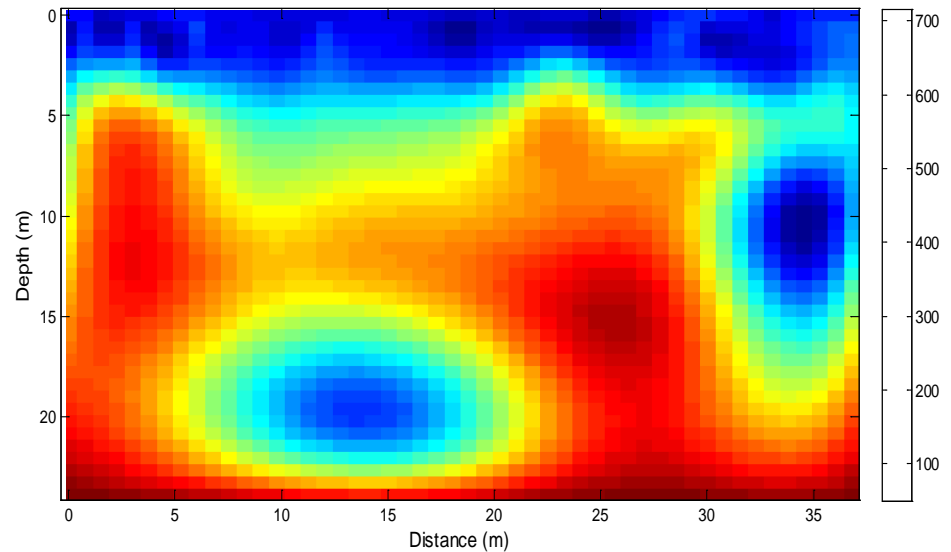
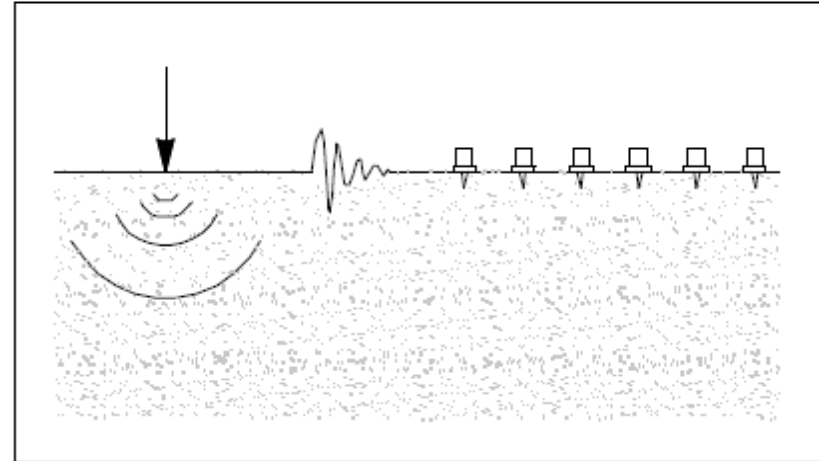


Detection of Sinkholes or Anomalies Using Full Seismic Wave Fields

GRIP 2013

Project Manager:
David Horhota, Ph.D., P.E.

Primary Researchers:
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University
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of Florida



Need of site investigation

- Problems and disputes during and after construction
- Structural damage/collapse
- Long-term affects on structures

Goals of site investigation

- Soil/rock stratigraphy
- Embedded Sinkholes/Anomalies



Sinkhole claims cost **\$1.4 billion** in Florida from 2006-2009 (FL Office of Insurance Regulation, 2010)

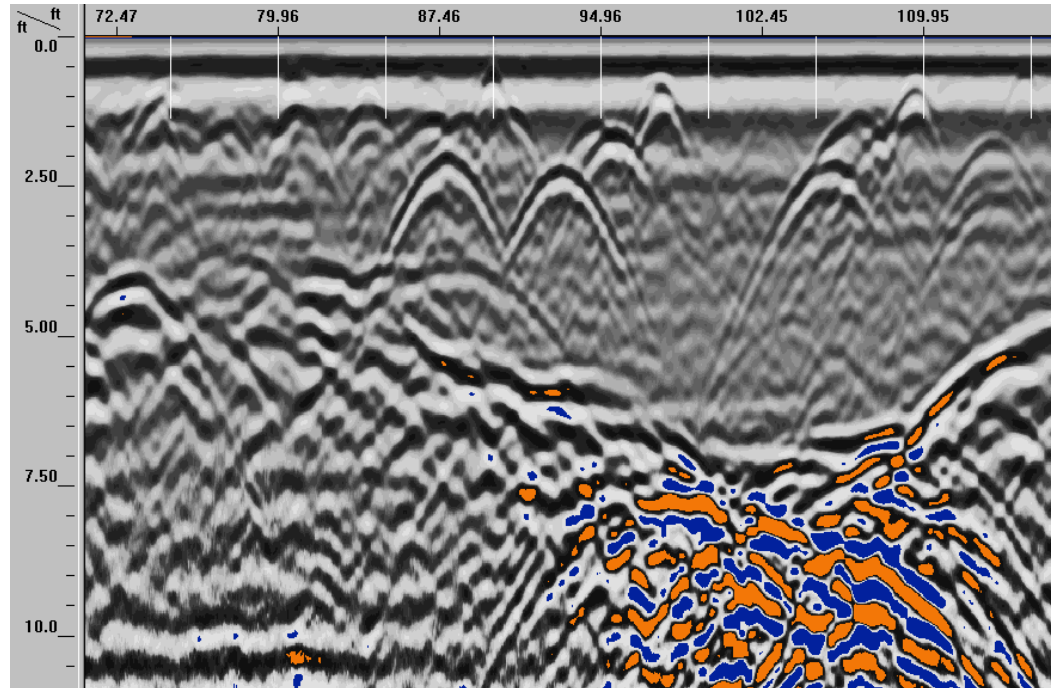
Current practice of site investigations

- Begin with Non-destructive tests (NDT) over a large volume of materials.
 - Ground penetration radar (GPR)
 - Traditional seismic wave methods (MASW, Refraction)
 - Gravity, Resistivity, Conductivity methods
- Follow by invasive tests (CPT, SPT) at suspicious locations (anomalies) for detailed information

Research Motivation

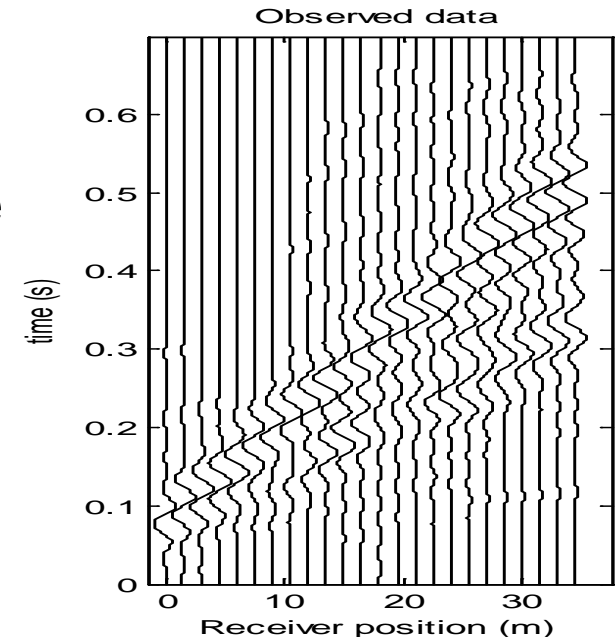
Ground penetration radar (GPR)

- Depth < 15 ft.
- No engineering properties of anomalies
- Limited by clay and ground water

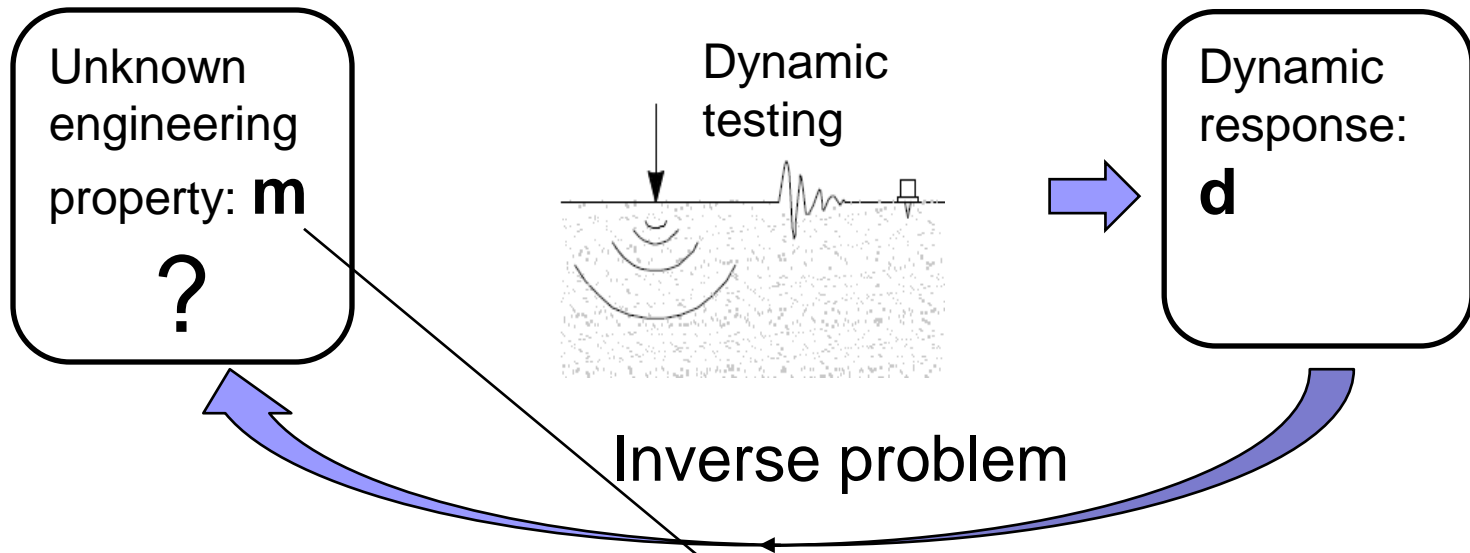


Full waveform inversion (FWI)

- Use entire measured seismic wave field for high-resolution characterization of soil/rock
- Shear wave (S-wave) and pressure wave (P-wave) velocities can be inverted independently to increase credibility
- Low-velocity anomalies can be well characterized
- Soil types can be determined from Poisson's ratio calculated from the P-wave and S-wave velocities
- Relatively easy implementation (no manual picking of travel times)



Overview of FWI



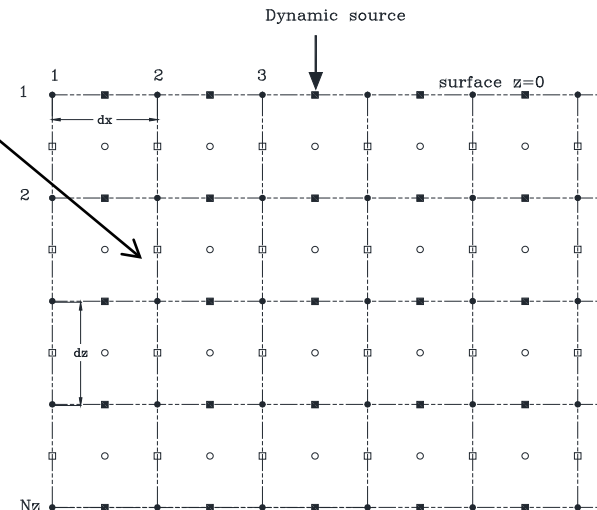
Inversion method:

1. Forward modeling $\mathbf{d} = f(\mathbf{m})$

- 2-D elastic wave equations
- $\mathbf{d}_{\text{est}} = f(\mathbf{m}_{\text{est}})$

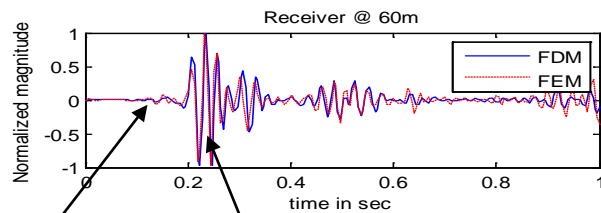
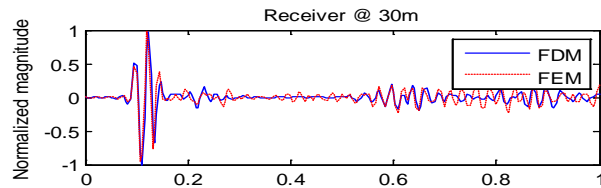
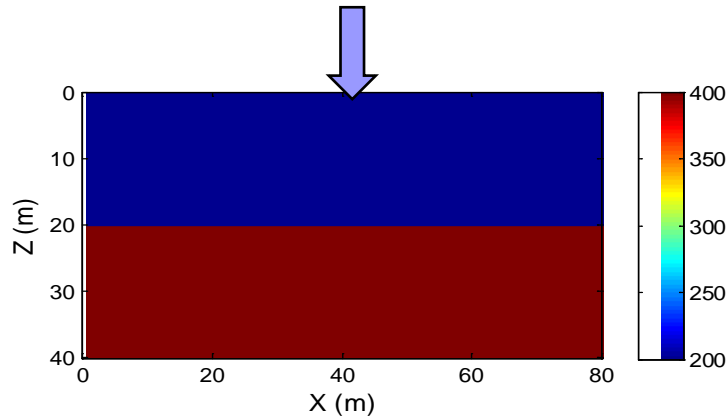
2. Model updating to get $\mathbf{d}_{\text{est}} \approx \mathbf{d}$

- Gauss-Newton method
- Converge when $\mathbf{d}_{\text{est}} - \mathbf{d} \sim 0$



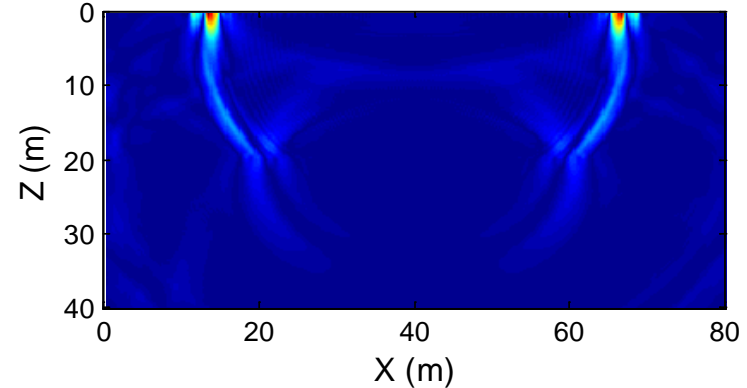
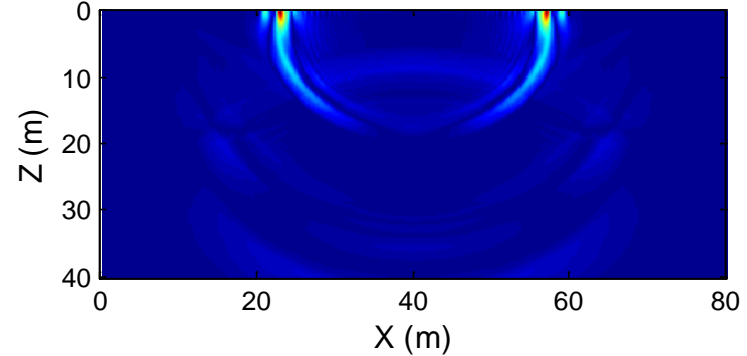
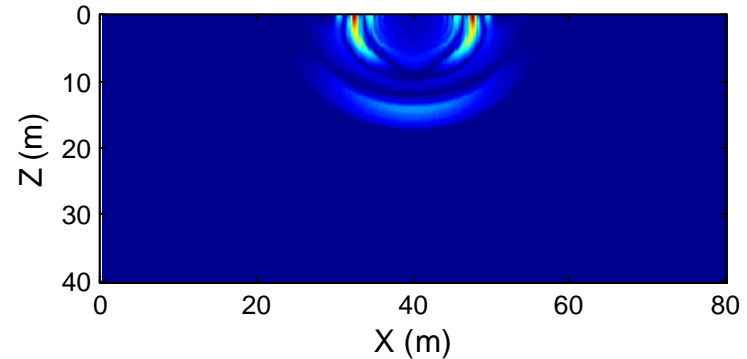
Full waveform inversion (FWI)

➤ Forward modeling



P-wave

Shear-wave and
Rayleigh wave



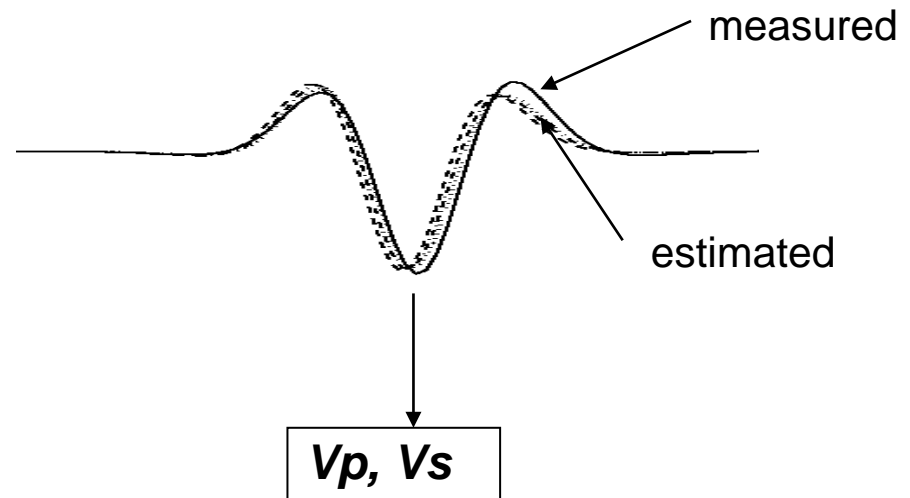
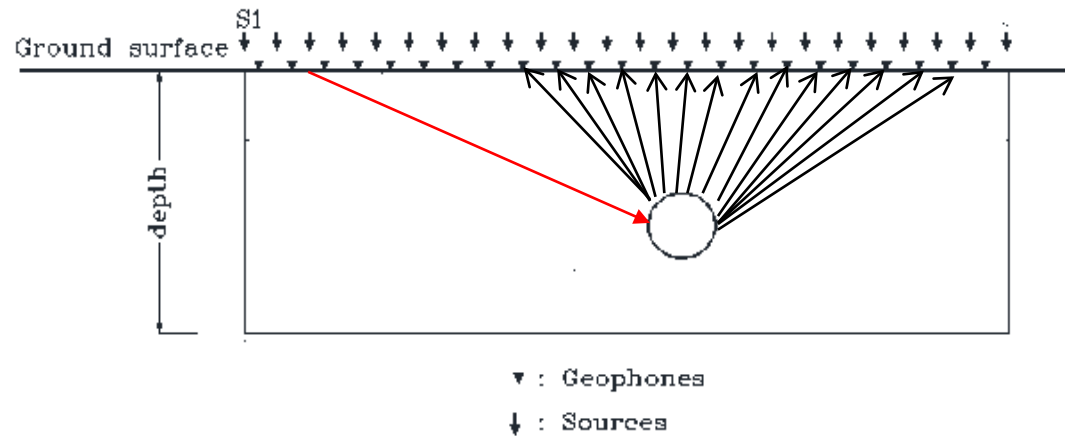
Data Acquisition and Analysis

■ Data Acquisition

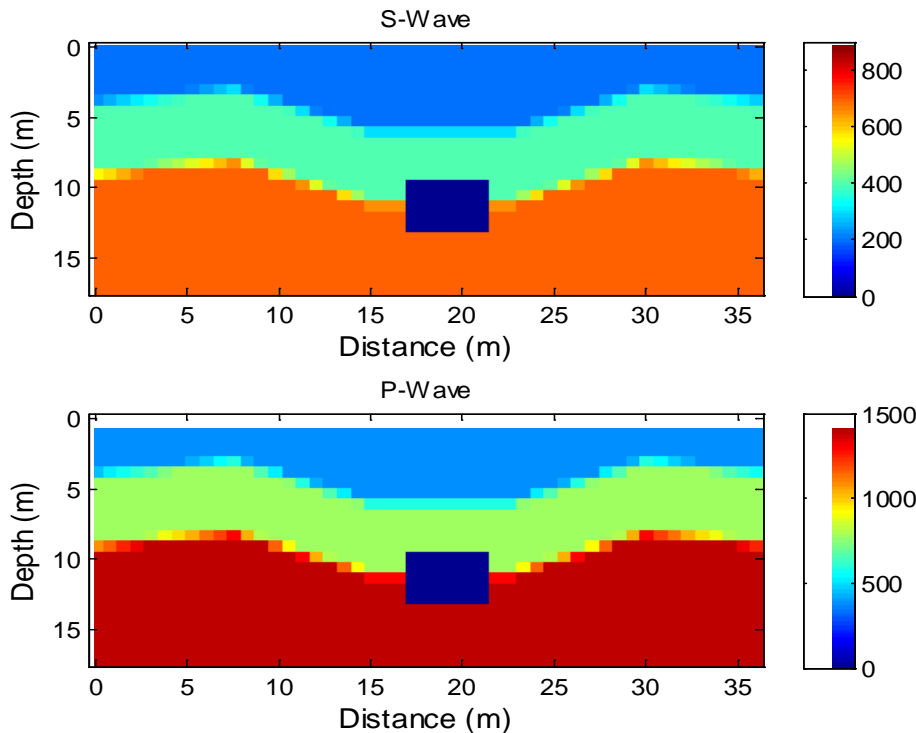
- Multiple geophones at 1 to 3 m spacing
- Multiple sources (strikes of hammer) at 1 to 3 m spacing
- 10-20 lb hammer (5-30 Hz signals)

■ Analysis

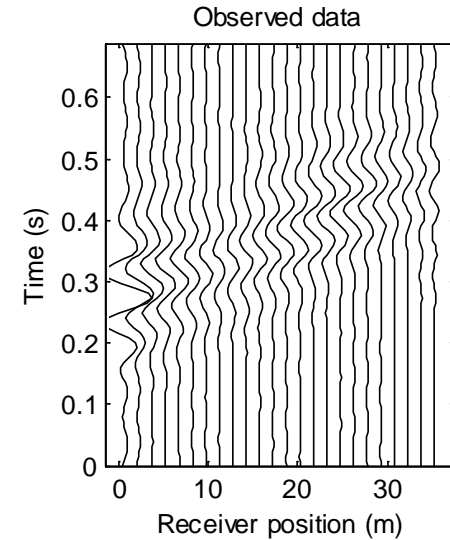
- Start analysis at lowest frequencies and move up
- Low frequencies (large wavelengths) require less detailed information of initial model



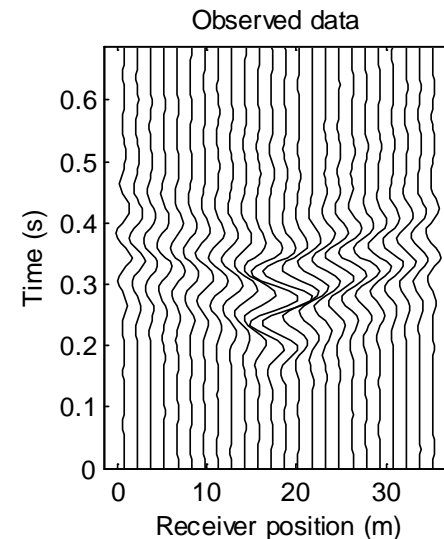
Synthetic test on air-filled void



Shot 1

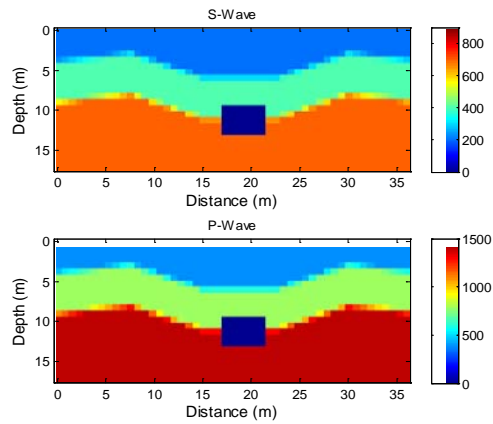


Shot 13

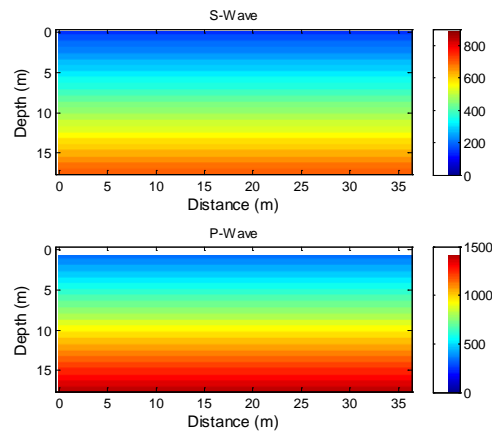


- Test configuration
 - 24 receivers at 1.5 m spacing
 - 25 shots at 1.5 m spacing

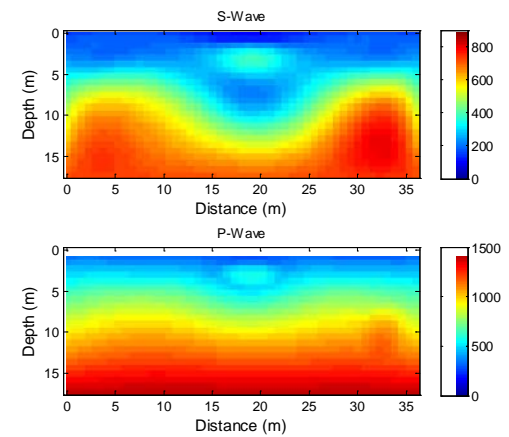
Synthetic test on air-filled void



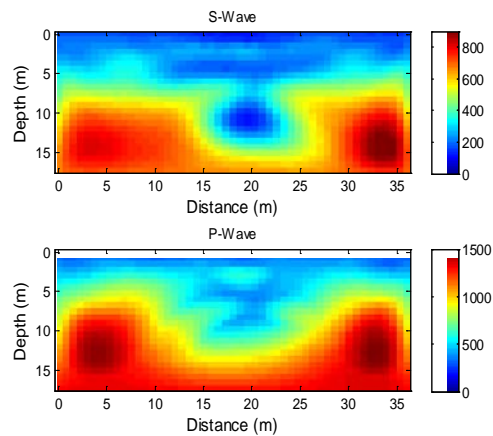
True model



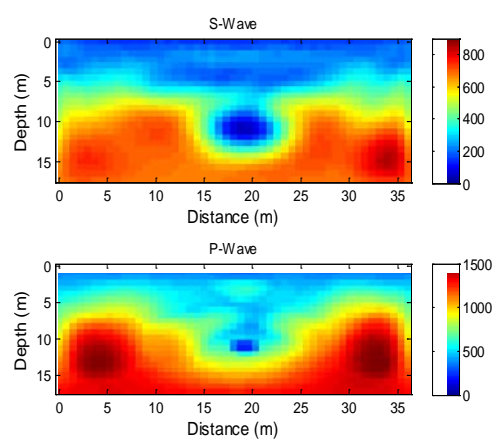
Initial model



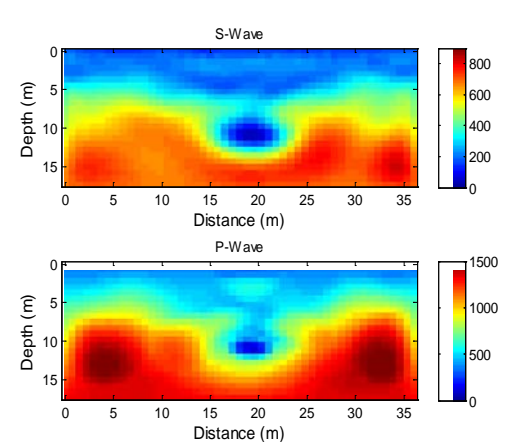
5 Hz



10 Hz

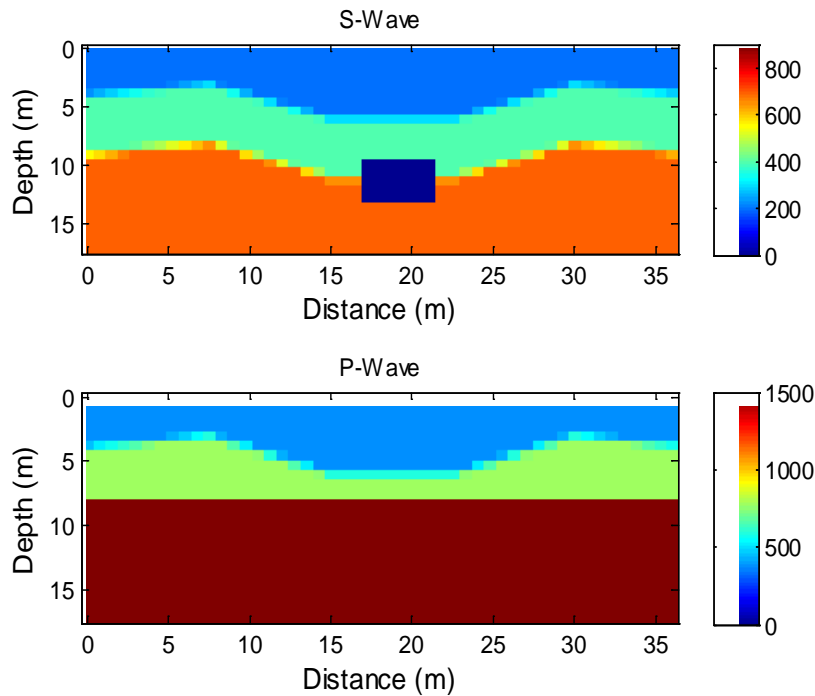


15 Hz



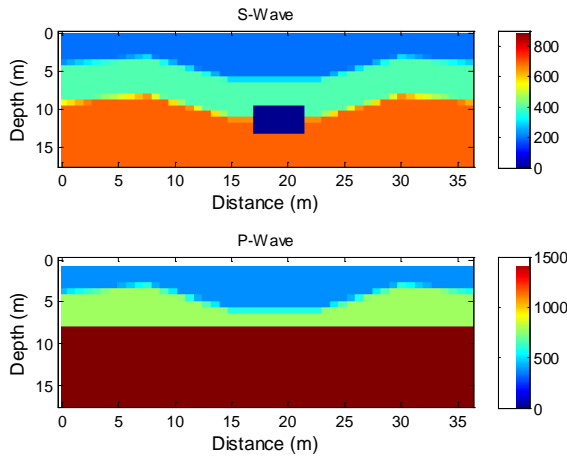
20 Hz

Synthetic test on water-filled void

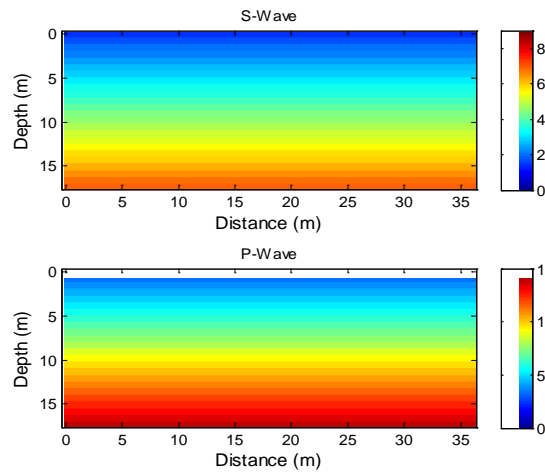


- Test configuration
 - 24 receivers at 1.5 m spacing
 - 25 shots at 1.5 m spacing

Synthetic test on water-filled void

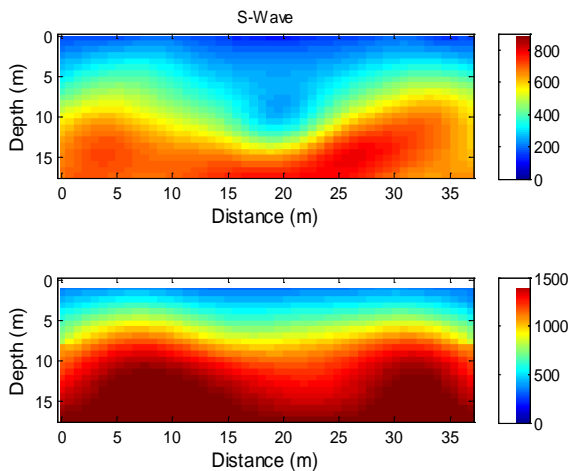


True model

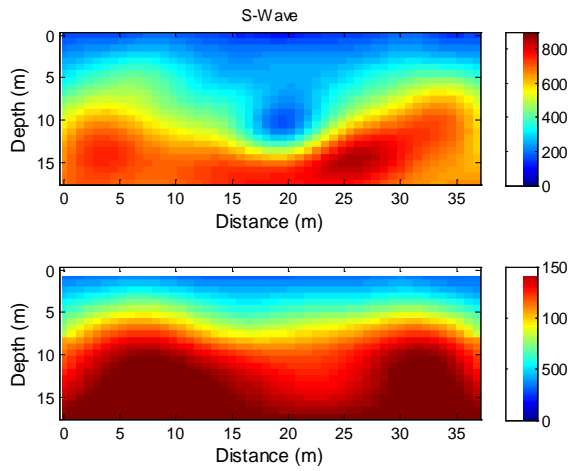


Initial model

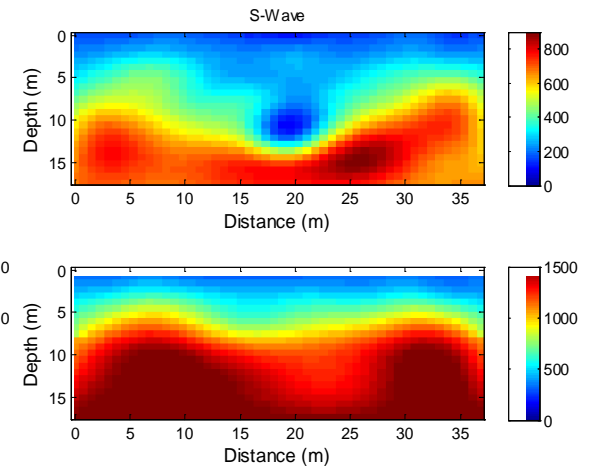
5 Hz



10 Hz



15 Hz

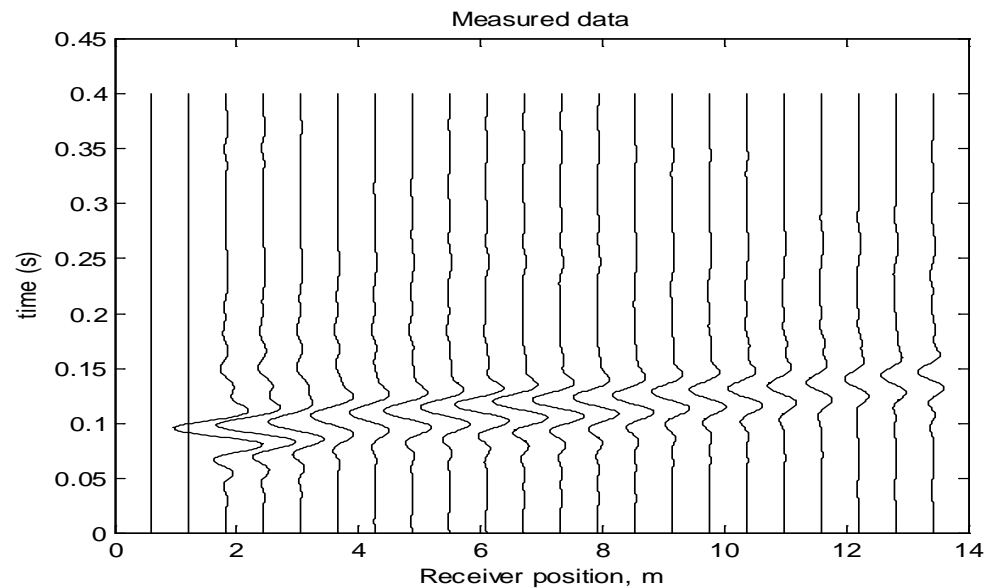
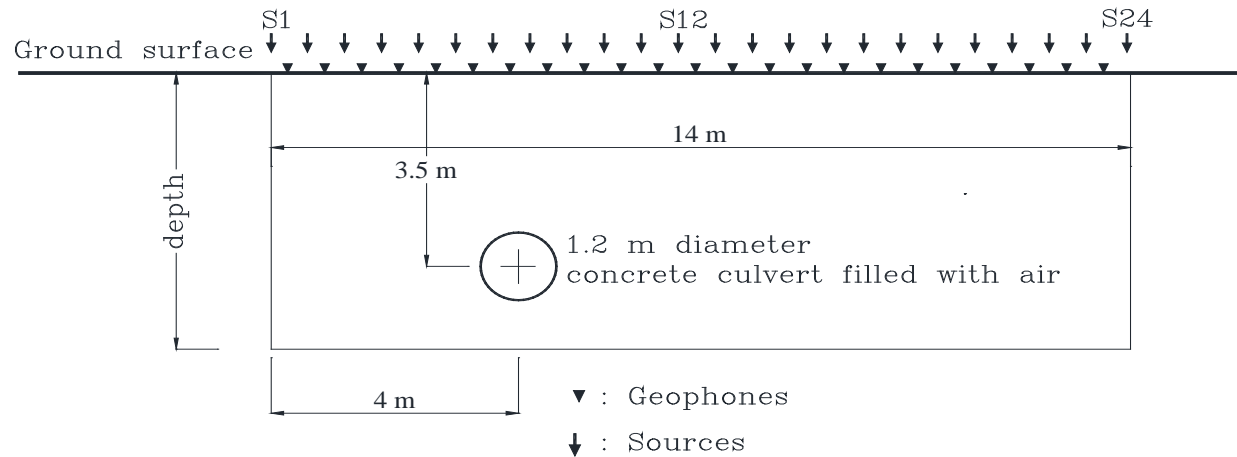


20 Hz

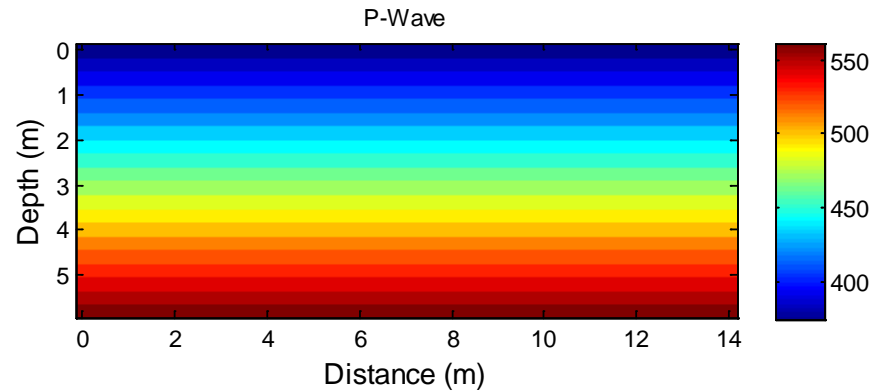
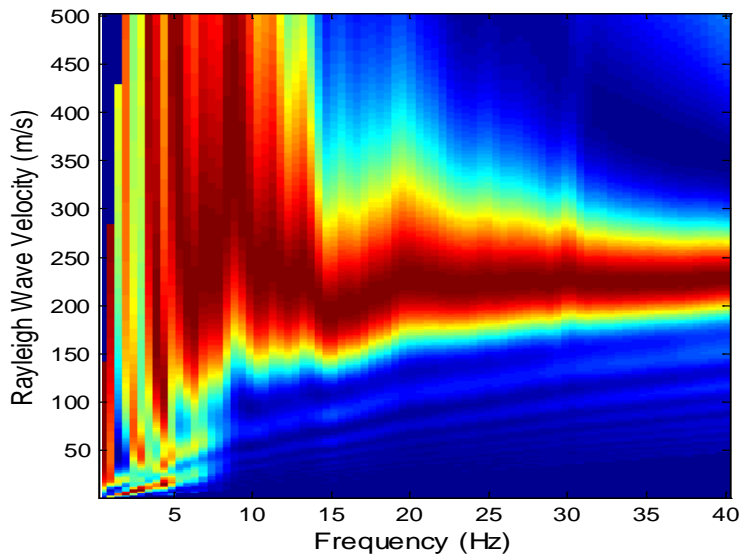
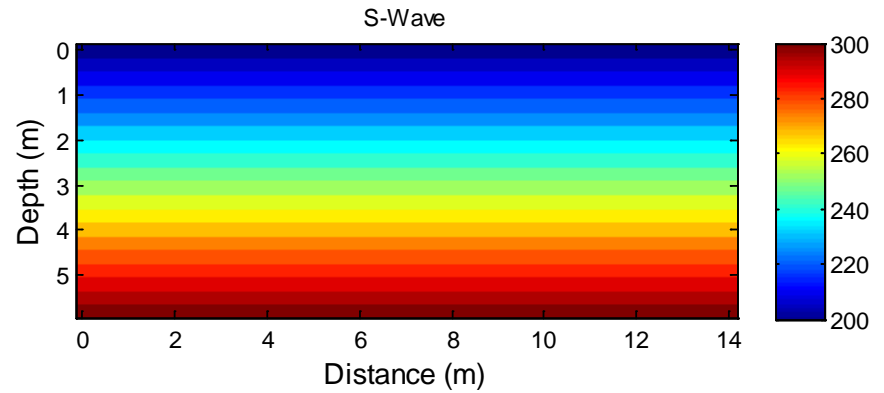
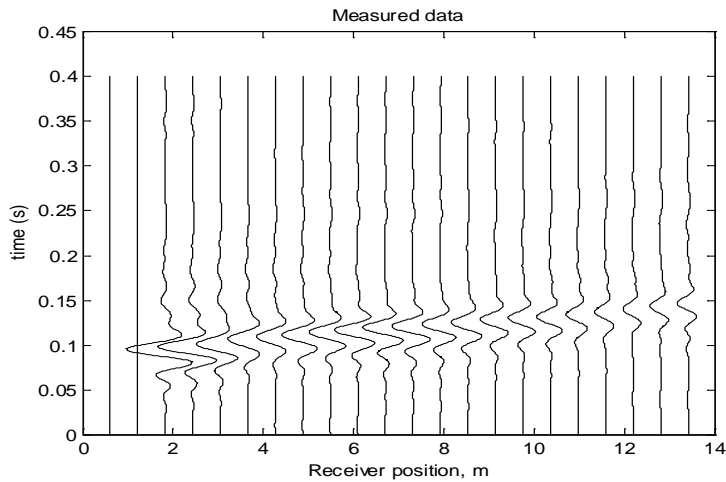
Site 1: Embedded culvert

- UF campus
- Embedded culvert
- 1.2 diameter at 3.5 m depth

- Test configuration
- 23 geophones at 0.6 m spacing
- 24 shots at 0.6 m spacing



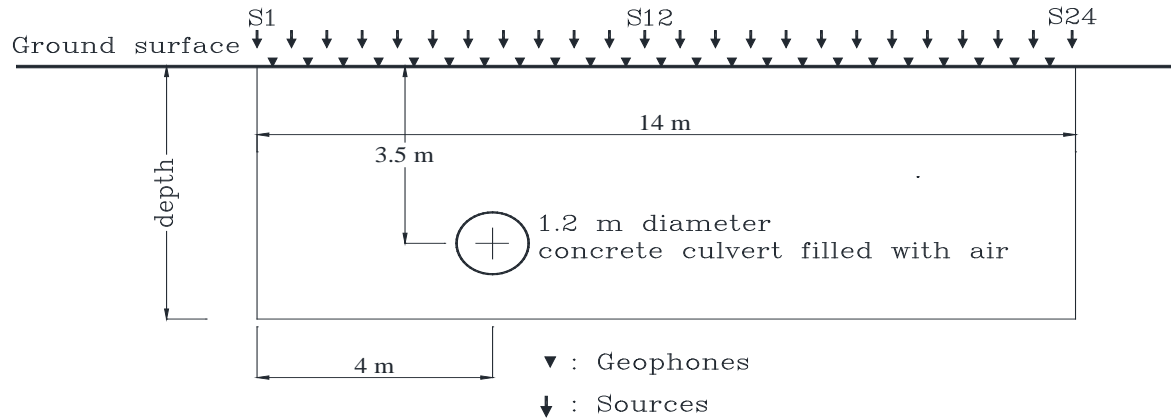
Site 1: Initial model



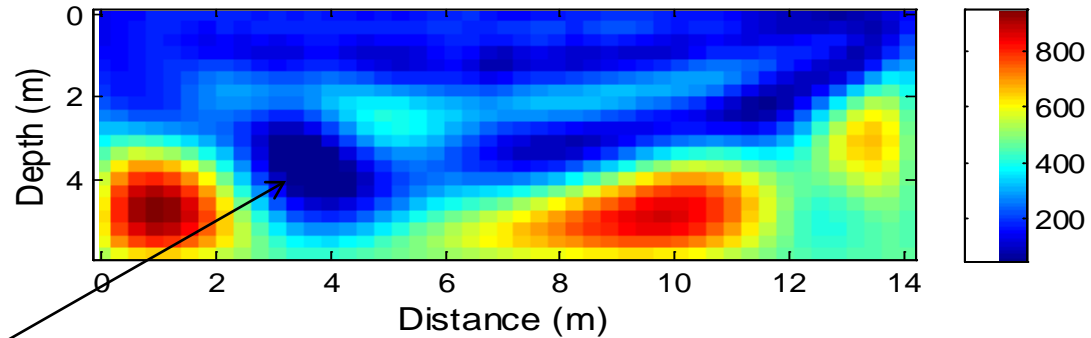
■ Initial model

■ Power spectrum

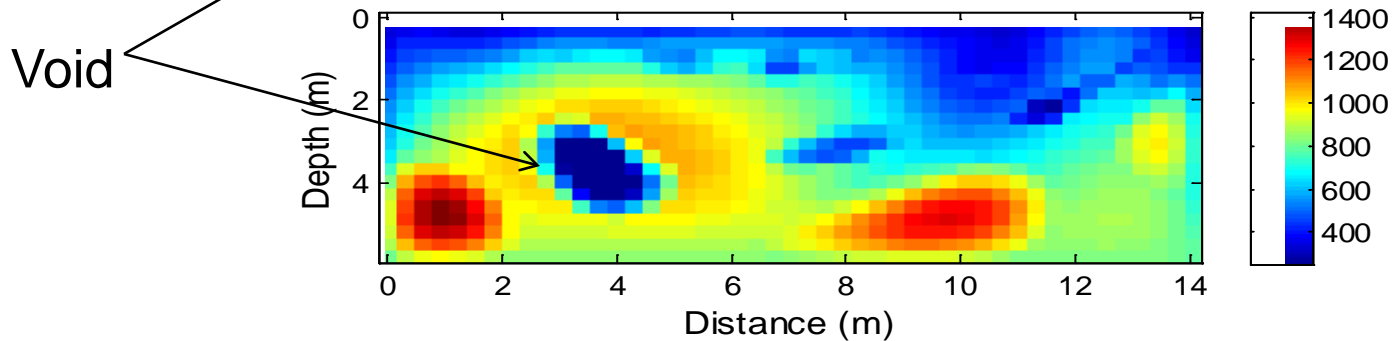
Site 1: Results



S-Wave



P-Wave

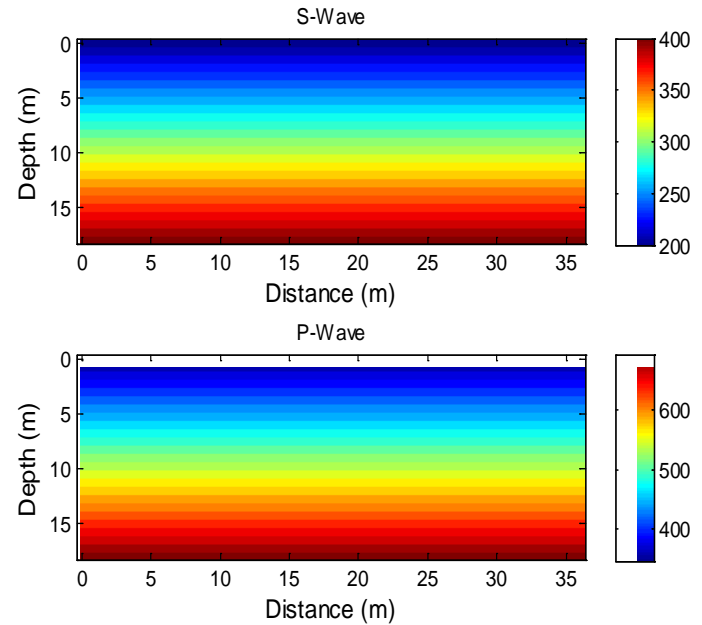
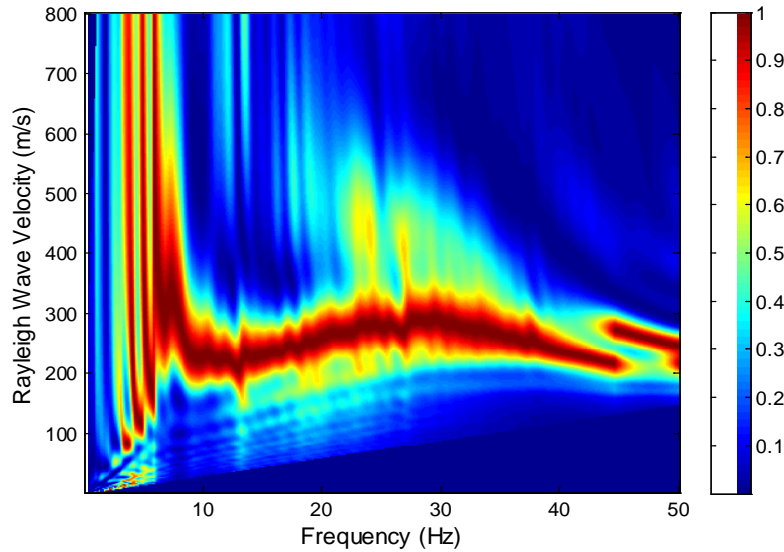


Site 2: embedded low-velocity zone

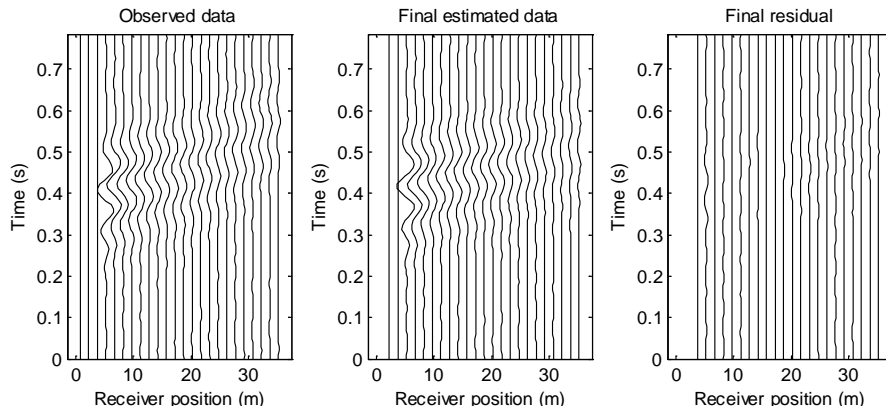
- US441 at Marion County, Florida
 - Repaired sinkhole
- Test configuration
 - 24 geophones at 1.5 m spacing
 - 25 shots at 1.5 m spacing



Site 2: Initial model



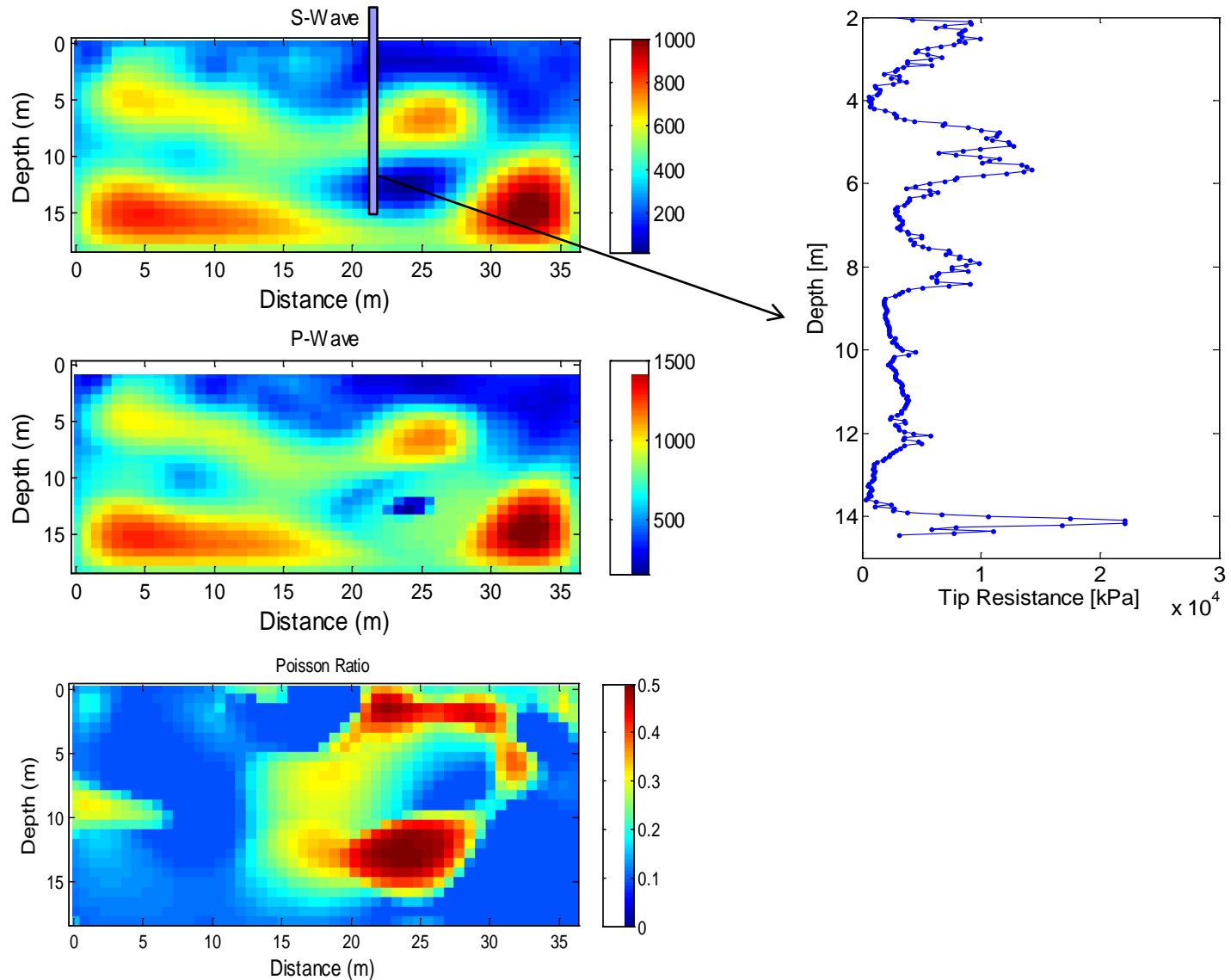
- Power spectrum



- Initial model

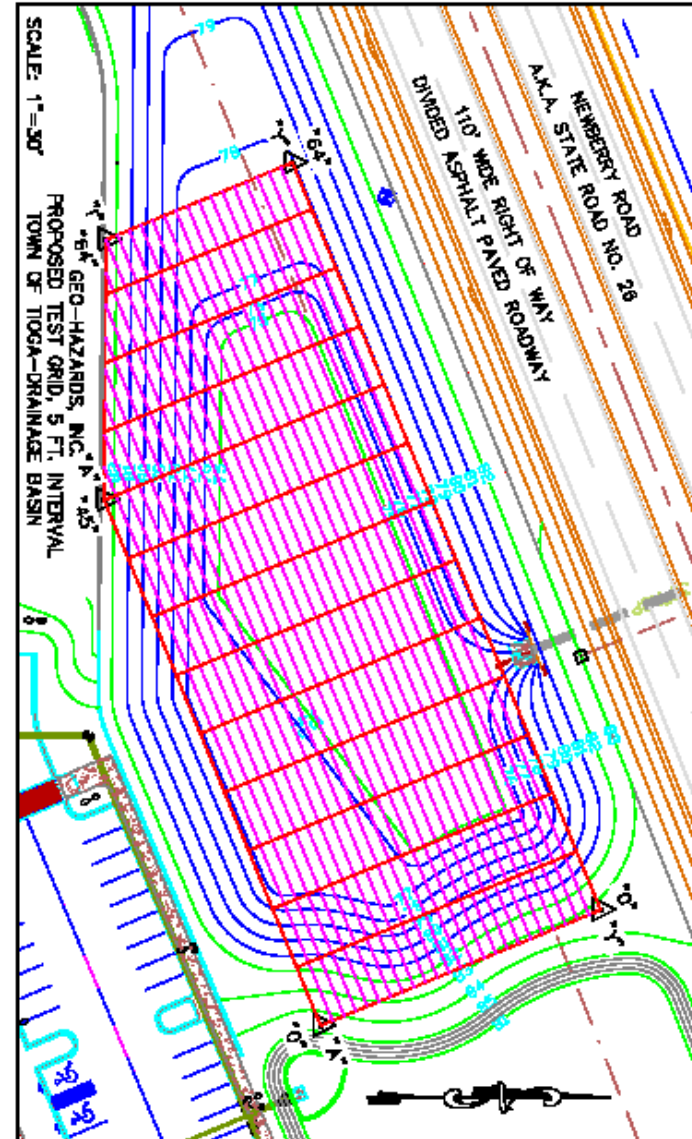
- Data comparison

Site 2: Results



Site 3:

- Dry retention pond in Newberry, Florida
- fine sand and silt of a few meters thick, underlain by highly variable limestone
- top of limestone varies from 2 m to 10 m in depth
- 26 lines (A to Z) at 3 m spacing
- 200 m long each line
- Open chimneys in the southern portion
- Flat open area in the northern portion

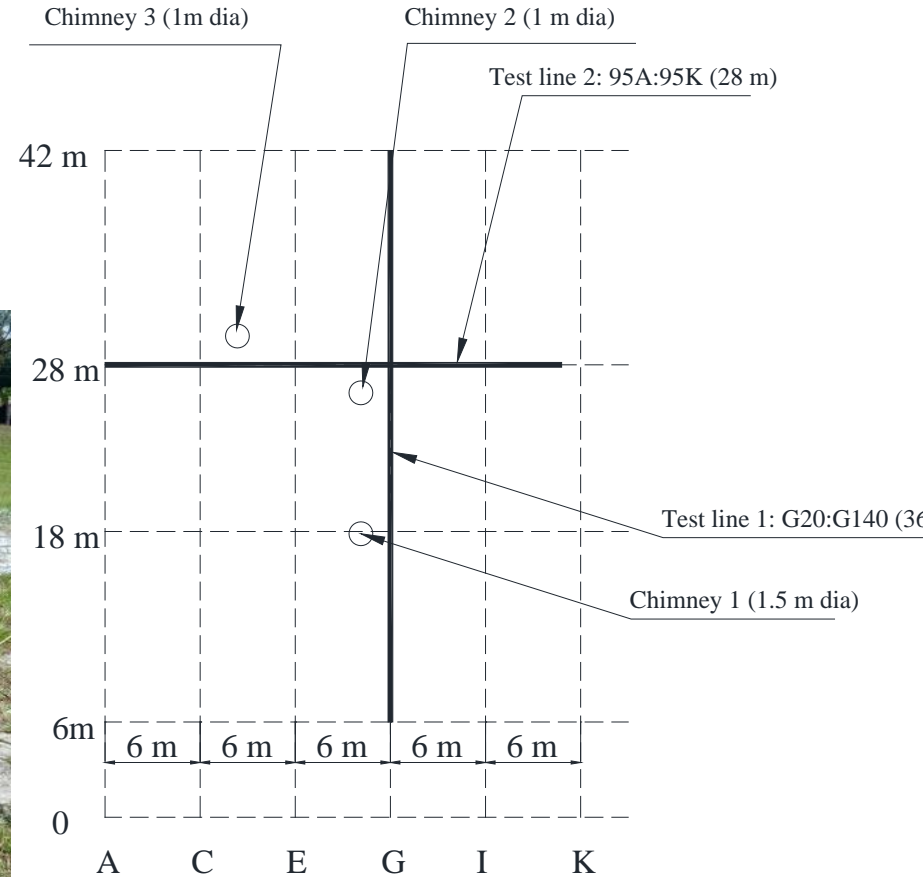


Site 3a: Southern portion

- Test configuration
 - 2 test lines next to next to open chimneys
 - 24 geophones, 25 shots



Chimney 1



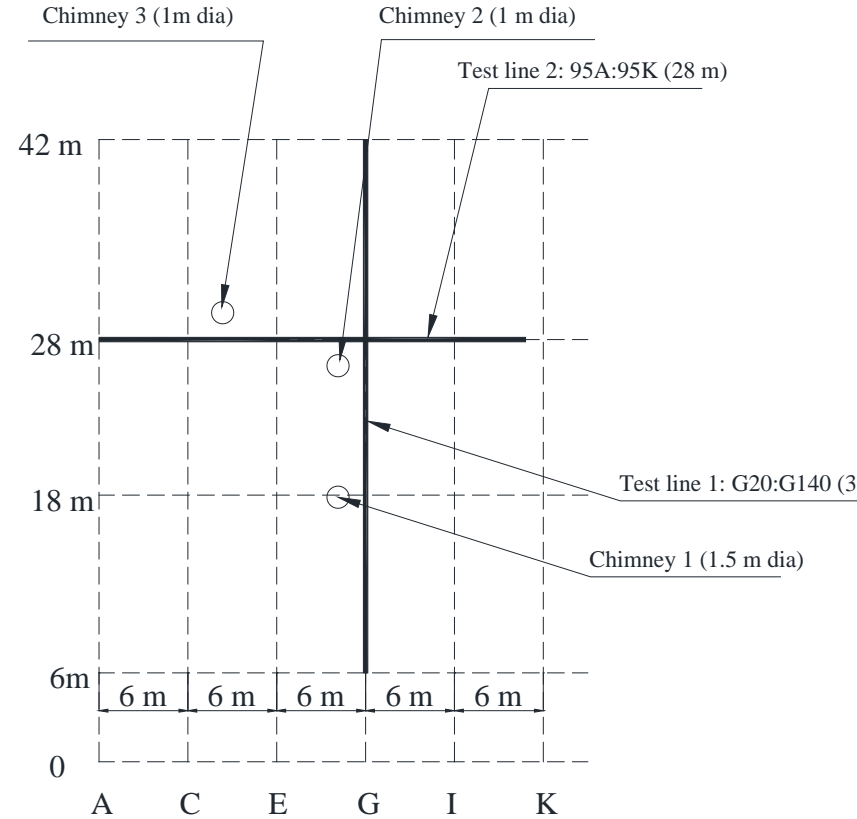
Site 3a: Southern portion



Chimney 2

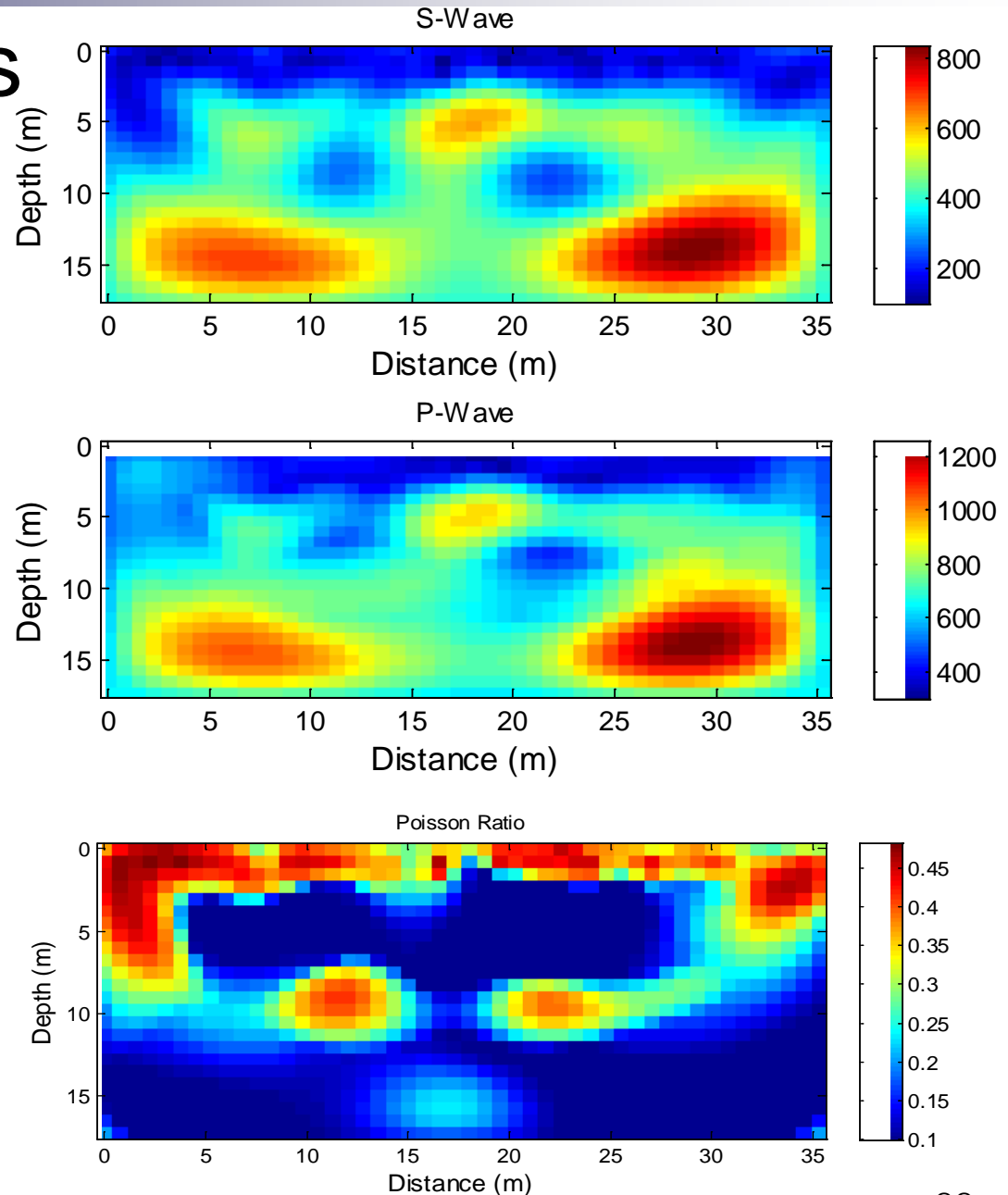


Chimney 3



Site 3a: Results

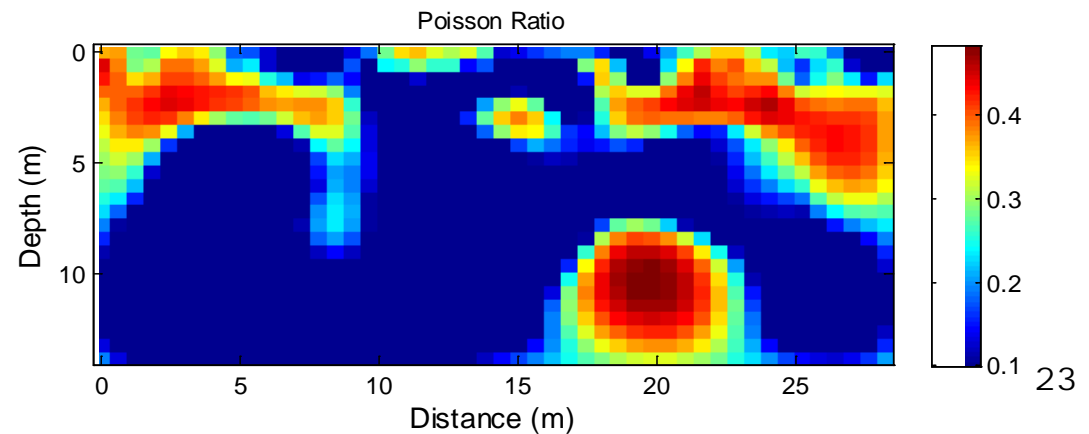
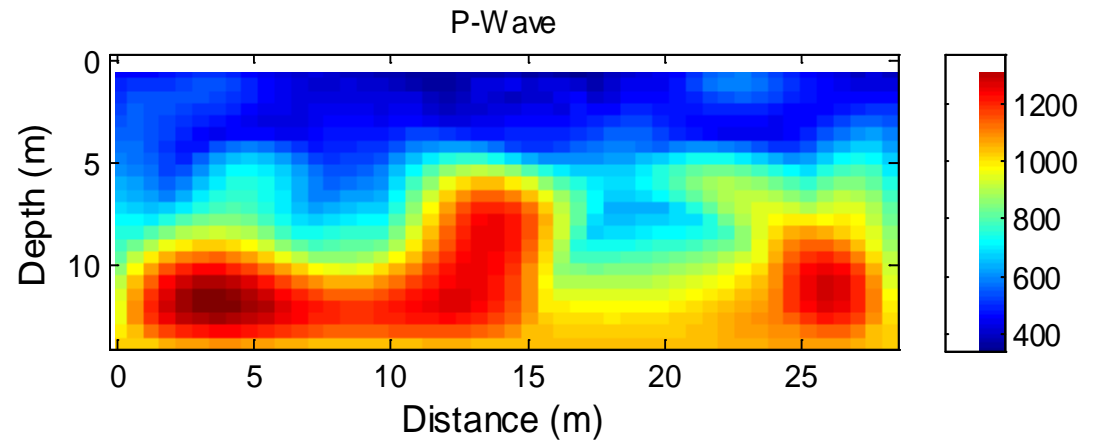
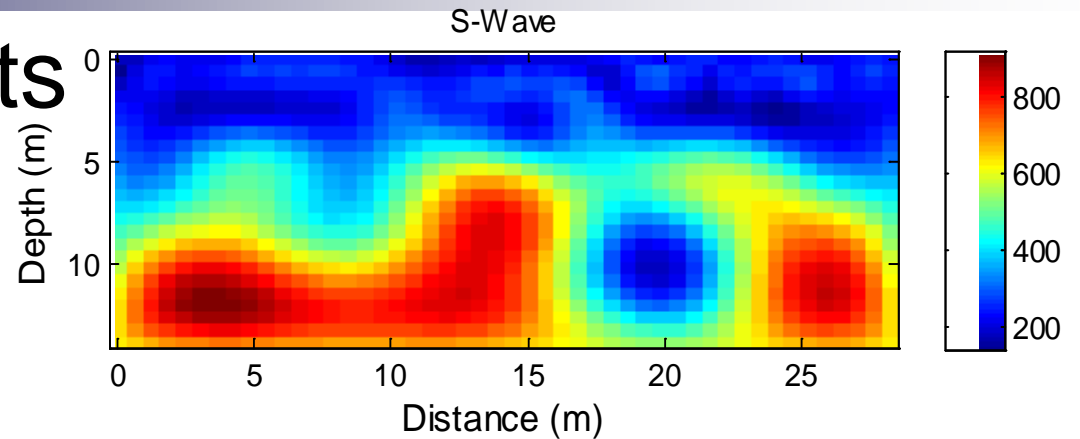
- Result of Line 1
 - 2 anomalies near chimneys 1 and 2 at locations 12 m and 21 m
 - Poisson's ratio is consistent with soil types



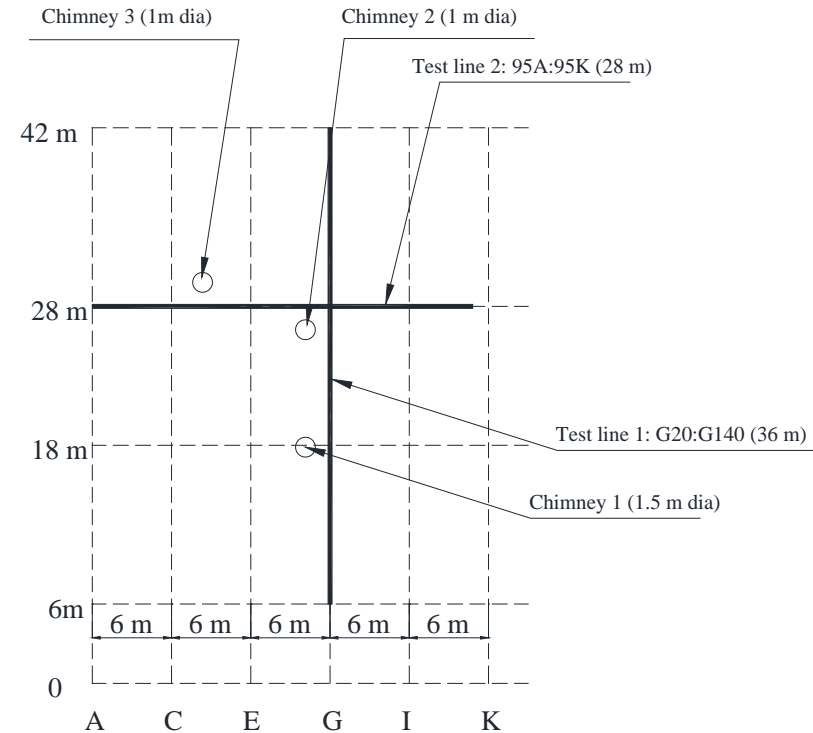
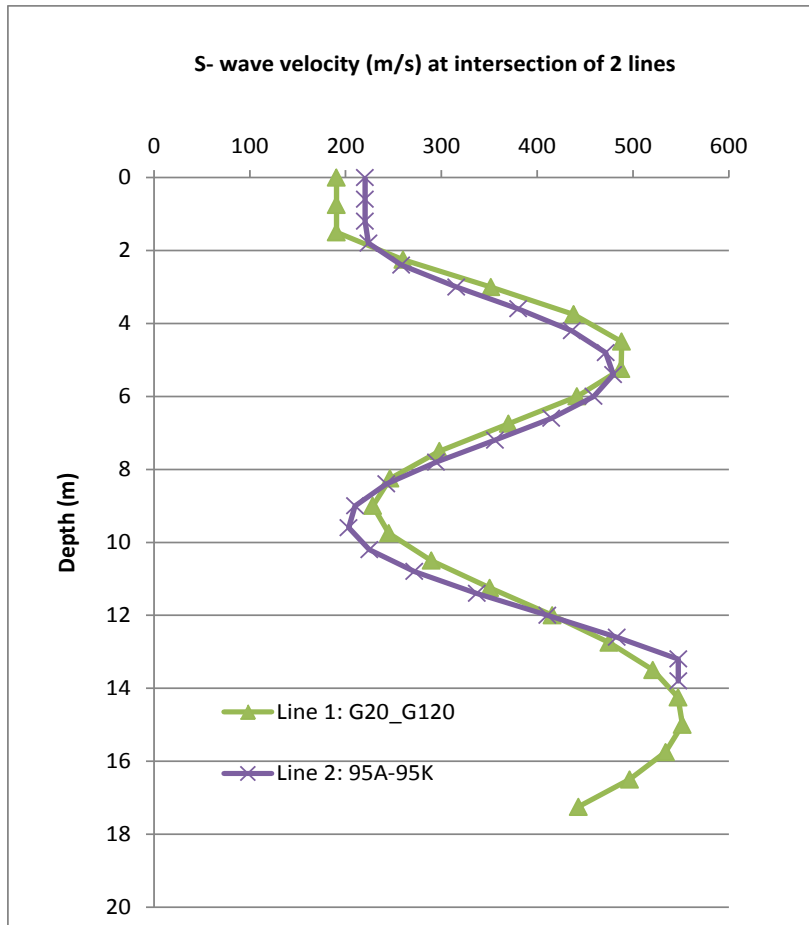
Site 3a: Results

➤ Result of Line 2

- Low-velocity soil near chimney 3 at location of 8 m
- anomaly near the chimney 2 at location of 17 m
- Poisson's ratio is consistent with soil types



Site 3a: Results



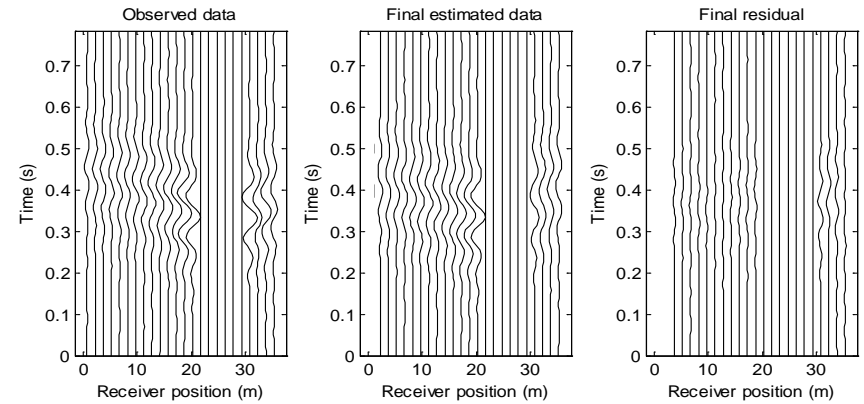
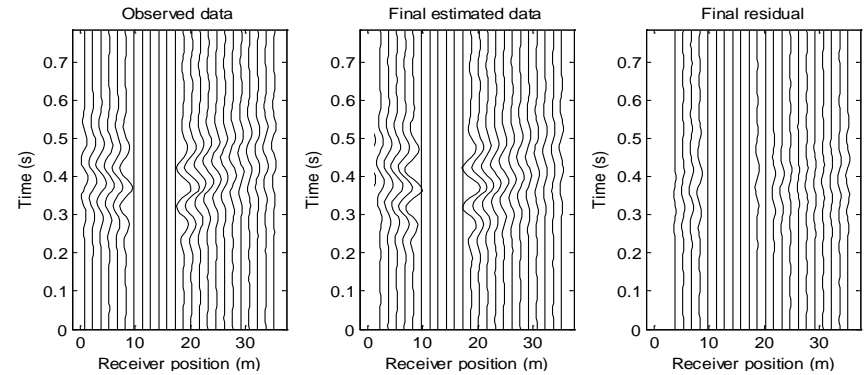
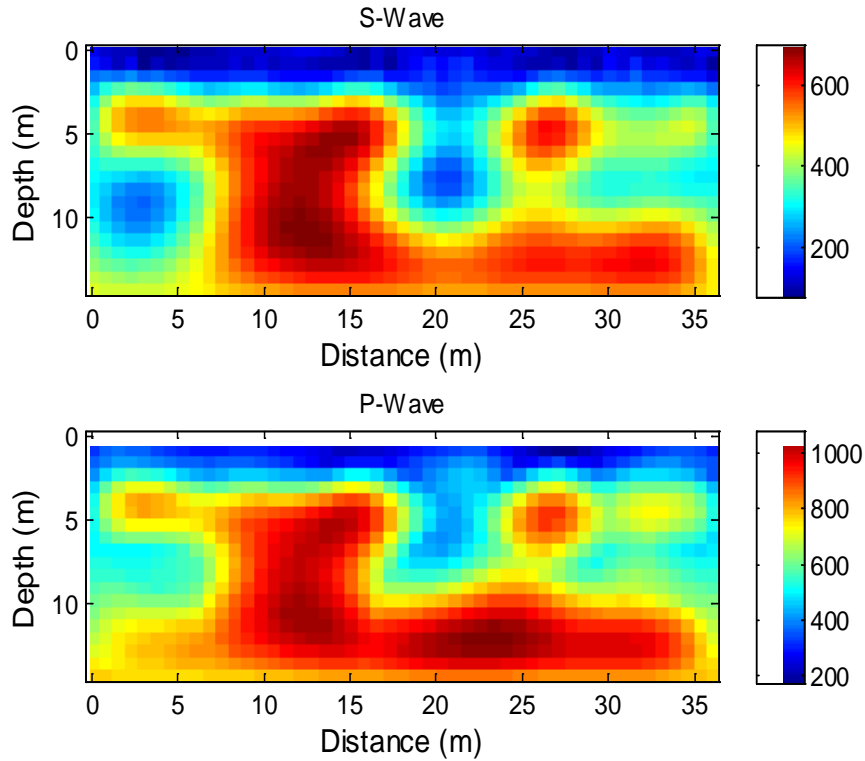
- Comparison of inverted S-wave velocity profiles at the intersection of 2 lines (22 m of line 1 and 18 m of line 2)

Site 3b: Northern portion

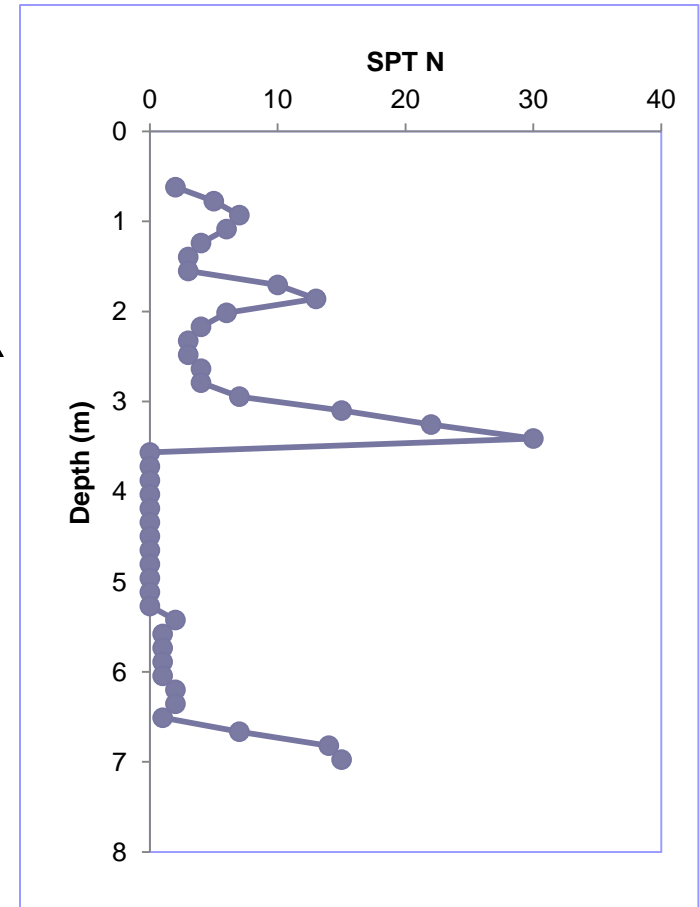
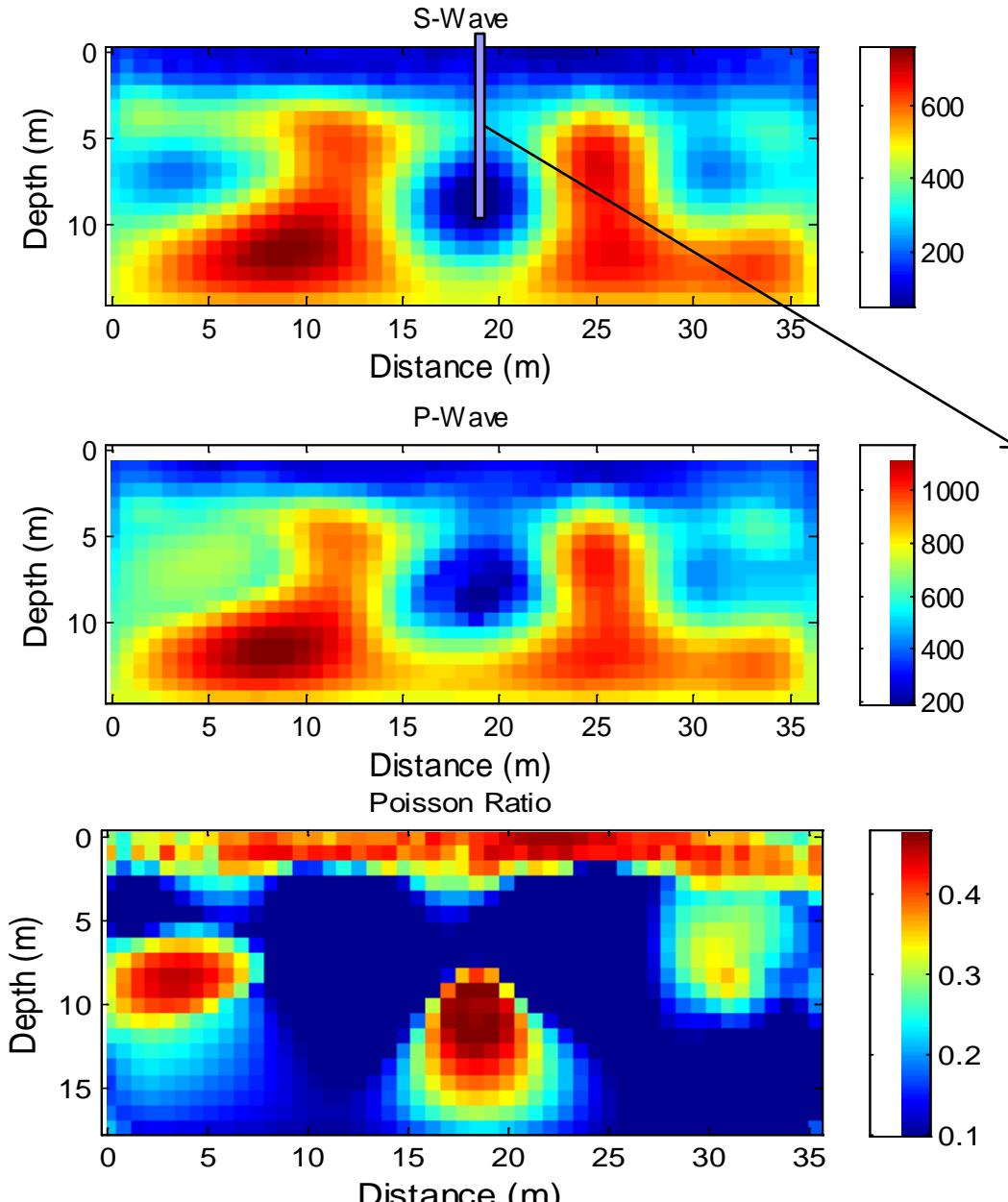
- Test configuration
 - No indication of voids on the surface
 - 10 testing lines at 3 m spacing (line K, L, M, N, O, P, Q, R, S, and T)
 - each line 36 m long
 - 24 geophones at 1.5 m spacing
 - 25 shots at 1.5 m spacing



Site 3b: Results of line P

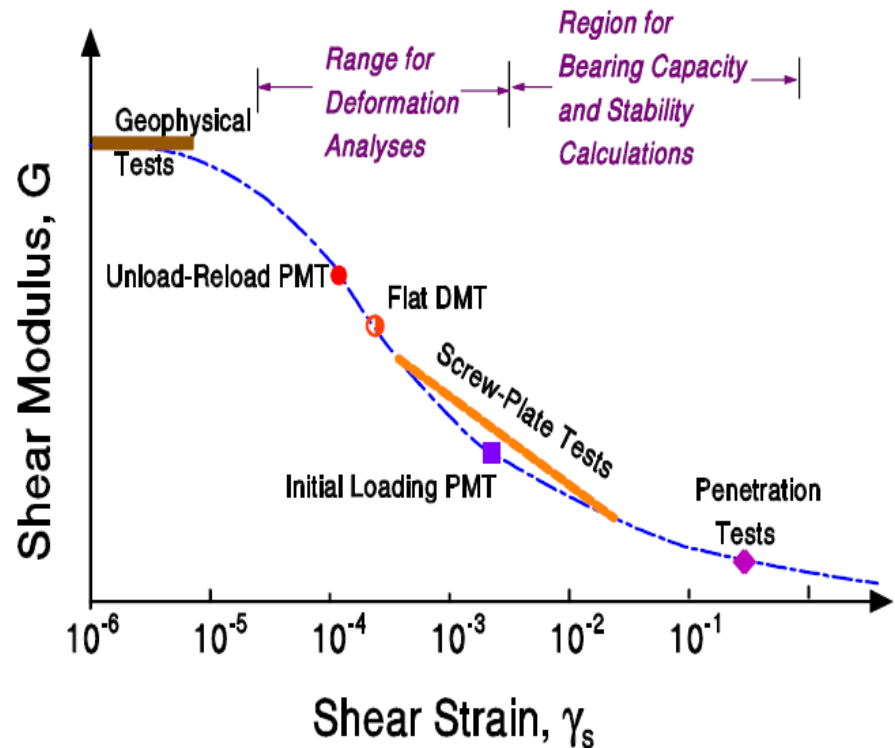


Site 3b: Results of line Q



Use FWI for Design of Foundations

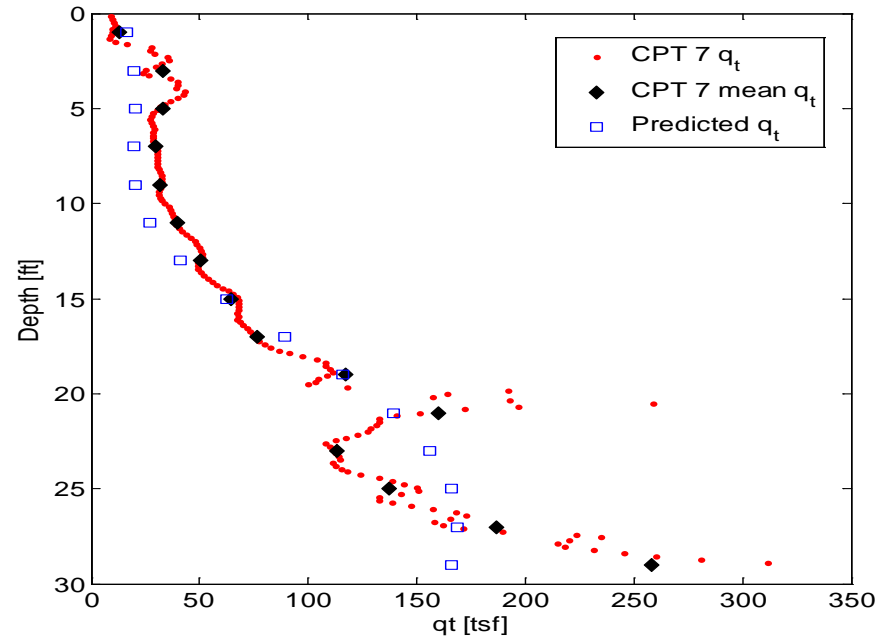
- Extrapolate shear modulus (G) at large strain levels from the maximum shear modulus (G_{max}) at low strain from NDT using reduction curves
- Use both shear modulus (G) and Poisson's ratio for design of foundations



- Reduction Curve (Mayne, 2001)

Use FWI for Design of Foundations

- Use FWI in combination with invasive tests to develop relationships between S-wave velocity vs. CPT or SPT parameters
- Use the developed relationships to predict the CPT or SPT parameters at unobserved locations



- Keystone Heights

Conclusion

Advantages:

- FWI technique provides high-resolution characterization of subsurface conditions (0.5 -1 m 2-D cells)
- S-wave and P-wave velocities are determined independently and simultaneously to increase the credibility of characterized profiles
- Embedded low-velocity anomalies/voids are well characterized without requirement of prior information of subsurface conditions
- Poisson's ratio calculated from the P-wave and S-wave velocities is consistent with soil types
- Both soil type and soil stiffness are obtained for design of foundations

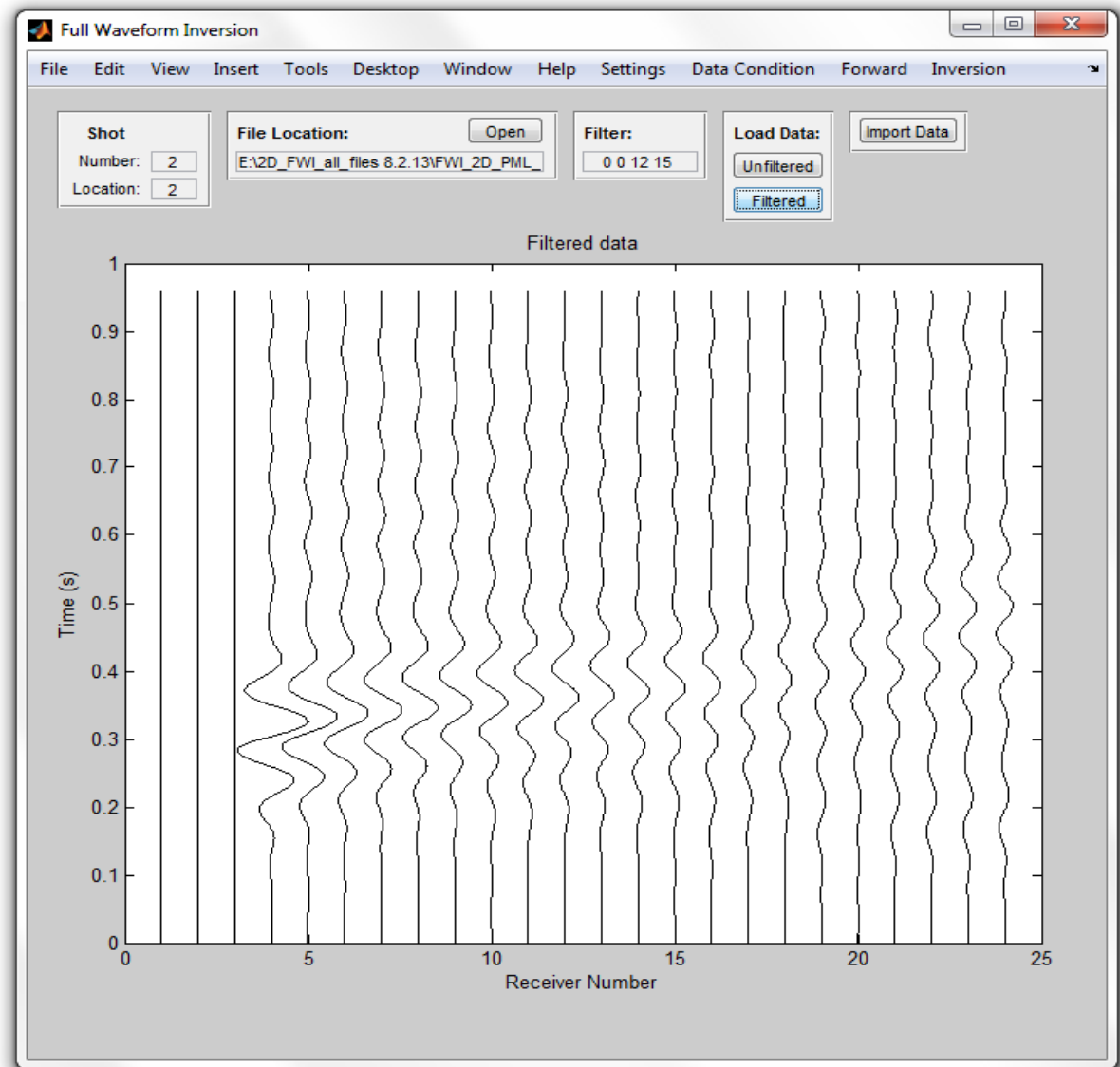
Limitation:

- 2-D FWI still requires significant field testing effort to identify an anomaly/void

Future work (Proposed)

1) Develop FWI software:

- Graphical User Interface (GUI)
- Interact through computer graphics
- Allow technician to collect and analyze data



Future work

2) Develop of a “real-time” FWI solution (20 min for inversion of one set of data):

- Automatic full waveform inversion (data condition, initial model, grid sizes...)
- Advanced boundary condition: perfectly matched layers
- Various sizes of grids for the inversion, temporal windowing, and parallelizing computations

3) Improve FWI use for foundation design:

- Develop Soil Classification Chart vs. FWI S- and P-wave velocities
- Establish FWI S- and P-wave velocities vs. Other Insitu (CPT, SPT) vs. Soil Type

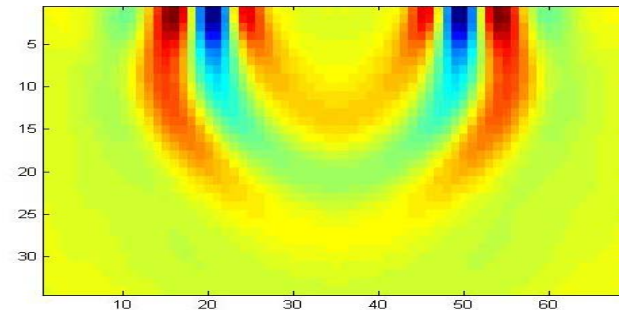
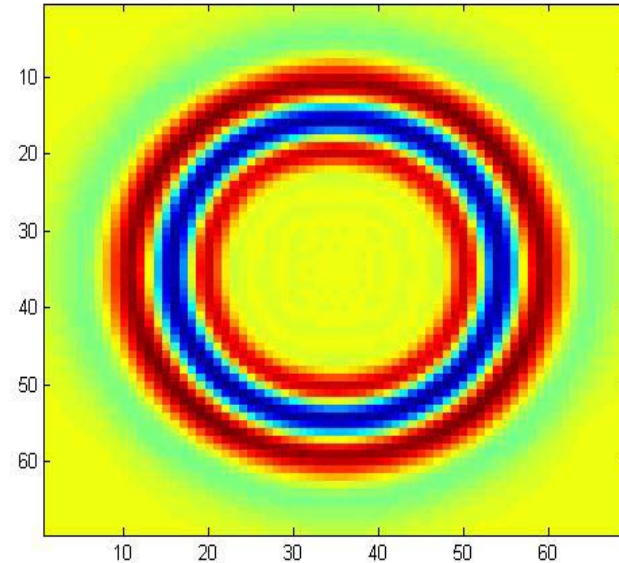
4) Improve of data acquisition

- Advanced source (propelled energy generator, air guns)
- Land streamer

Future work

5) Develop a 3-D FWI technique:

- Use 2-D uniform grids of geophones and shots on the ground surface
- Invert measured data to extract 3-D velocity structures
- Applications: anomalies under existing structures, unknown foundations



Propagation of 3-D waves:
plan view on surface (top)
and side view (bottom).

References

- Tran K.T., McVay M., Faraone M., and Horhota D. (2013) “Sinkhole Detection Using 2-D Full Waveform Tomography”, ***Geophysics***, Vol. 78 (5), pp. 1-9
- Tran K.T. and McVay M. (2012). “Site Characterization Using Gauss-Newton Inversion of 2-D Full Seismic Waveform in Time Domain”, ***Soil Dynamics and Earthquake Engineering***, Vol. 43, pp. 16-24.
- Tran K.T., McVay M., Horhota D., Faraone M., and Brian S. “Full Seismic Waveform Tomography at Highly Variable Sites”, ***Soil Dynamics and Earthquake Engineering***, under review

Thank You!

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