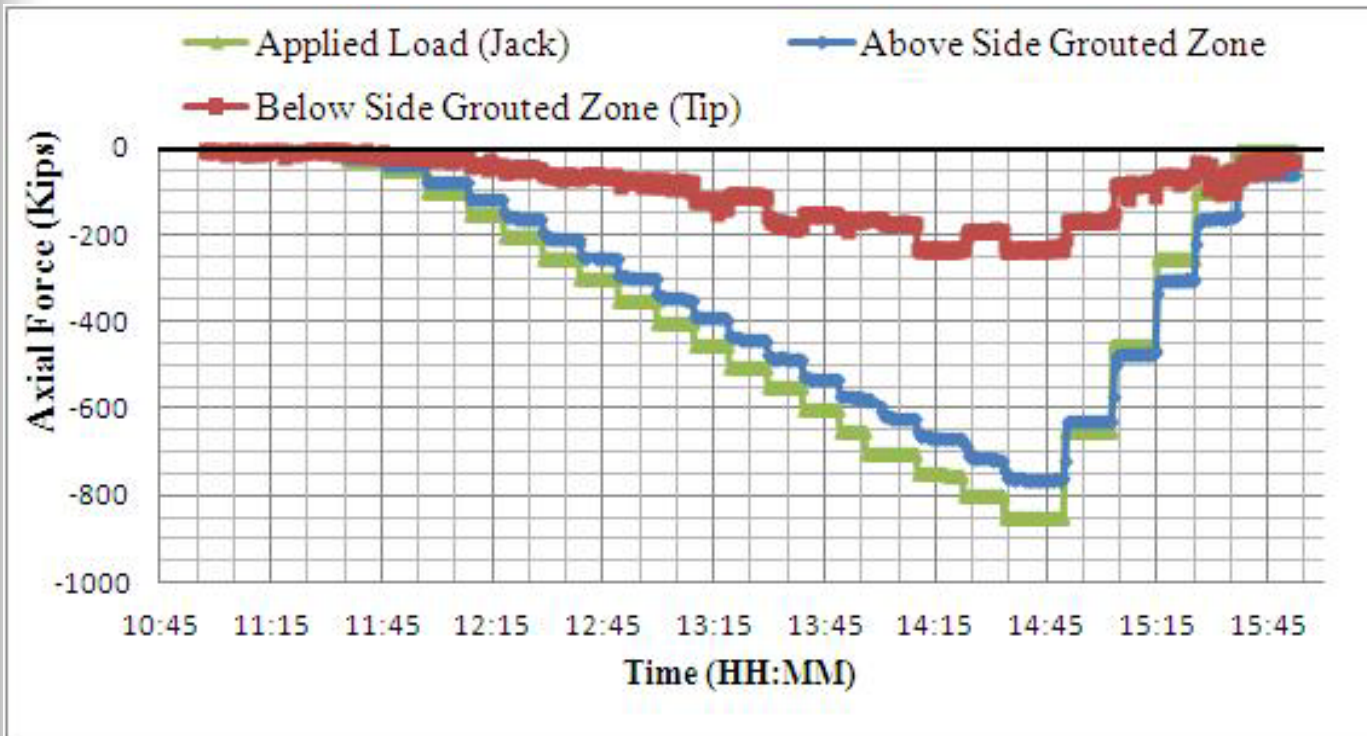
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FDOT Test Site

Field Shaft (3-1/2' x 25') – Top-Down Test

Internal Forces during Top-Down Test



Failed Reaction Shafts (4' x 55')

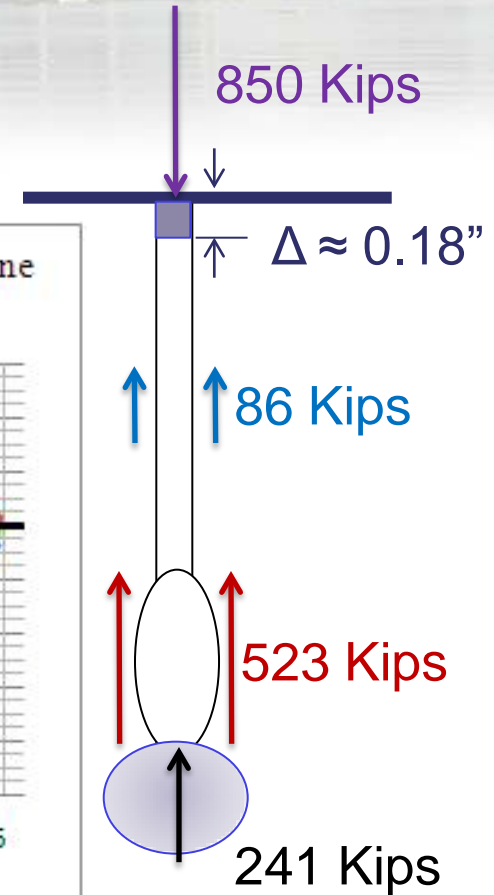
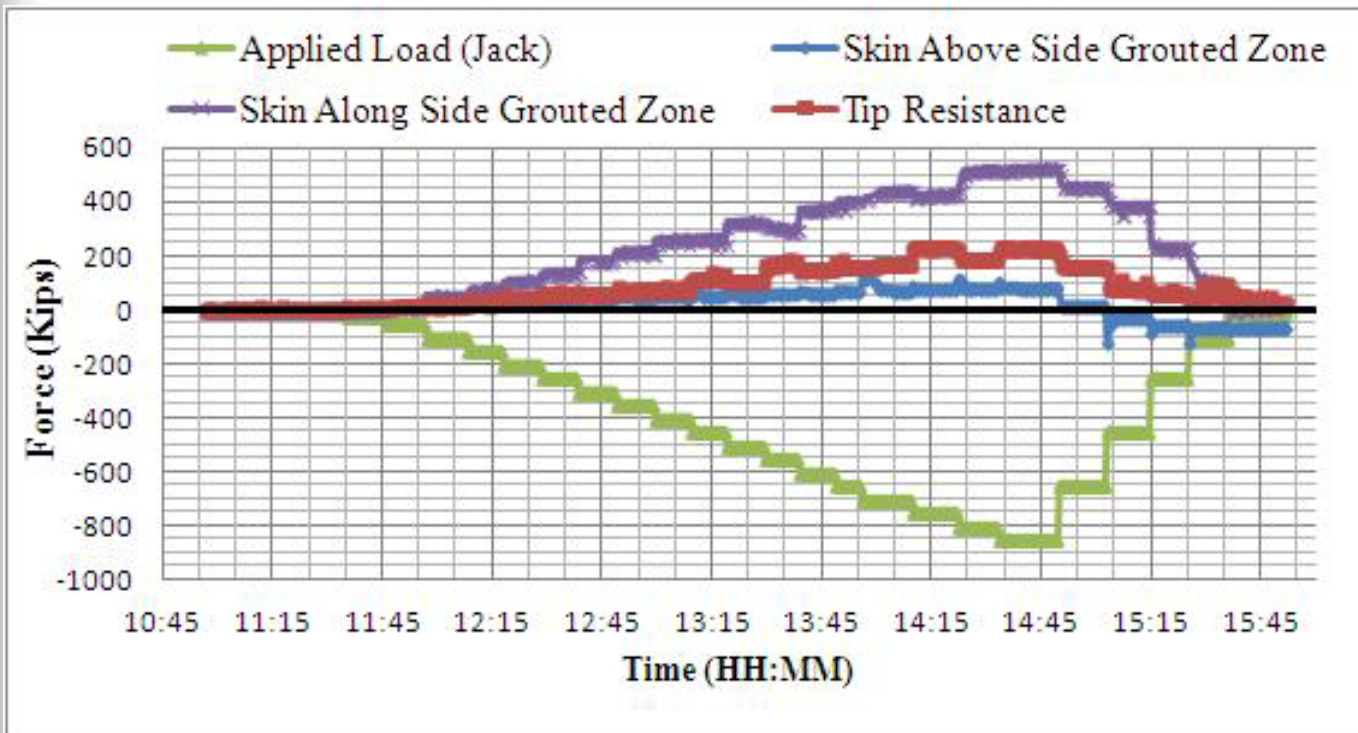
Maximum Upward Displacements

- South Shaft – 0.58"
- North Shaft – 0.37"

FDOT Test Site

Field Shaft (3-½' x 25') – Top-Down Test

Mobilized Resistance during Top-Down Test



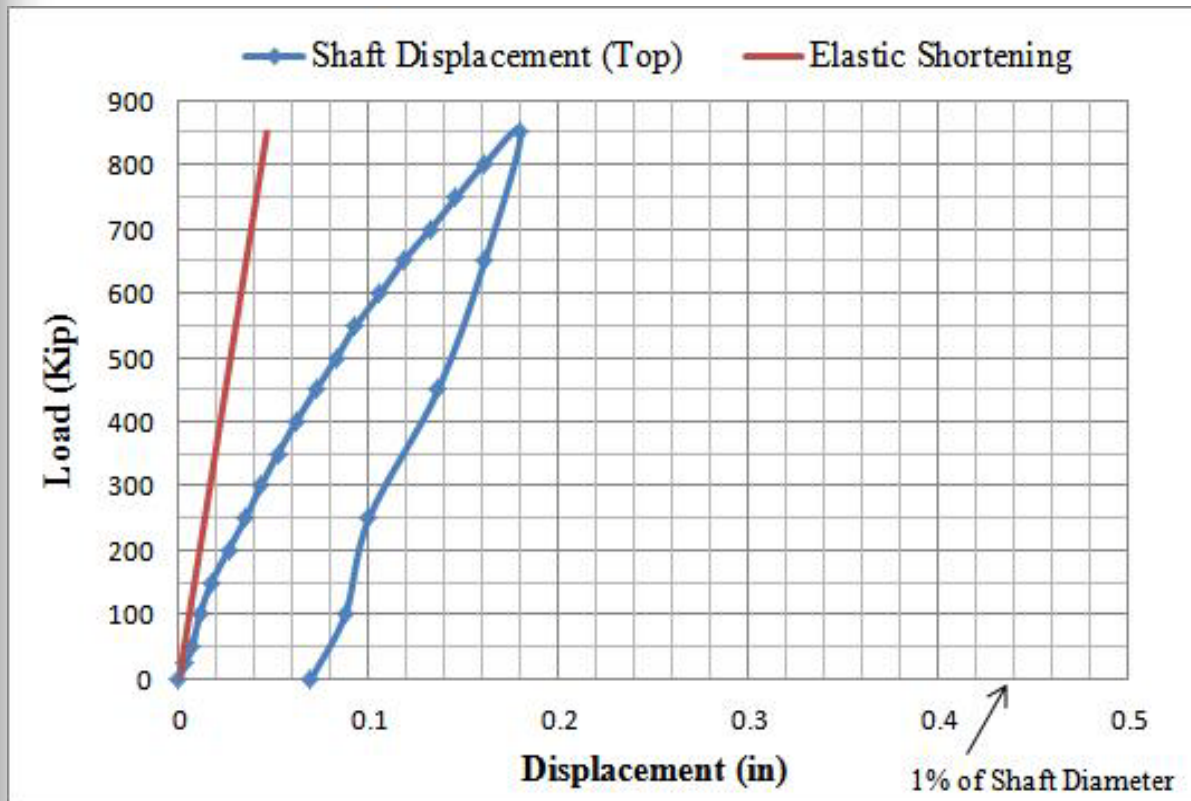
**61% of Applied
Load Carried by
Side Grouted
Zone!!!**

FDOT Test Site

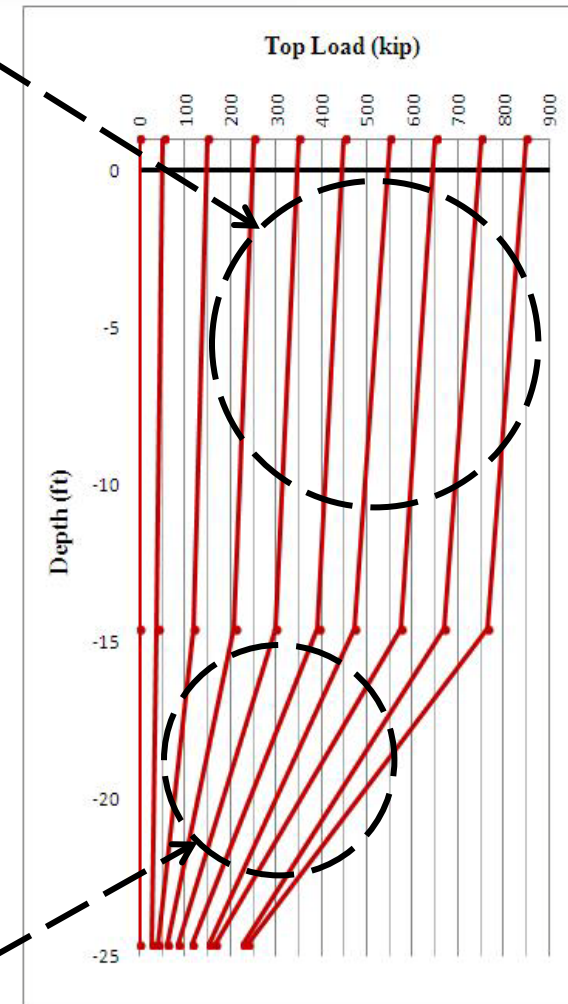
Field Shaft (3-1/2' x 25') – Top-Down Test

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Fully Mobilized above Side Grouted Zone



Not Fully Mobilized along Side Grouted Zone



UngROUTED Drilled Shafts

Predicted Capacity – Skin (Alpha & Beta) (FHWA/AASHTO, 2007)

Layer (#)	Soil Type	Depth (ft)	Depth to Mid-Point of Zone, z (ft)	Avg. Cone Tip Resist., Q_c (ton/ft ²)	Vertical Stress, σ_v (lb/ft ²)	Undrained Shear Strength, C_u (kip/ft ²)	(1) Alpha Value, α	(2) Unit Side Resistance, f_{su1} (kip/ft ²)	Surface Area (Top 8 ft), A_{side1} (ft ²)	Side Resistance (Top 8 ft), (kip)
1	Clay	0 - 8	4	18.06	460	1	0.55	0.55	87.96	48 = q_{s1}

(1) $\alpha = 0$ (if $z < 5$ ft); $\alpha = 0.55$ (if $z > 5$ ft); $\alpha = 0$ (bottom of shaft for 1 diameter length & length of casing)

(2) Ultimated Unit Load Transfer in Side Resistance, $f_{su} = \alpha * C_u$

Layer (#)	Soil Type	Depth (ft)	Depth to Mid-Point of Zone, z (ft)	Avg. Uncorrected Blow Count (N-Value)	Vertical Effective Stress, σ_v' (lb/ft ²)	(1) Beta Value (β_0)	(2) Corrected Beta Value (β)	(3) Unit Side Resistance, f_s (kip/ft ²)	Surface Area, A_{side} (ft ²)	Side Resist., q_s (kip)
2	Sand	8 - 15	11.5	5.5	1122	1.0422	0.3821	0.43	77	33 = q_{s2}
3	Sand	15 - 25	20	16	1636	0.8963	0.8963	1.47	110	161 = q_{s3}
4	Sand	25 - 40	32.5	55	2456	0.7304	0.7304	1.79	N/A	N/A

(1) $\beta_0 = 1.2$ (if $z < 5$ ft); $\beta_0 = 1.5 - 0.135v(z)$ (if $5 \text{ ft} < z < 86 \text{ ft}$); $\beta_0 = 0.25$ (if $z > 86 \text{ ft}$)

(2) Corrected Beta, $\beta = (N/15) * \beta_0$ (if $N < 15$)

(3) Unit Side Resistance, $f_s = \beta * \sigma_v'$

UngROUTED Drilled Shafts

Predicted Capacity – Skin & Tip (FHWA/AASHTO, 2007)

Side Resistance above Side Grouted Zone, $Q_{s\text{-above}}$ (kip)	81	= $q_{s1} + q_{s2}$ vs. 86 & 87 Meas.
Side Resistance along Side Grouted Zone, $Q_{s\text{-along}}$ (kip)	161	= q_{s3}
Total Side Resistance, $Q_{s\text{-Total}}$ (kip)	243	= $q_{s1} + q_{s2} + q_{s3}$

Tip Area, A_T (in ²)	1385.44
Tip Area, A_T (ft ²)	9.62
(1) Average Tip N-Value	28
(2) Unit Tip Resistance, q_T (ton/ft ²)	16.8
(3) Tip Resistance, Q_T (kip)	323

(1) Average N-Value of Soil 1.5*D above Tip down to 3*D below Tip
(2) Unit Tip Resistance (AASHTO 2007), q_T (ton/ft ²) = 0.6*N
(3) Tip Resistance, Q_T (kip) = $A_T(\text{ft}^2) * q_T(\text{ton/ft}^2) * 2(\text{kip/ton})$

566 Kips Total Axial Resistance before Grouting (Conventional Drilled Shaft)

Side and Tip Grouted Shafts

Predicted Capacity – K_g Method (Thiyyakkandi & McVay, 2013)

Soil Layer (#)	Depth (ft)	Depth to Mid-Point of Soil Layer (ft)	Peak Friction Angle, ϕ_p	Post Grout Surface Area, A_{sg} (ft ²)	Vertical Effective Stress, σ_v' (lb/ft ²)	(1) K_g	(2) Post Grout Vertical Stress, σ_{vg}' (lb/ft ²)	(3) Post Grout Unit Side Resist., f_{s3-Kg} (kip/ft ²)	(4) Post Grout Side Resist., q_{s3-Kg} (kip)
3	15 - 25	20	41.2	156.69	1636	1.85	3027	4.40	689
(1) Use $\phi_c = \phi_u = 36.2^\circ$ (See Plot Below)									(5) Total Side Resistance (Post Side Grout), $Q_{sg-Total-Kg} = 770$
(2) Post Side Grout Vertical Effective Stress, $\sigma_{vg}' = K_g * \sigma_v'$									
(3) Post Grout Unit Side Resistance along Side Grouted Zone, $f_{s3-Kg} = \sigma_{vg}' * [\sin\phi_p / (1 - \sin\phi_p)] * \sin(90 - \phi_p)$									
(4) Post Grout Side Resistance along Side Grouted Zone, $q_{s3-Kg} = f_{s3-Kg} * A_{sg}$									
(5) Total Side Resistance after Side Grouting, $Q_{sg-Total-Kg} = Q_{s-above} + q_{s3-Kg}$									

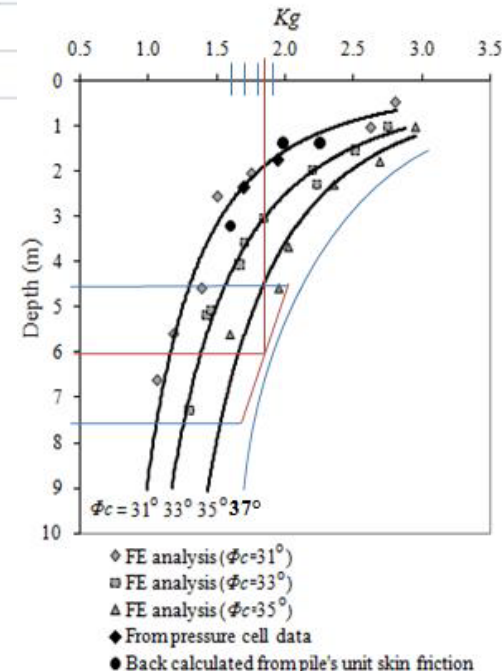
= Q_{s3-Kg}
= 689 + 81 kips

Estimated Total Capacity = Skin + Tip

Since,

Total Skin < Tip Spherical Expansion Pressure x Tip Area

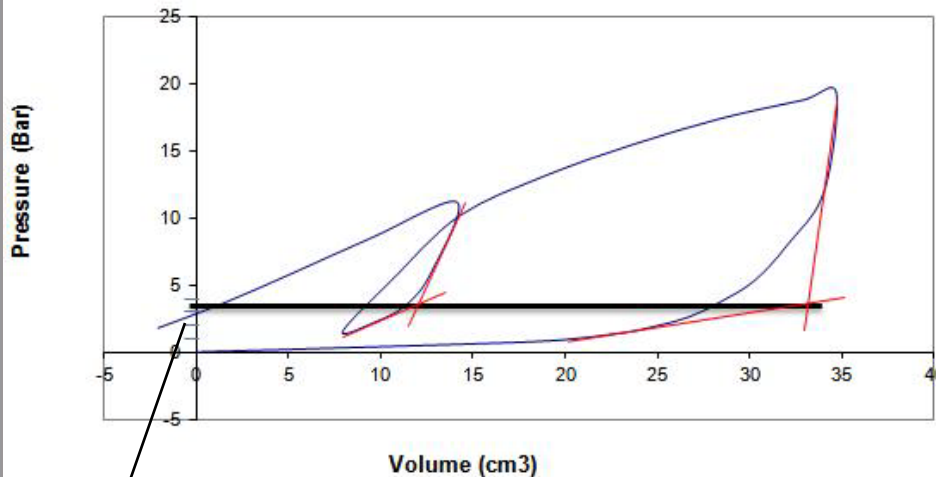
Total Capacity > 2 x Skin = 2 x 770 = **1540 Kips**



Side and Tip Grouted Shafts

Predicted Capacity – PMT Method (FDOT BDK-545 #31, 2009)

Fully Corrected Pencil Pressuremeter Curve



Estimated Total Capacity = Skin + Tip

Since,
Total Skin < Tip Spherical Expansion
Pressure x Tip Area

Total Capacity > 2 x Skin = 2 x 824
= **1648 Kips**

Residual Stress (Bar)	Residual Stress (lb/in ²)	Peak Friction Angle, ϕ_p	Post Grout Surface Area, A_{sg} (ft ²)	(1) Unit Side Resist. along Side Grouted Zone, f_{s3-PMT} (ksf)	(2) Friction along Side Grouted Zone, q_{s3-PMT} (kip)	(3) Total Side Resist., $Q_{sg-Total-PMT}$ (kip)
3.5	50.76	41.2	156.69	4.74	743	824

= 743 + 81 kips

(1) Post Grout Unit Side Resistance along Side Grouted Zone, $f_{s3-PMT} = (\text{"Residual Stress"}) \cdot \tan(\delta_i')$

where: Interface Friction Angle, $\delta_i' = \Delta_i \cdot \phi_p = 33^\circ$

(2) Post Grout Side Resistance along Side Grouted Zone, $q_{s3-PMT} = f_{s3-PMT} \cdot A_{sg}$

(3) Total Side Resistance after Side Grouting, $Q_{sg-Total-PMT} = Q_{s-above} + q_{s3-PMT}$

Side and Tip Grouted Shafts

Predicted & Measured Capacities

	Above Side Grouted Zone (Top 15 ft of Shaft)		Along Side Grouted Zone (Bottom 10 ft of Shaft)		Total Side Resistance (Kip)	Tip Resistance (Kip)	Ultimate Load (Kip)
	Unit Side Resistance (ksf)	Side Resistance (Kip)	Unit Side Resistance (ksf)	Side Resistance (Kip)			
UngROUTED Drilled Shaft (Neglect Tip Resist.)	0.49	81	1.47	161	243	---	243
UngROUTED Drilled Shaft (Include Tip Resist.)	0.49	81	1.47	161	243	323	566
Side & Tip Grouted Drilled Shaft, Kg Method	---	---	4.40	689	770	---	1540
Side & Tip Grouted Drilled Shaft, PMT Method	---	---	4.74	743	824	---	1648
*Mobilized during Tip Grouting (Max)	0.53	87	4.37	684	771	771	1542
Mobilized during Top-Down Test (Max)	0.52	86	3.34	523	609	241	850*

*Upward Displacement (Top of Shaft) = 0.34 Inch (0.81% of Shaft Diameter)

**Downward Displacement (Top of Shaft) = 0.18 Inch (0.43% of Shaft Diameter)

***Maximum Applied Load during Top-Down Test so Not an Ultimate Load

**Quantify the Ultimate Capacity by Performing Statnamic Axial Test
(up to 2000 Kips Maximum Load)**

References:

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5. Thiyyakkandi, S., McVay, M., Bloomquist , D., and Lai P. (2013), “Measured and Predicted Response of a New Jetted and Grouted Precast Pile with Membranes in Cohesionless Soils,” ***Journal of Geotechnical and Geoenvironmental Engineering***, 139 (8), 1334-1345.
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Thank You
Questions?