

Pile/Shaft Design Using Artificial Neural Networks (i.e. Genetic Programming) with Spatial Variability Considerations

FDOT Contract No.:

BDK-75-977-68

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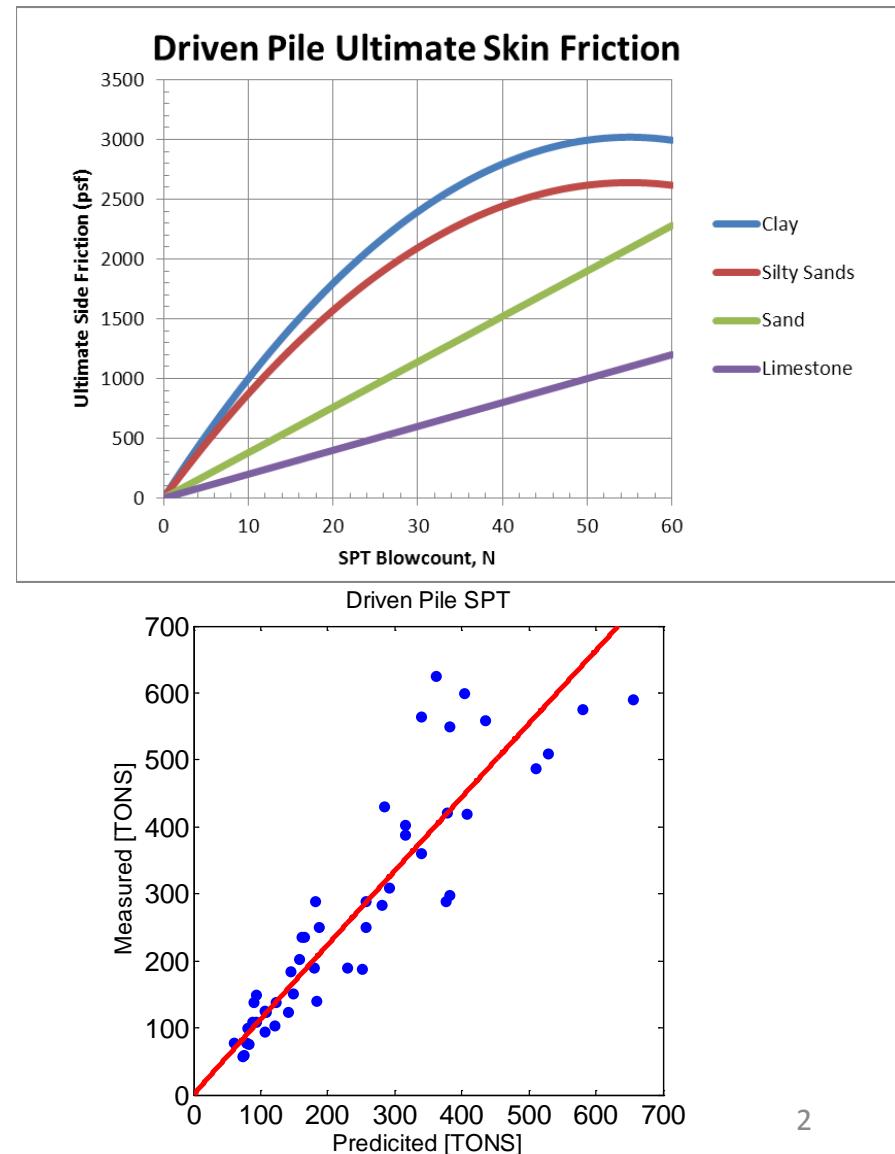
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Scope

- Improvement of prediction equations (side and tip resistance) used by FB-DEEP for both prestressed concrete piles and drilled shafts.
- Optimizing prediction equations by use of a Genetic Program (GP) from site insitu and load test data.



Research Tasks

1. Data Collection
2. Development of Genetic Code to improve Pile/Shft predictions
3. Inclusion of Spatial Variability in assessment of Pile/Shft Capacity Equations
4. Development and Evaluation of Pile Capacity Equations from Insitu Data
5. Final Report and Database Upload

Data Collection

- Geotechnical Reports
 - SPT Boring Logs
 - Lab Test for Rock
 - q_u - unconfined compressive strength
 - q_t - split tensile
 - E - Modulus
 - REC/RQD – Recovery
- Load Test Reports
 - Drilled Shafts and Driven Piles
 - Static
 - Osterberg
 - Statnamic

FDOT Database

- Standardize format
- Organize site data based on hierarchy structure
 - Project
 - Bridge
 - Pier
 - Pile/Shaft
 - Load Test
 - Subsurface
 - Borings
 - Lab Data
 - fdot.ce.ufl.edu

Formatting Insitu Data

Insitu_v2-01 [Compatibility Mode] - Microsoft Excel

File Home Insert Page Layout Formulas Data Review View

Cut Copy Format Painter

Font Alignment Number Styles Cells Editing

AutoSum Fill Clear Sort & Filter Find & Select

I7 f1

Project Name: Buckman Bridge

Section: Township: Range: Coord. System: Vertical Datum: Project #: 72001-3462

county: Duval hole name: B-21 test date: report date:

GWT elev: 2 (ft) top of boring: -20 (ft) ground elev: -20 (ft) latitude: longitude: station #: 285+50 offset: 94 Reference:

x coord.: #N/A (ft) y coord.: #N/A (ft)

x coord.: 28550.00 (ft) y coord.: 94.00 (ft)

Generate elev from depth **CLEAR CONTENTS**
Generate depth from elev **DELETE THIS RECORD**

Soil Pre-descriptor **Soil Type** **Soil Post-descriptor** **USCS** **AASHTO**

Note

Line # elev. (ft) depth (ft) N blows interval (in)

1 scroll & click in list boxes here

line #	elev. (ft)	depth (ft)	N blows	interval (in)	Soil Pre-descriptor	Soil Type	Soil Post-descriptor	USCS	AASHTO	Note
1	-22.00	2.00	0	12	BROWN	Muck/Peat	SOFT	Pt		
2	-27.00	7.00	0	12	BROWN	Muck/Peat	SOFT	Pt		
3	-32.00	12.00	0	12	BROWN	Muck/Peat	SOFT	Pt		
4	-37.00	17.00	1	12	BROWN	Muck/Peat	SOFT	Pt		
5	-42.00	22.00	1	12	BROWN	Muck/Peat	SOFT	Pt		
6	-47.00	27.00	2	12	BROWN	Muck/Peat	SOFT	Pt		
7	-52.00	32.00	2	12	BROWN	Muck/Peat	SOFT	Pt		
8	-55.00	35.00				Stratum Change				
9	-57.00	37.00	10	12	DARK TO LIGHT BROWN FINE	Sand	TO DENSE	SP		
10	-62.00	42.00	15	12	DARK TO LIGHT BROWN FINE	Sand	TO DENSE	SP		
11	-67.00	47.00	33	12	DARK TO LIGHT BROWN FINE	Sand	TO DENSE	SP		
12	-70.00	50.00				Stratum Change				
13	-72.00	52.00	20	12	GRAY FINE	Sand	COMPACT	SP-SC		
14	-77.00	57.00				Stratum Change				
15	-77.00	57.00	10	12	GRAY	Clay	STIFF	CH		
16	-80.00	60.00				Stratum Change				
17	-82.00	62.00	39	12	GRAY TO BROWN FINE	Sand	VERY	SP		
18	-87.00	67.00	35	12	GRAY TO BROWN FINE	Sand	VERY	SP		
19	-92.00	72.00	70	12	GRAY TO BROWN FINE	Sand	DENSE TO V	SP		
20	-97.00	77.00	70	12	GRAY TO BROWN FINE	Sand	DENSE TO V	SP		
21	-102.00	82.00	52	12	GRAY TO BROWN FINE	Sand	DENSE TO V	SP		
22	-105.00	85.00				Stratum Change				
23	-107.00	87.00	14	12	BLUE	Clay	STIFF	CH		
24	-110.00	90.00				Stratum Change				
25	-112.00	92.00	31	12	BLUE	Clay	WITH SAND	CH		
26	-115.00	95.00				Stratum Change				
27	-117.00	97.00	49	12	GRAY	Sand	WITH CLAY	SP-SC		
28	-122.00	102.00	51	12	GRAY	Sand	WITH CLAY	SP-SC		

SPT N

Average: -1.75 Count: 9 Sum: -7 90% 6

Formatting Load Test Data

Sample

Project No.	49010-353	Name	Appalachic	
Bridge No.	1	Load	Disp 2	Disp 4
Pier Name	16	0.00	0.00	0.00
Pile Name	LT4	13.00	0.00	0.01
Pile Type	1 - concrete	18.40	0.01	0.01
Description	circular	32.80	0.01	0.02
Pile Elastic Modulus (ksi)	4030.509	51.00	0.02	0.03
Void Diameter (in)	0.00	67.20	0.03	0.03
Width or Diameter (in)	18.00	85.20	0.03	0.04
Cross Sectional Area (in ²)	324.00	103.00	0.04	0.05
Total Length (ft)	65.20	121.80	0.05	0.07
Embedment Length (ft)	61.00	138.80	0.07	0.08
Pile Weight (kip)	22.00	156.60	0.08	0.10
Concrete Strength (ksi)	5	175.20	0.10	0.11
Station	132+09.00	194.00	0.11	0.13
Offset	0	210.80	0.13	0.16
Company		227.80	0.16	0.19
LT Type	1 - Compression Cycle	246.60	0.19	0.24
		265.60	0.24	0.31
		283.40		

Add Record Load Vs Disp4

Select Record : Pier = 16, Pile = LT4
Pier = 14, Pile = LT2
Pier = 16, Pile = LT4
Pier = 25, Pile = LT3
Pier = 3, Pile = LT1

Static LT Comments :

Save as XML Load XML Exit

Load Vs Disp4

Disp4 (in)	Load (kips)
0.00	0
0.02	10
0.05	30
0.10	60
0.15	100
0.20	150
0.30	220
0.40	280
0.50	320
0.60	340
0.70	350
0.80	300
0.90	250
0.95	350
1.00	350

Driven Pile Datasets

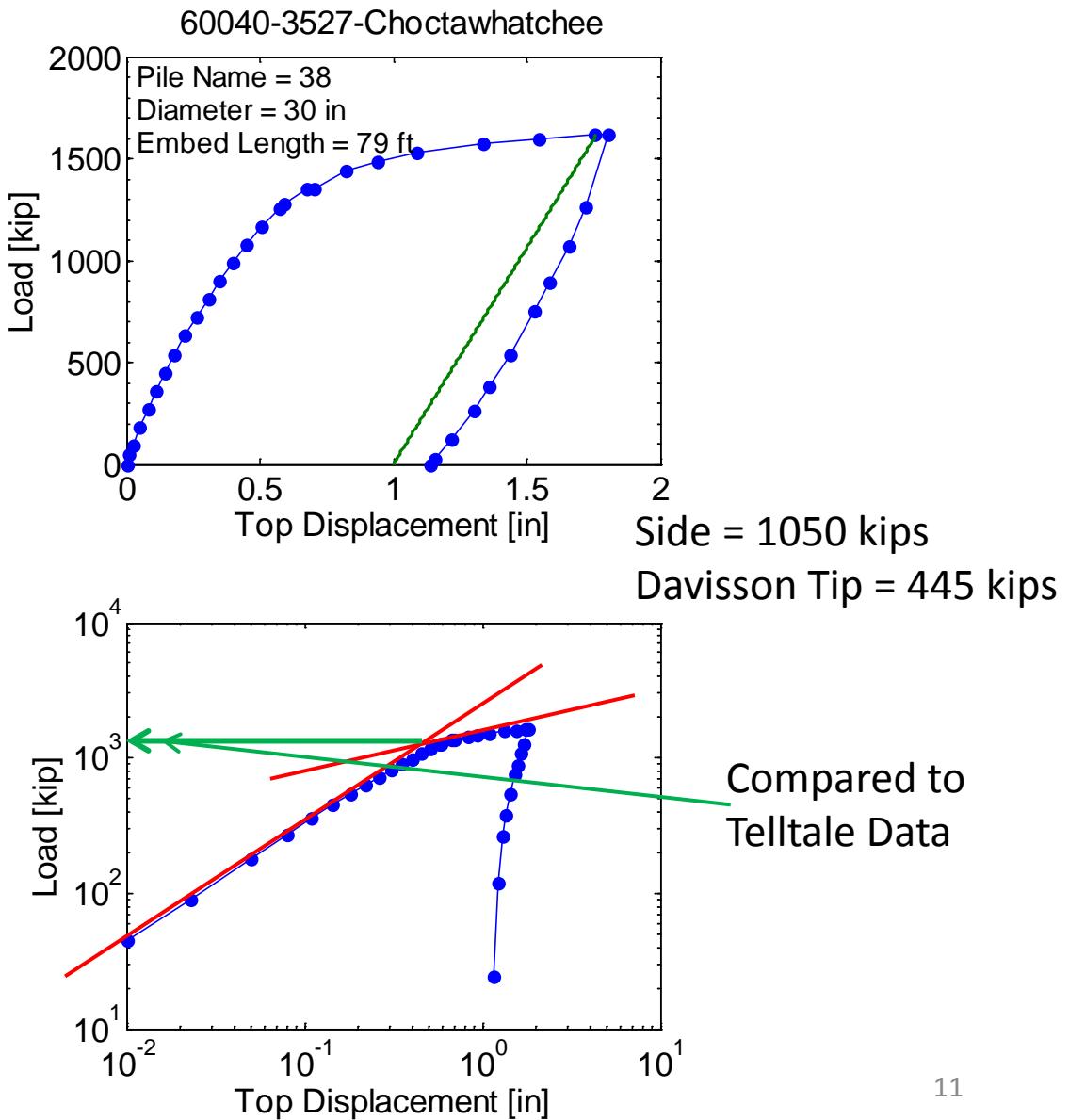
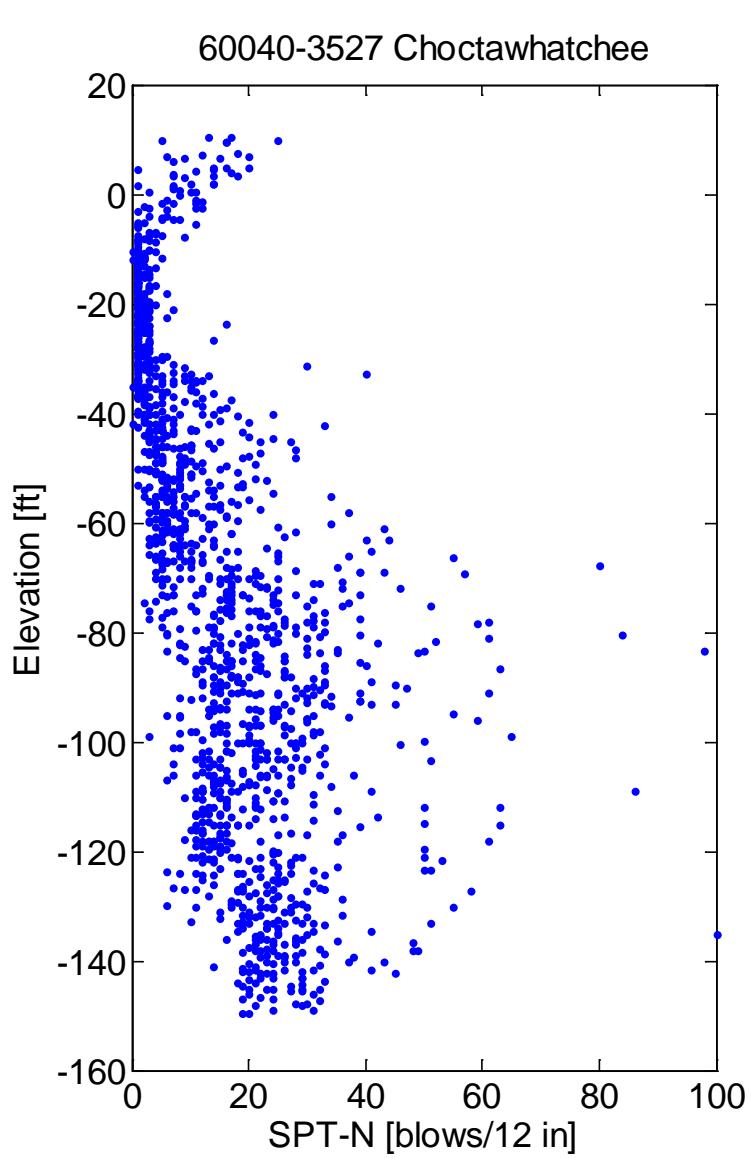
Project Site	Project Number	Borings (Firm)	Load Tests (Firm)	No. Borings	No. Load Tests	Foundation		
						Dimension (in.)	Pile (Concrete/Steel)	Length (ft)
5th St. Bascule Bridge	412808-1-52-01	Mactec	Applied Foundations	7	4	18	Concrete	55
Acosta Bridge	72160-3506	Law Engineers	Schmertmann & Crapps	53	3	24	Concrete	39-67
Apalachicola Bay	49010-3536	F.D.O.T.	Schmertmann & Crapps	28	5	18-24	Concrete	68.2-123.7
Apalachicola River	49010-3533	F.D.O.T.	Schmertmann & Crapps	33	4	18-30	Concrete	65.2-93.2
Bayou Chico	48050-3536	F.D.O.T.	Williams Earth Sciences Inc.	7	3	24	Concrete	46-87
Blackwater Bridge (I-10)	58002-3449	Williams Earth Sciences Inc.	Williams Earth Sciences Inc.	4	2	24	Concrete	115
Buckman Bridge	72001-3462	Ardaman & Associates	Schmertmann & Crapps	40	8*	30	Concrete	104.5-121
Caminida Bay	061-01-0040	Applied Foundations	LA D.O.T.	4	2	30	Concrete	55-60
Choctawhatchee	60040-3527	F.D.O.T.	Schmertmann & Crapps	35	10	24-30	Concrete	69-125
Dixie Highway	230656-1-52-01	PSI	Applied Foundations	22	3	24	Concrete	50

Project Site	Project Number	Borings (Firm)	Load Tests (Firm)	No. Borings	No. Load Tests	Foundation		
						Dimension (in.)	Pile (Concrete/Steel)	Length (ft)
Dodge Island	87000-3675	Law Engineers	Law Engineers	6	3*	30	Concrete	65-110
Escambia River	48140-3509/58080-3516	F.D.O.T.	Schmertmann & Crapps	53	2	24	Concrete	65-92
Fort Myers	12001-3513	Ardaman & Associates	HDR	5	1	14	Concrete	34.3
Howard Frankland	15190-3479	Williams and Associates	HDR	49	4	30	Concrete	52.9-101.8
Julington Creek	78070-3517	PEC	Ardaman & Associates	29	3	24	Concrete	80-95
Mantanzas River (SR 312)	78002-3509	F.D.O.T.	Williams Earth Sciences Inc.	8	4*	24	Concrete	140-150
Port Orange	79180-3514	Franco/Williams/ Dawson	Schmertmann & Crapps	11	2	18	Concrete	32.8-34.3
Roosevelt Bridge	89010-3541	Law Engineers	Law Engineers	41	2	30	Concrete	62.5-70
Sunshine Skyway	15170-3421	Williams and Associates	Schmertmann & Crapps	22	7	20-24	Concrete/Steel	38.2-79.6
West Bay Bridge	217911-5-52-01	F.D.O.T.	Dames & Moore	19	2	30	Concrete	105-130
White City Bridge	51020-3514	F.D.O.T.	Dames & Moore	16	2	24	Concrete	31-125.6
* = includes tension tests				Borings	Load Tests			
			Totals:	492	61			

Drilled Shaft Datasets

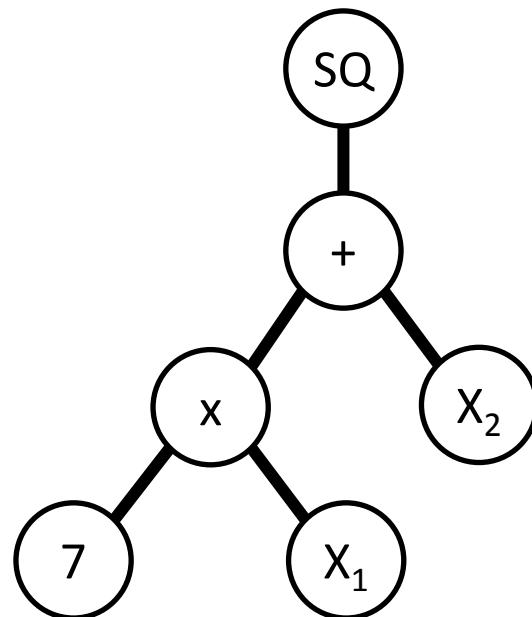
Project Site	Project Number	Borings (Firm)	Load Tests (Firm)	No. Borings	No. Load Tests	Foundation	
						Dimension (in.)	Length (ft)
Appalachicola River (S.R.20)	47010-3519/ 56010-3520	Ardaman and Associates	Schmertmann & Crapps	148	8	108	80-160
Fuller Warren	72020-1485	Law Engineering	N/A	26	4	36-72	74.5-201.5
Gandy Bridge	10130-1544	Beiswenger, Hoch & Assoc.	Williams and Associates	116	6	48	43.1-83
Macarthur Causeway	87060-1549	Law Engineering	Law Engineering	44	5	48	30.5-150
17th Street	86180-1522	Williams and Associates	LOADTEST Inc	95	3	48	40-100
Sunshine Skyway	15170-3421	Williams and Associates	Schmertmann & Crapps	22	10	24-48	38.2-79.6
Venetian Causeway	11120-158-141	Dames & Moore	Florida Testing & Engineering, Inc	17	10	48	50-82
Victory Bridge	53020-3540	F.D.O.T.	Schmertmann & Crapps	28	6	48	69-100
Lee Roy Selmon	10190-1416	PSI	Applied Foundation	504	13	48	46.7-79.9
				Borings	Load Tests		
			Totals:	1000	65		

Data for Genetic Program



Genetic Program

- Optimization tool based on natural selection and evolutionary algorithms.
- Optimizes a prediction model based on a set of inputs (insitu data) and corresponding outputs (load test).
- Previous work done for driven pile models using CPT- q_t , and shallow foundation settlement from SPT-N.
- Begins with generation of random population of models.
- Model represented by tree structure

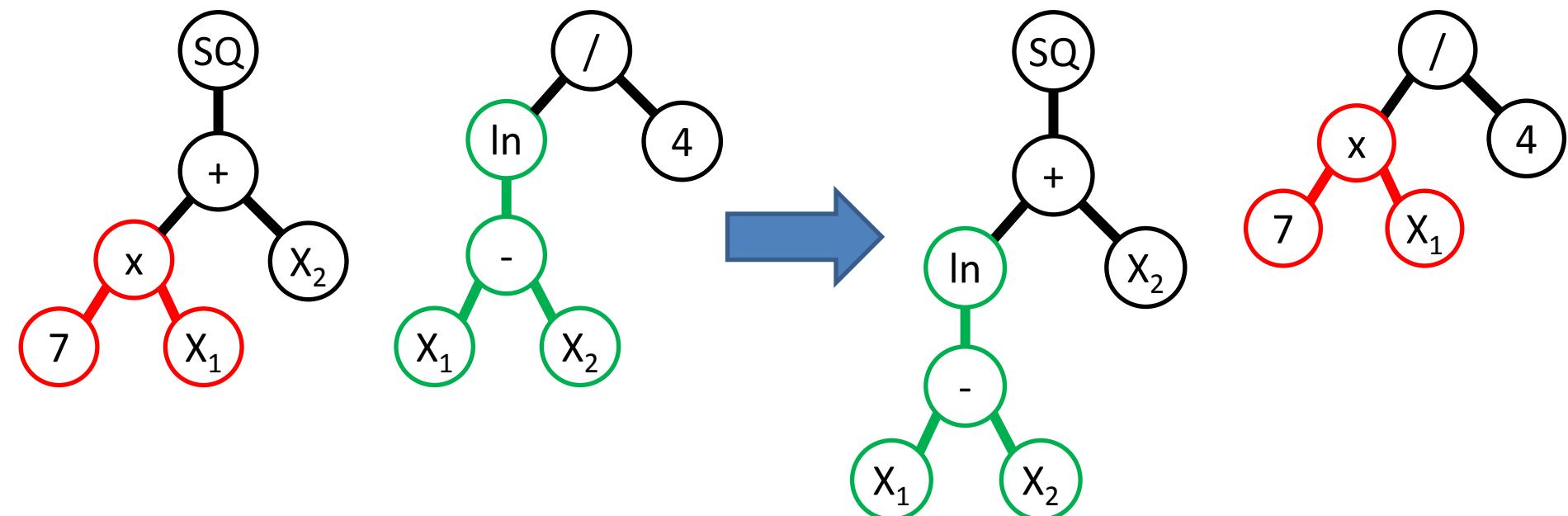


$$[7X_1 + X_2]^2$$

Crossover

Selection of two models from the population

Resulting new models for next generation



$$[7X_1 + X_2]^2$$

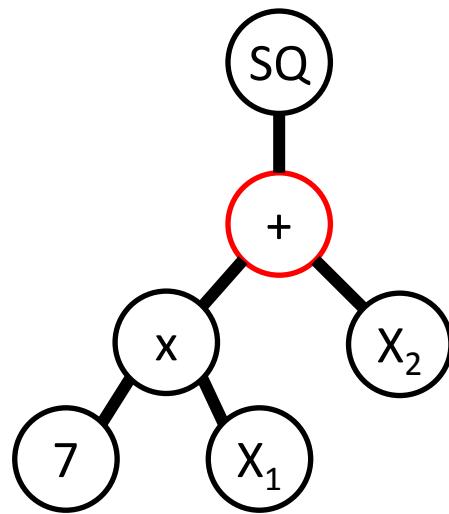
$$\frac{\ln(X_1 - X_2)}{4}$$

$$[\ln(X_1 - X_2) + X_2]^2$$

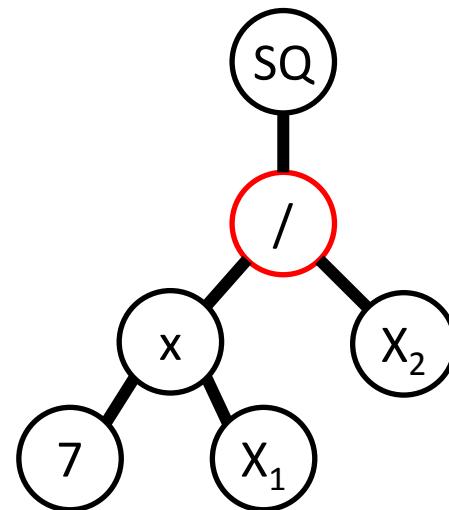
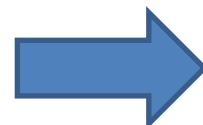
$$\frac{7X_1}{4}$$

Mutation

Selection of one model from the population



Resulting new model for next generation

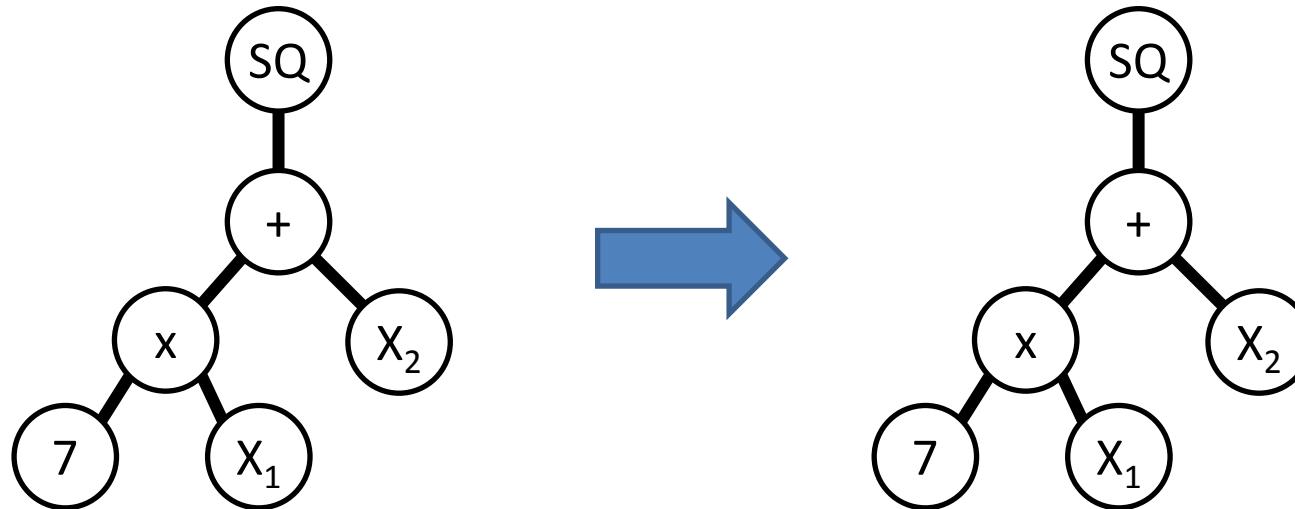


$$[7X_1 + X_2]^2$$

$$\left[\frac{7X_1}{X_2} \right]^2$$

Reproduction

- One model is selected from the population and copied over to the next generation.



$$[7X_1 + X_2]^2$$

$$[7X_1 + X_2]^2$$

Selection Criteria/Fitness

- Need a basis for which models are selected for use in evolutionary algorithms.
- For symbolic regression can use R^2 , mean squared error (MSE), etc. to quantify how well the predict model fits the measured data.
- Assign a probability of selection for model based on fitness score relative to entire.
 - i.e. Better fitting models have a higher chance of being selected.
- Repeat this process for multiple generations until optimal solution is determined.

$$MSE = \frac{1}{N} \sum (M - P)^2$$

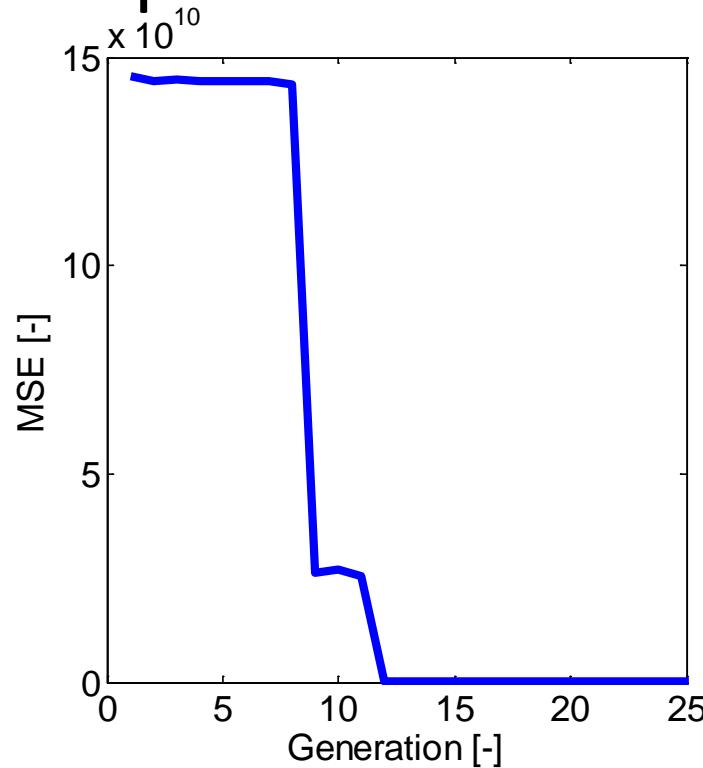
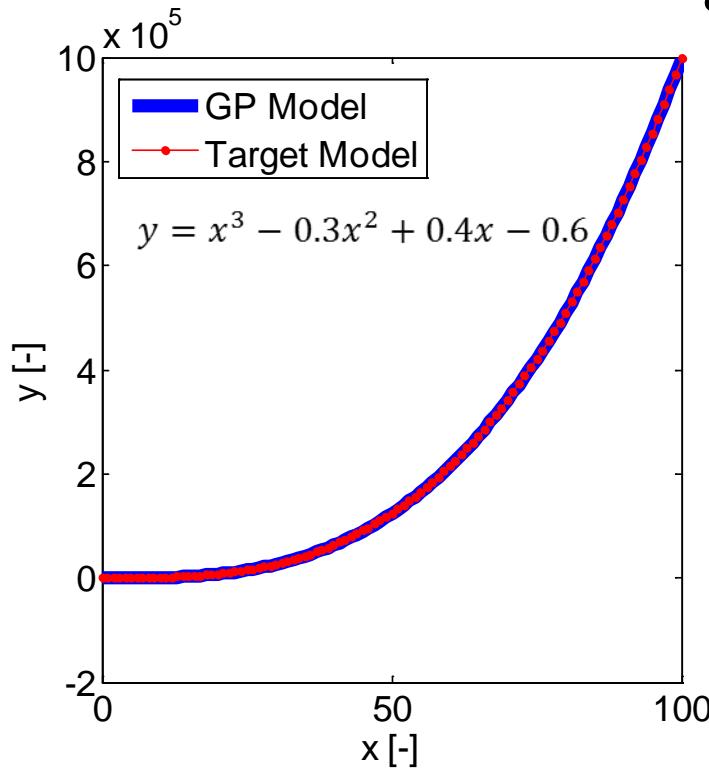
M – measured value

P – corresponding model prediction

N – number of data points

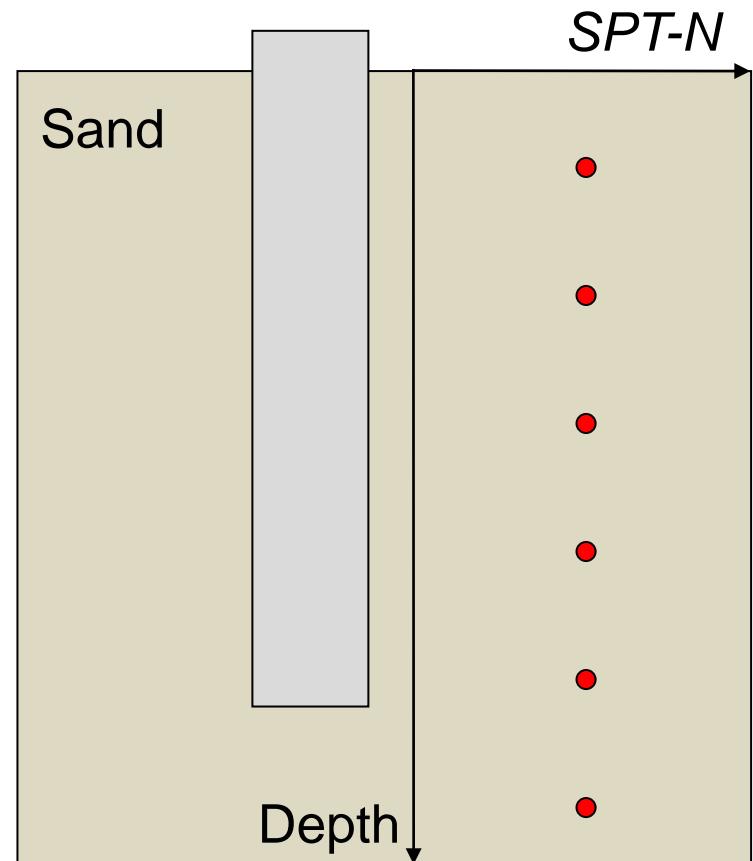
Implementation and Validation

- Coded in MATLAB using data downloaded from the FDOT database.
- Validation for solving 1 equation.



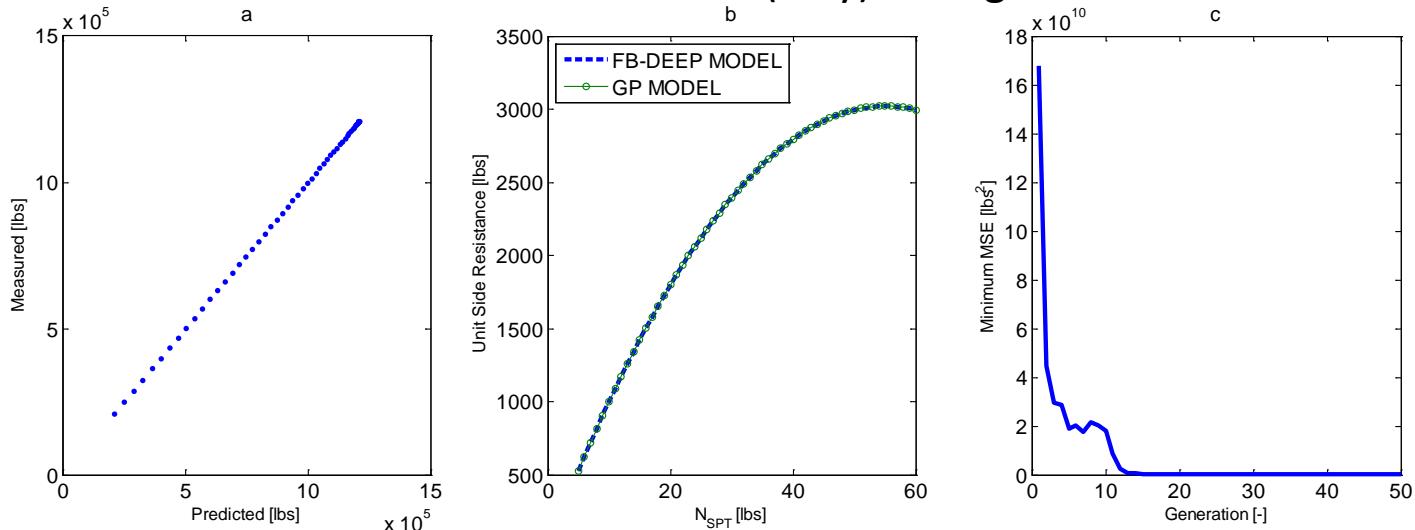
Validation cont.

- See how well GP predicts FB-DEEP models.
- Create borings logs of uniform SPT-N blow count and soil type.
- Generate multiple profiles with different SPT-N.
- Use FB-DEEP calculation to be representative load test.

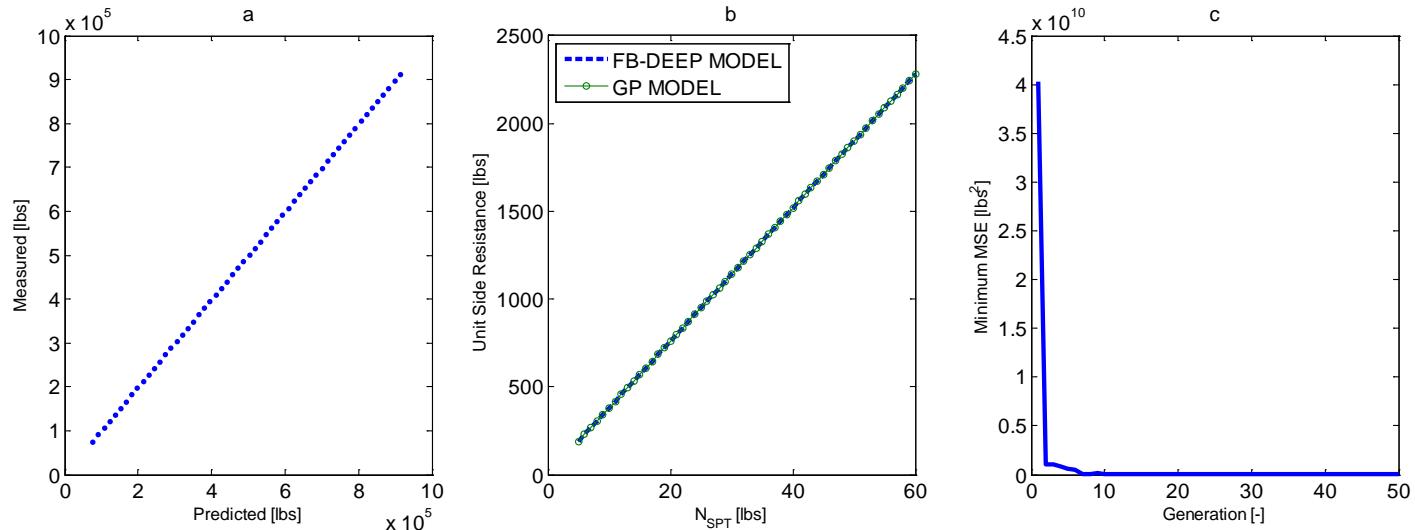


Validation cont.

FB-DEEP SOIL TYPE 1 (Clay) Fitting

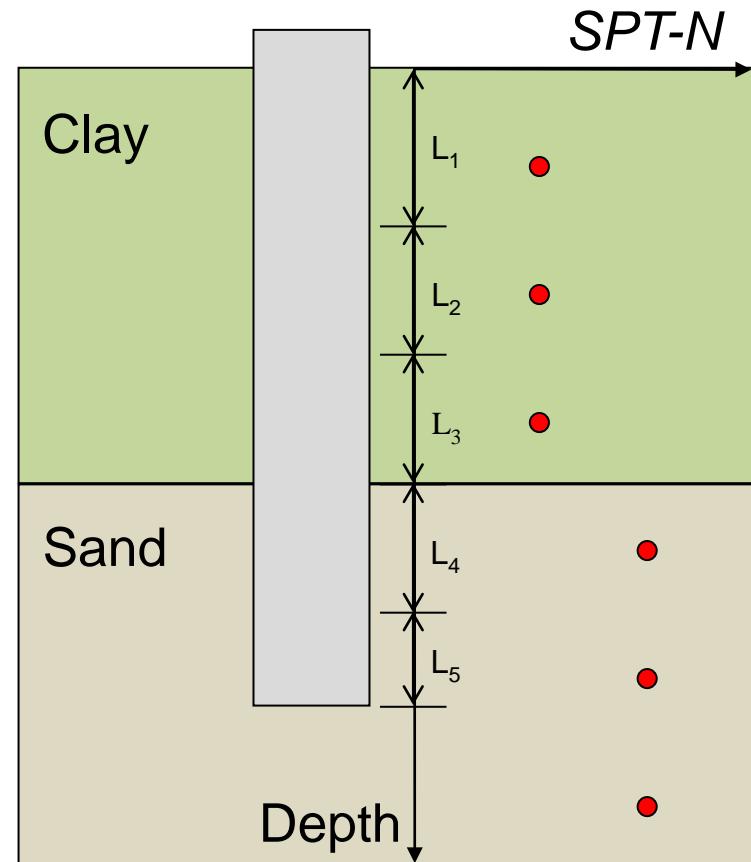


FB-DEEP SOIL TYPE 3 (Sand) Fitting



Validation cont.

- See how well GP predicts 2 FB-DEEP models at the same time.
- Create borings logs with 2 uniform layers of SPT-N blow count and soil type.
- Generate multiple profiles with different layering and SPT-N.
- Determine L_i , to evaluate SPT-N's contribution to side resistance.



GP Capacity Prediction

- GP needs to account for different layering sizes as well as sample spacing.
- Li provides means to determine a weighted average.
- Driven Pile data set only provides total resistance, which side and tip can be derived from.
- GP then has to evaluate fitness based on total side resistance, when optimizing multiple soil type models.

$$\bar{f}_s = \frac{1}{\sum L_i} \sum f_{s_i} L_i$$

$$USF = P \sum \bar{f}_s \sum L_i$$

\bar{f}_s – mean unit side friction of soil type

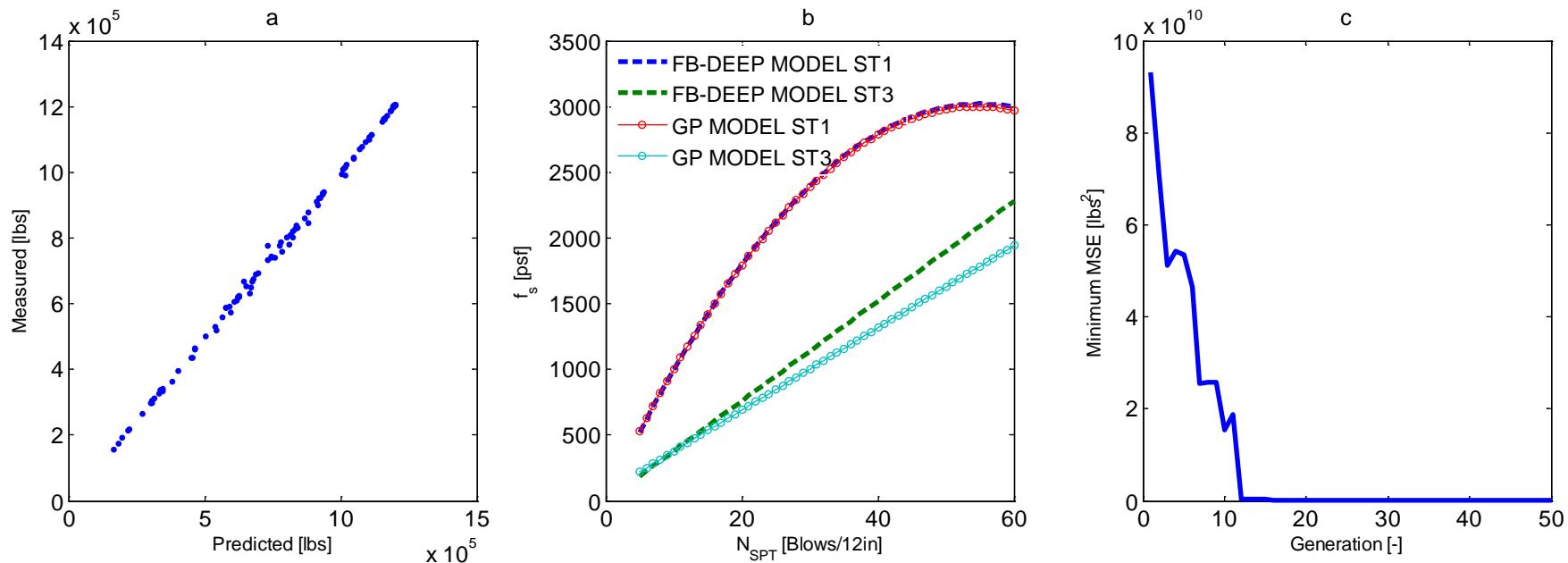
f_{s_i} – unit side friction, function of soil type and SPT-N

L_i – samples attributed length

USF – Ultimate Side Friction of Pile

P – Pile's perimeter

Validation cont.



GP Run	ST 1 Model $f_s = 109.8N_{SPT} - N_{SPT}^2$ (psf)	ST 3 Model $f_s = 38N_{SPT}$ (psf)	MSE (lbs^2)
1	$109.8N_{SPT} - N_{SPT}^2 + 5.28$	$31.3N_{SPT} - \sin(N_{SPT} + 65.5) + 65.1$	1.14e+08
2	$65.9N_{SPT}$	$38.1N_{SPT} - 3.6/\ln(N_{SPT}) + 26.6$	2.07e+10
3	$109.6N_{SPT} - \sin(\sin(14.3 - N_{SPT})) - N_{SPT}^2$	$33.2N_{SPT}$	1.25e+08

GP with Real Data

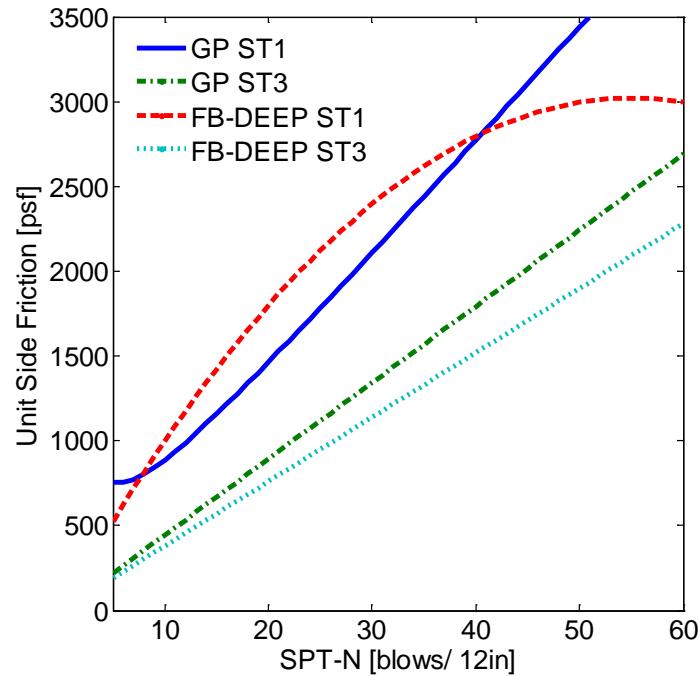
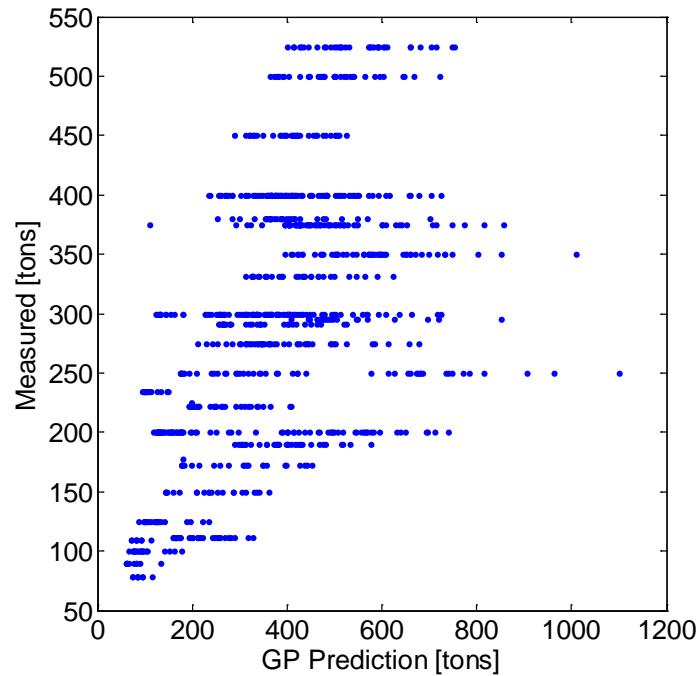
- 9 sites totaling 233 boring 34 load test.
- Ultimate side friction from load test data.
- Optimizing 2 soil type models
- Limited SPT-N to max value of 60
- For each site, ultimate side friction is evaluated for each boring and compared to the corresponding load test piles.

Assignment of Soil Type

- First attempt fitting for cohesion and cohesionless models.
- Binning based on either USCS classification or boring log soil description.
- Automatically sorted using database fields.
- Advantages:
 - less computation time
 - Learn how GP works with real data

Soil Type 1	Soil Type 3
CL	GW
ML	GP
CL-ML	GM
CH	GC
MH	GC-GM
OL	GW-GM
OH	GW-GC
SC	GP-GM
SW-SC	GP-GC
SP-SC	SW
SM-SC	SP
SW-SM	SM
SP-SM	
Pt	

Results



Large scatter can partially be to GP's model error and spatial variation across the site.

Next Phase of GP Work

- Entering Additional FDOT sites into Online database
- Investigation of Different Soil/Rock descriptors
 - Refining of USCS binning.
- Task 3, inclusion of spatial variability in error assessment.
- Investigate the separation of site into multiple zones due to stratigraphy or anisotropy

Next Phase of GP Work -cont

- Evaluate Tip resistance based on soil &rock type.
- Develops Models based on Davisson and Ultimate
- Evaluate Skin and Tip Resistance for Drilled shafts using GP

Questions?